

Traffic Impact Assessment: Hugo Wind Energy Facility (WEF), near De Doorns

Prepared for: ERM (Environmental Resources Management Southern Africa (Pty) Ltd)

5 August 2024

Client Reference No. 0695823_TIA





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Document Control

Document Type	Traffic Impact Assessment Report
Project Title	Traffic Impact Assessment: Hugo WEF, near Beaufort West
Project Number	JT0075
File Location	\\ZAJHFPV002.sjgroup.local\A000 Work on Risk\P1J1\2023\Small Bid folder\JT0075 - Hugo and Khoe Energy Facilities\07 Technical\TIA Report\Hugo WEF Report (.docx)
Revision Number	01


Revision History

Revision No.	Date	Prepared By	Reviewed By	Approved for Issue By
00	9/05/2024	Reabetswe Mokomele Siphelele Ndwandwe	Reabetswe Mokomele	Victor de Abreu
01	5/08/2024	Reabetswe Mokomele Siphelele Ndwandwe	Reabetswe Mokomele	Victor de Abreu

Issue Register

Distribution List	Date Issued	Number of Copies
ERM (Environmental Resources Management Southern Africa (Pty) Ltd)	16/05/2024	01
ERM (Environmental Resources Management Southern Africa (Pty) Ltd)	5/08/2024	02

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1 Introduction

1.1 Background

SMEC South Africa (Pty) Ltd was appointed by ERM (Environmental Resources Management Southern Africa (Pty) Ltd) to undertake a Traffic Impact Assessment (TIA) for the proposed Hugo Wind Energy Facility (WEF) and associated Infrastructure. This TIA is a Specialist Study: Traffic and Transportation intended to support the Environmental Impact Assessment (EIA) approval application for the proposed WEF development.

The proposed development named Hugo WEF is located approximately 35 km southeast of the town of De Doorns, 65 km east of the town of Worcester within the jurisdiction of the Breede Valley Local Municipality, Cape Winelands District Municipality, Western Cape Province.

The proposed Hugo WEF is planned to comprise up to 42 turbines with a maximum output capacity of up to 360 MW. The location of the proposed Hugo WEF is shown in Figure 1-1 and will be located on six (6) land parcels which are indicated on an aerial view of the site in Figure 1-2 and summarised in Table 1-1.

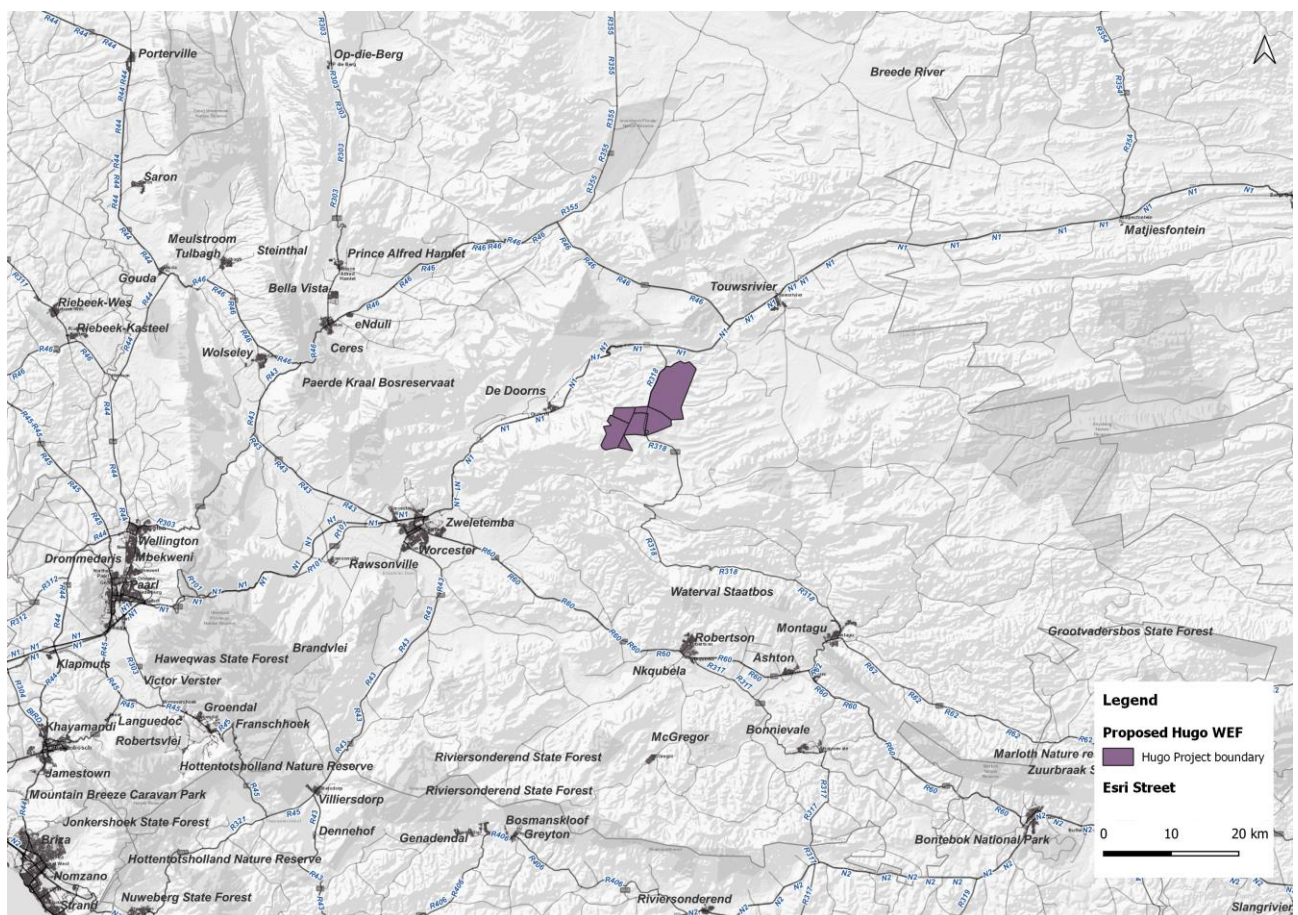


Figure 1-1: Locality Plan (Source: Google Earth)

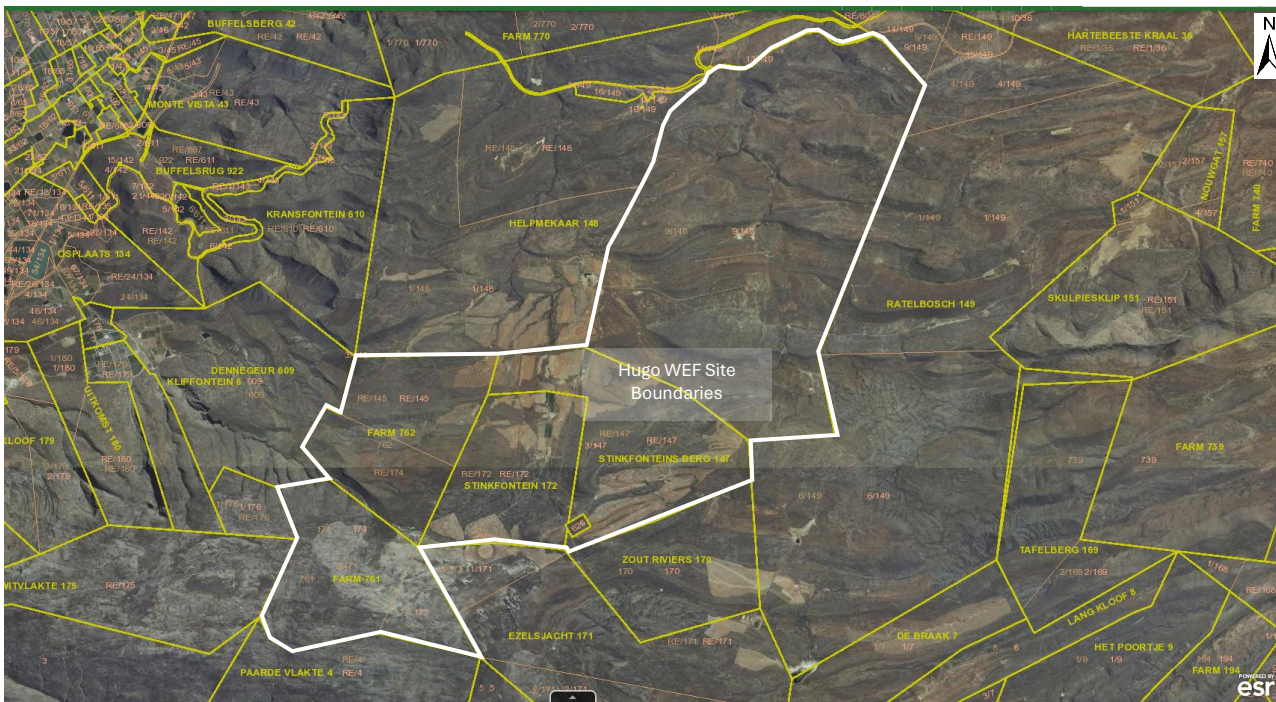


Figure 1-2: Aerial View (Source: <http://csg.drdir.gov.za/>)

Table 1-1: Hugo WEF Land Parcels

Farm Portion (s) Description	Farm No.	Portion (s)
Remainder of the Farm Ou de Kraal No.145	145	RE
Remainder of the Farm Stinkfonteins Berg No. 147	147	
Portion 2 of the Farm Stinkfontein No. 172	172	
Remainder of the Farm Presents Kraal no. 174	174	
Farm Driehoek No. 173	173	0
Portion 9 of the Farm Helpmekaar No.148	148	9

1.2 Objectives

The purpose of this report is to:

- Evaluate the impacts of the proposed development on the existing surrounding road network and associated traffic volumes on the affected roadways;
- Determine the specific traffic needs during the different stages of implementation, namely construction and installation, operations, and decommissioning;
- Evaluate the intersection capacity of the affected existing road network;
- Identify the position and suitability of the preferred access roads for the development;
- Confirm the associated clearances required for the necessary equipment to be transported from the point of delivery to the various implementation sites;
- Confirm freight and transport requirements during initial construction, operation, maintenance and decommissioning phases;
- Propose routes connecting the origins and destinations of site specific equipment;
- Advise on (abnormal load) permit requirements; and
- Reporting.

1.3 Project Overview

The following is a summary of project technical details of the Hugo WEF. Details of the proposed overall layout of the grid connection and associated infrastructure are indicated in Appendix A – Project Description: Hugo.

- Up to 42 Wind Turbine Generators (WTG);
- Hub height (from ground level) up to Maximum 150 m;
- Rotor diameter up to maximum 200 m;
- Blade length up to 100 m;
- Structure height (tip height) up to 250 m;
- On-site substation (OSS) with capacity of 33 kV to 132 kV and inverter transformer stations/substations occupying an area of up to 2.5 ha;
- Operations and maintenance buildings (O&M Building) are up to 1.0 ha with parking area;
- Battery Energy Storage System (BESS) with a footprint area up to 5 ha;
- Laydown area for permanent and construction laydown areas of up to 9 ha;
- Site access will be via the existing R318, and access roads will be constructed or upgraded to provide access to the WEF from new or existing internal roads;
- Internal roads with a width of approximately 4.5 m and a servitude of 13.5 m providing access to the site and between project components; and
- Water supply $\pm 26500\text{m}^3$ for the construction, commissioning, and test phase (± 26 months), the majority being consumed during year-one of the construction with an estimated consumption of $90\text{m}^3/\text{annum}$ for the life-of-WEF (20-25 years).

The general WTG specifications (dimensions) and typical main components are schematically depicted in Figure 1-3 and Figure 1-4, respectively.

The proposed layout of WTG's across respective land parcels is shown in Appendix B – WTG Layout Hugo WEF.

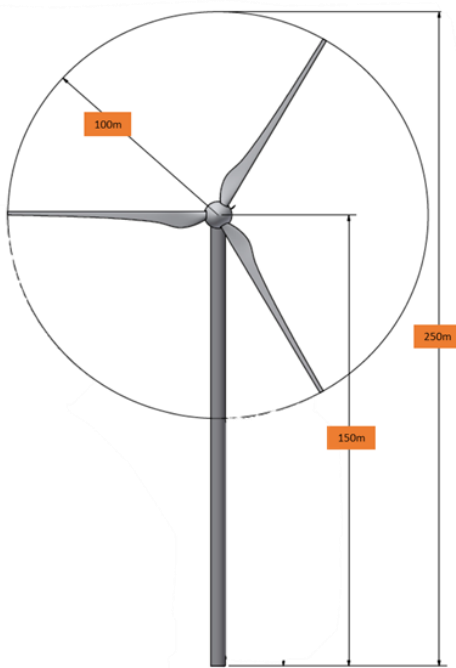


Figure 1-3: Turbine Specifications and Typical Components

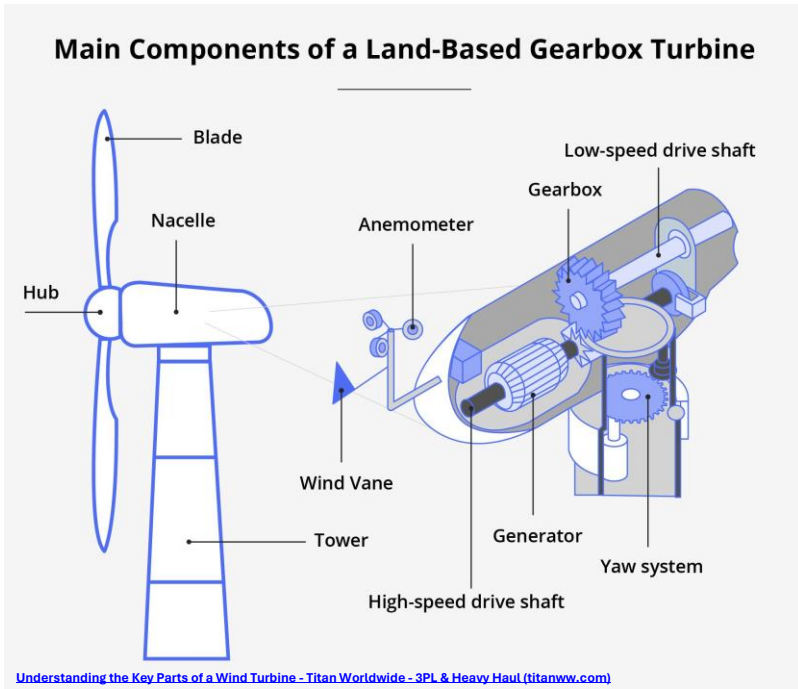


Figure 1-4: Key Parts of a Wind Turbine

Figure 1-5 shows the proposed layout of WTG's and associated infrastructure across respective land parcels for the Hugo WEF (Appendix B – WTG Layout Hugo WEF).

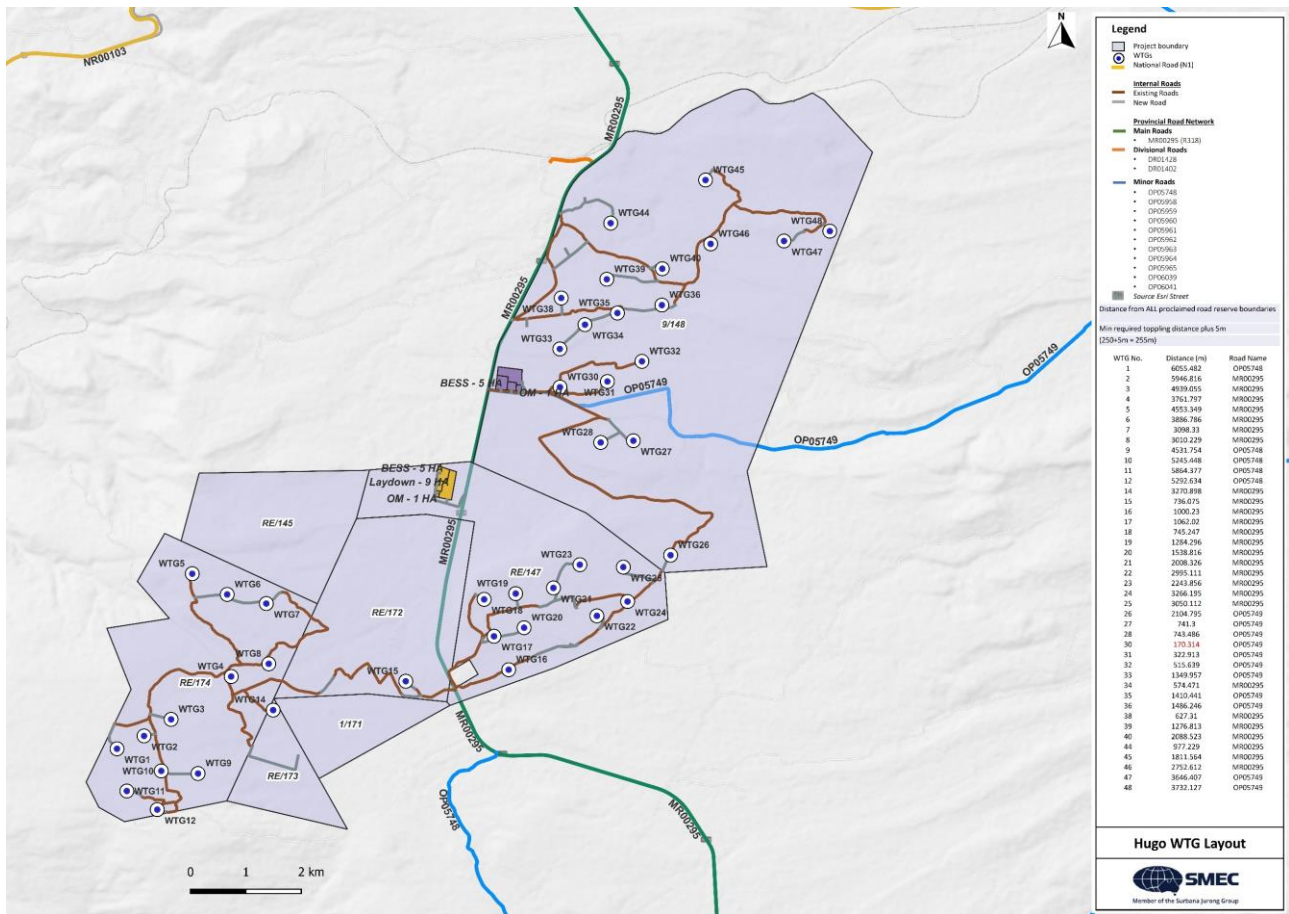


Figure 1-5: Proposed Hugo WEF Layout

1.4 Study Area

The extent of the study area covers key routes and intersections within a 10 km radius near the development on which the expected traffic generated by the development may have a significant impact. Thus, the following intersections were included in the study area:

1. Intersection 1: N1 and R318 (MR00295);
2. Intersection 2: R318 and DR01442 (Road to Matroosbergstasie);
3. Intersection 3: R318 and OP05749 (Road to UITSIG); and
4. Intersection 4: R318 and OP05748 (Road to Middelberg Guest Farm).

The surrounding land use and supporting road network hierarchy are outlined in the following section.

2 Status Quo

2.1 Land Use

The proposed Hugo WEF development site is situated mainly in agricultural land, with some natural and semi-natural vegetation. These activities are expected to continue during the construction, operation, and eventual decommissioning of the sites.

2.2 Surrounding Road Network

2.2.1 Road Hierarchy

The road network in the immediate vicinity of the development site is shown in Figure 2-1. The general location of the sites is made up of farmlands with rural unpaved Class 4 roads supporting movement between the various farms as well as access to some of these land parcels.

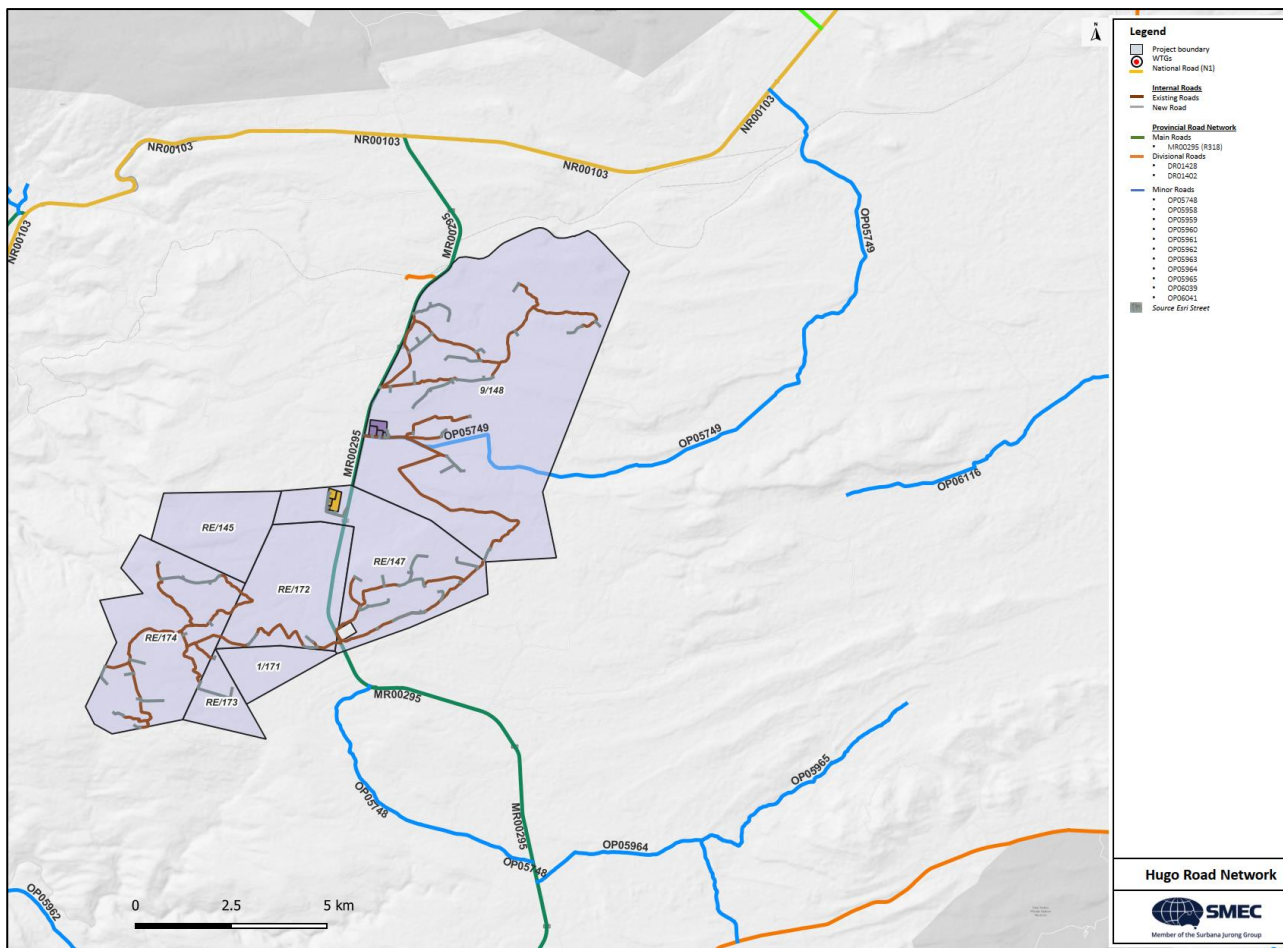


Figure 2-1: Road Network Hierarchy

The hierarchy of the road network in the immediate vicinity of the development site is shown in Appendix C – Existing Surrounding Road Network and summarised below. Additionally, general conditions of existing roads are shown in Appendix C.

- N1:** N1 is a Class 1 National Road that runs from Cape Town through Bloemfontein, Johannesburg, Pretoria, and Polokwane to Beit Bridge on the border with Zimbabwe. The N1 is part of the Trans-African Highway network and forms the Cape to Cairo Road with the N4 and the A1 in Zimbabwe. The N1 is also a scenic route that offers views of the Cape Winelands, the Hex River Valley, the Karoo, the Free State, and the Waterberg.

The traffic flows on the N1 vary according to the time of day, the season, the weather, and the road conditions. The N1 is one of the busiest roads in South Africa, especially in the urban areas of Cape Town, Johannesburg, and Pretoria. The N1 has a speed limit of 120 km/h. The length of N1 in kilometres is 1937 km (Start: Cape Town, End: Beit Bridge Border Post).

- **R318:** R318 is a Class 3 Provincial Main Road (MR00295) that runs in the north-south direction from the N1 near De Doorns through Montagu to R60 near Ashton. The R318 road passes through the Hex River Valley, which is known for its vineyards, fruit farms, and scenic views. The R318 road has a general posted speed limit of 100 km/h and connects to the R62 road, which is a popular tourist route that links Cape Town and Port Elizabeth. The length of R318 in kilometres is 77.4 km (Start: Jct N1 De Doorns, End: Montagu);
- **Road DR01442:** Road DR01442 is a Provincial Divisional Road (gravel road), which is a collector road that provides access to Matroosbergstasie to the west of R318. Road DR01442 has a speed limit of 40 km/h. The length of Road DR01442 in kilometres is 0.8 km (Start: Jct MR295 Matroosberg, End: Matroosberg Station);
- **Road OP05749:** Road OP05749 is a Provincial Minor Road (gravel road) to the east of R318 and connects to the south of the N1 National Route. The length of Road OP05749 in kilometres is 22.74 km (Start: Jct NR1/3 near Grootstraat Far, End: Jct MR295 on Helpmekaar); and
- **Road OP05748:** Road OP05748 is a Provincial Minor Road (gravel road) to the west of R318. The length of Road OP05748 in kilometres is 7.42 km (Start: Jct MR295 on Zout Riviers Berg, End: Property 171 Ezeljagt & 7 De B).

2.2.2 Key Intersections

Key intersections within the study area summarised below in terms of the junction configuration and control. Current conditions of these intersections are indicated in Appendix D – Existing Intersections.

- Intersection 1: N1 (Beaufort west - Worcester) and R318 (Montagu);
 - 4-Way Junction;
 - N1 main road with right of way in the east-west direction;
 - R318 minor side road (south) with a stop control;
 - Private access road (north) with a stop control; and
 - Intersection configuration consists of a single lane in the north-south direction, a single lane in the east approach/exit direction and two lanes in the west approach/exit direction comprising of one full lane and an accommodative 120 m passing lane eastbound.
- Intersection 2: R318 and Road DR01442;
 - T-Junction;
 - R318 main road with right of way in the north-south direction;
 - Road DR01442 Matroosbergstasie minor side road (west) with a yield control; and
 - Intersection configuration consists of a single lane in each direction.
- Intersection 3: R318 and Road OP05749;
 - T-Junction;
 - R318 main road with right of way in the north-south direction;
 - Road OP05749 forms an access-controlled minor side road (east); and
 - Intersection configuration consists of a single lane in each direction.
- Intersection 4: R318 and Road OP05748;
 - T-Junction;
 - R318 main road with right of way in the east-west direction;
 - Road OP05748 forms access-controlled minor side road (west); and

- Intersection configuration consists of a single lane in each direction.

2.3 Data Collection and Traffic Volumes

2.3.1 Current Traffic Volumes

To understand the effects of additional traffic on the road network, an understanding of existing road network traffic conditions is required. Thus 12-hour manual classified traffic counts were conducted at four (4) key intersections which are outlined in Section 2.2 above. These traffic counts were carried on Monday, 15 April 2024 between 06h00-18h00.

The volume of traffic on the Main Road R318 is relatively low compared to traffic volumes along the N1 National Road. Similarly, all other roads (Road DR01442, Road OP05749 and Road OP05748) carry significantly very low levels of traffic volumes compared to both Main Road R318 and the N1 National Road.

Traffic flow diagrams representing the 2024 existing traffic count data (total vehicles) are shown in Appendix J – Traffic Flow Diagrams for the weekday AM peak hour, PM peak hour and 12-hour periods. Observed AM and PM peak hour volumes are summarised in Figure 2-2 below and occurred during the following periods:

- AM peak hour: 10h45 – 11h45; and
- PM peak hour: 16h00 – 17:00.

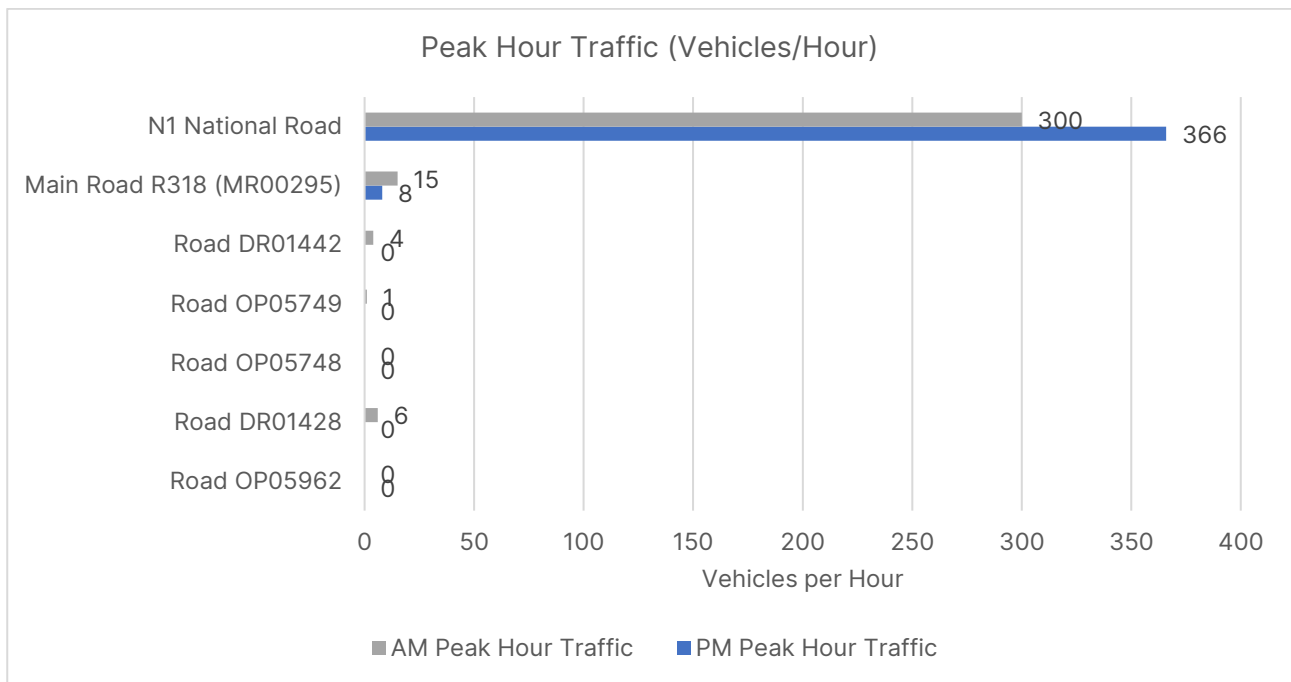


Figure 2-2: Road Network Peak Hour Traffic (vehicles per hour)

N1 National Road: 300 vehicles per hour and 366 vehicles per hour were recorded during the AM peak hour and PM peak hour, respectively, including 56 and 99 heavy vehicles during the respective peak hours.

Main Road R318 (MR00295): 15 vehicles were recorded during the AM peak hour and 8 vehicles were recorded during the PM peak hour. Only 2 heavy vehicles were recorded during the AM peak hours and 0 in the PM peak hour.

Road DR01442: A total of 4 vehicles including heavy vehicles were recorded during the AM peak hour and none during the PM peak hour.

Road OP05749: A single vehicle was recorded in the AM peak hour and none in the PM peak hour.

Road OP05748: There were no vehicles observed during peak periods on Road OP05749.

2.3.2 Provincial Roads and SANRAL Counts

Additional traffic counts data sets sourced from the Western Cape Province’s Road Network Information System and the South African National Roads Agency Limited (SANRAL) were reviewed to develop an understanding of general traffic patterns along the surrounding major road network.

Projected traffic volumes to the current year as obtained from the Road Network Information System estimated an Annual Average Daily Traffic (AADT) of 248 AADT on Main Road R318 and 52 AADT on Divisional Road DR01442 with no record of traffic counting along all Minor Roads, Road OP05749 and Road OP05748.

There were no current year 2024 traffic volume counts from the SANRAL database, however, historical traffic data were only available for year 2019 and prior years and recorded an Average Daily Traffic (ADT) of 3772 to 4815 ADT on the N1 National Road within the vicinity of the site as observed from SANRAL CTO station 18018 and 18017, respectively.

Daily traffic volumes from the above two data sets are included in Appendix F – Provincial Roads and SANRAL Counts and are summarised in Table 2-1 in comparison to the 2024 12-hour surveys. Considering that approximately 30% ADT comprises of night traffic as per SANRAL station data, the short term 12-hour counts provide a reasonable representation of traffic flows within the study area.

Table 2-1: Typical 12-Hour and Daily Traffic Volumes

Road Name	12-Hour Counts (SMEC)	Projected Counts (AADT) (Western Cape Province)	Historical Counts (ADT) (SANRAL)
N1 National Road	3282-3295	N/A	3772-4815
Main Road R318 (MR00295)	124-194	248	N/A
Divisional Road DR01442	21	52	N/A
Minor Road OP05749	2	N/A	N/A
Minor Road OP05748	2	N/A	N/A

N/A – means counts not undertaken by the road authority and/or the authority is not the responsible road authority

2.3.3 Non-Motorised Transport and Public Transport

The roads surrounding the development site can be categorised as rural roads with no provision for non-motorised transport (NMT) and public transport (PT) facilities as the demand is very low. Thus, there are no formalised pedestrian and public transport facilities on the surrounding road network.

The following summary indicates the total number of buses and minibus taxis observed along the N1 National Road and Main Roads R318 (MR00295) during the 12-hour counting period:

- N1 National Road:
 - 32 Buses; and
 - 11 Minibus Taxis.
- Main Road R318 (MR00295):
 - 1 Bus; and
 - 3 Minibus Taxis.

3 Development Layout

3.1 Planning Guidelines

The proposed Hugo WEF development falls outside of an urban area, thus as per the Western Cape Provincial Transport Infrastructure Act, 2023, the following building lines and building restriction areas with respect to provincial roads apply:

- On each side of the road or railway line within a distance of 95 metres from the centre line, measured at right angles to the centre line of the road or railway line; and
- Within a distance of 500 metres from any point of intersection of the centre line of such road.

In addition to the above requirements, the Western Cape Province Roads Authorities have previously imposed/recommended a minimum offset distance (from nearby roads) of tip height of WTG's plus 5 m to guard against toppling failure of WTG structures onto nearby public roads. Thus, the following minimum distances of structure location from the nearest provincial road reserve are preferred:

- 250 m (tip height) + 5 m = 255 m.

The arrangement of the overall project infrastructure is indicated in Appendix G – Building Lines in relation to the above requirements and outlined in the following subsections.

3.2 WTG Layout

None of the WTG structures fall within the 95 m building restriction lines relative to adjacent provincial roads as summarised in Table 3-1.

All WTG structures are located at a distance greater than 500 m from centrelines of intersecting provincial roads as summarised in Table 3-2.

Except for WTG 30 which is located at an offset distance of less 255 m (170 m) from Minor Road OP5749, all other WTG's comply with the recommended offset distance of 255 m from all provincial roads within the project vicinity as summarised in Table 3-2 (See Appendix B).

However, it must be noted that in the event of road closure of Minor Road OP5749 between km 21 and km 22 because of WTG 30 toppling failure over Minor Road OP5749, other areas of site would still be accessible through existing alternative routes/detours within site as shown schematically in Figure 3-1.

Table 3-1: WTG positions relative to adjacent provincial road centre line

Provincial Road	95 m Building Line
Minor Road OP5479	Closest WTG 30 is located +170 m (> 95 m)
Minor Road OP5478	Closest WTG 15 is located +1880 m (> 95 m)

Table 3-2: WTG positions relative to adjacent intersecting centre lines of provincial roads

Intersection of Provincial Roads	500 m Building Line
Main Road R318 (MR00295) and Minor Road OP5479	Closest WTG 30 is located +1270 m (> 500 m)
Main Road R318 (MR00295) and Minor Road OP5478	Closest WTG 15 is located +1500 m (> 500 m)

Table 3-3: WTG positions relative to toppling offset distance from adjacent provincial road reserves

Provincial Road	Structure height (tip height) 250 m + 5 m = 255 m
Minor Road OP5479	Closest WTG 30 is located +170 m (< 255 m)
Minor Road OP5478	Closest WTG 15 is located +1880 m (> 255 m)



Figure 3-1: Alternative Route/Detour

3.3 Associated Infrastructure

The preferred location of the associated WEF facility infrastructure and alternative location of the associated WEF facility infrastructure within the development site has been assessed in relation to their proximities to the centrelines of adjacent provincial roads (Main Road R318 and Minor Road OP5479) and nearest intersecting provincial roads (Intersection of Main Road R318 and Minor Road OP5479).

Appendix H – Standard Plans shows the proposed layout of associated WEF facility infrastructure relative to the surrounding road network.

The preferred location of the associated WEF facility infrastructure relative to Main Road R318 (MR00295) complies fully with the requirements of building lines and building restriction areas, thus satisfying the minimum requirements as indicated in Table 3-4. These WEF infrastructure facilities are located at a distance greater than 230 m (> 95 m) from Main Road R318 and at a greater distance of at least 1580 m (> 500 m) from the intersection of Main Road R318 and Minor Road OP5479.

Table 3-5 shows that the proposed location (footprint) of the alternative associated infrastructure does not fully satisfy the minimum requirements as some areas of the infrastructure are situated within the building lines and building restriction areas.

In this regard the preferred site is therefore recommended for Environmental Authorisation for this development.

Table 3-4: Preferred Associated Infrastructure

Preferred Associated Infrastructure and Extent/Footprint Area (ha)	95 m Building Line (Road)	500 m Building Line (Intersection)
On-Site Substation (OSS): up to 2.5 ha	+430 m > 95 m	+1580 m > 500 m
Operations and Maintenance (O&M building) with parking: up to 1 ha	+455 m > 95 m	+2052 m > 500 m
Battery Energy Storage System (BESS): up to 5 ha	+365 m > 95 m	+1580 m > 500 m
Laydown areas (Permanent and Construction Areas): up to 9 ha	+230 m > 95 m	+1580 m > 500 m

Table 3-5: Alternative Associated Infrastructure

Alternative Associated Infrastructure and Extent/Footprint Area (ha)	95 m Building Line (Road)	500 m Building Line (Intersection)
On-Site Substation (OSS): up to 2.5 ha	+30 m < 95 m	330-520 m
Operations and Maintenance (O&M building) with parking: up to 1 ha	+25 m < 95 m	495-600 m
Battery Energy Storage System (BESS): up to 5 ha	+20 m < 95 m	125-422 m
Laydown areas (Permanent and Construction Areas): up to 9 ha	+135 m > 95 m	300-705 m

4 Access Planning

4.1 Main Access Points

The site location and layout are such that two primary roads potentially provide access to the proposed Hugo WEF development being the N1 National Road and Main Road R318 (MR00295). Thus, the proposed locations of providing main access to the development are from the existing intersections and accesses off Main Road R318 (MR00295).

Positions of 5 proposed accesses to the site off Main Road R318 (MR00295) are shown in Figure 4-1 and comprise mostly of existing private farm accesses with only one new access location being preferred to provide access to the associated WEF facility infrastructure located to the west of Main Road R318 (MR00295).

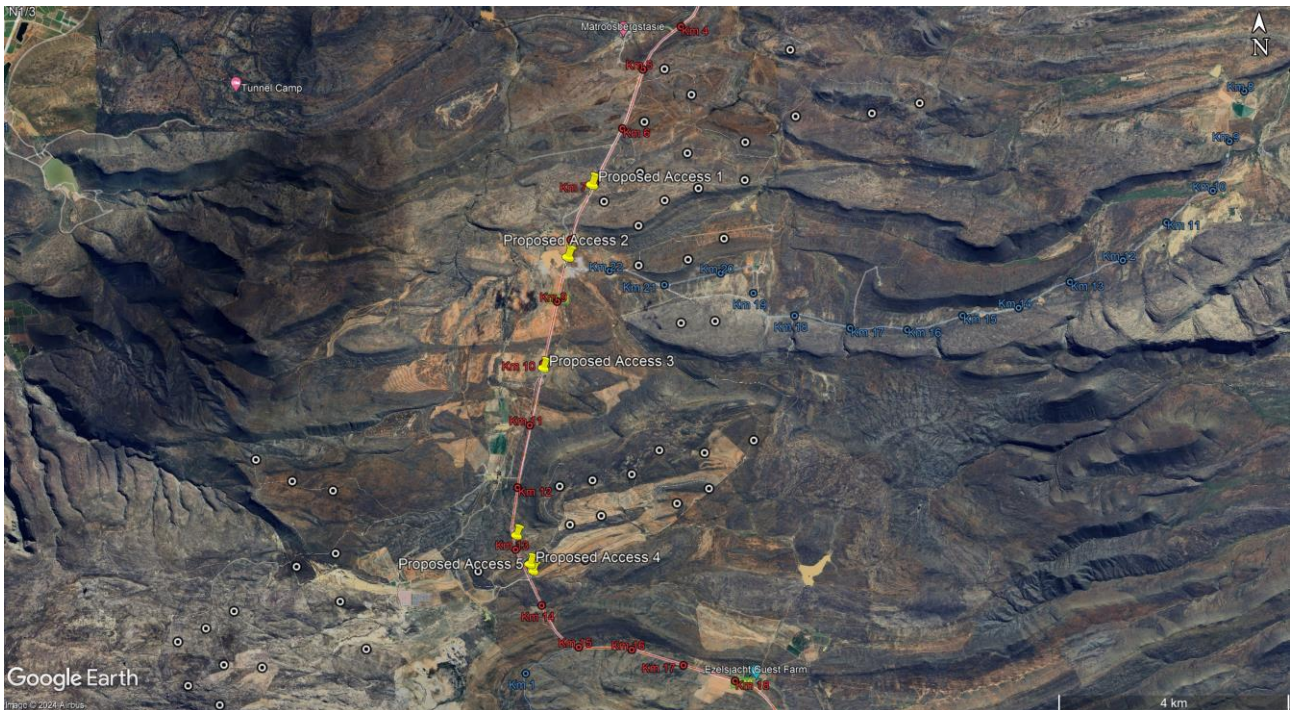


Figure 4-1: Proposed Access Locations (Source: Google Earth Pro)

Proposed site access locations, access spacing, and illustrations of current access conditions are summarised in Table 4-1.

Table 4-1: Existing and Proposed Accesses

Access Location and Access Spacing	Current Access Condition
<p>Proposed Access 1</p> <ul style="list-style-type: none"> Existing farm access but not in use 7.6 km from intersection N1 and R318 3.2 km south of Divisional Road DR01442 East of Main Road R318 Between KM 7 – KM 8 of Main Road R318 1.3 km north of proposed Access 2 	
<p>Proposed Access 2</p> <ul style="list-style-type: none"> Existing farm access At Intersection of Main Road R318 and Minor Road OP5749 East of Main Road R318 Between KM 8 – KM 9 Main Road R318 1.9 km north of proposed Access 3 	
<p>Proposed Access 3</p> <ul style="list-style-type: none"> New access West of Main Road R318 Between KM 10 – KM 11 Main Road R318 3.5 km north of proposed Access 4 	
<p>Proposed Access 4</p> <ul style="list-style-type: none"> Existing farm access East of Main Road R318 Between KM 13 – KM 14 Main Road R318 130 m north of proposed Access 5 	
<p>Proposed Access 5</p> <ul style="list-style-type: none"> Existing farm access West of Main Road R318 Between KM 13 – KM 14 Main Road R318 1.4 km north of Minor Road OP5748 	

Table 4-2: Alternative Associated Infrastructure

Access Spacing	TRH 26 Road Classification and Access Management Manual	Access Management Guidelines, 2020 (Western Cape Provincial Transport Department)
Access 1 to 2	1.3 km < 1.6 km: Noncompliant	1.3 km > 850 m: Compliant
Access 2 to 3	1.9 km > 1.6 km: Compliant	1.9 km > 850 m: Compliant
Access 3 to 4	3.5 km > 1.6 km: Compliant	3.5 km > 850 m: Compliant
Access 4 to 5	0.130 km < 1.6 km: Noncompliant	0.130 km < 850 m: Noncompliant
Access 5 to Road OP5749	1.4 km < 1.6 km: Noncompliant	1.4 km > 850 m: Compliant

In accordance with TRH 26 Road Classification and Access Management Manual guidelines in Table 4-3, two access positions comply with the recommended access spacing of 1.6 km, two are marginally noncompliant while one is noncompliant.

However, four out of five accesses are compliant based on the minimum spacing guidelines as per the Access Guideline Manual, 2020 (Western Cape Provincial Transport) for a Class 3 road with posted speed limit of 100 km/h (See Table 4-4).

Table 4-3: Minimum Spacing Requirements for full intersections on Mobility Roads

Class	Rural	Urban signals(*)	Urban roundabouts and priority(*)
Class 1	8.0 km	n/a	n/a
Class 2	5.0 km	800 m ± 15%	800 m ± 15%
Class 3	1.6 km	600 m ± 20%	600 m ± 20%

(*) These values can be halved for the leg of T-junctions and for one-way streets.

Table 4-4: Minimum spacing distances of driveways/public roads intersecting with through roads in rural roadside development environments

Class of continuous route	Operating speed km/h	Minimum spacing between a public road or driveway and another public road or driveway along a through route						
		Upstream functional distance			Downstream functional distance			Total spacing metres
		Perception-reaction distance metres	Deceleration distance to stop metres	Total upstream distance metres	Acceleration distance from stop metres	Taper distance metres	Total downstream distance metres	
Class 1 & 2	120	65	255	320	940	85	1 025	1 345
Class 3	100	55	205	260	490	70	560	820
Class 4	80	45	115	160	235	55	290	450
Class 5	60	35	65	100	120	40	160	260

4.2 Access Points to Respective WTG sites

Access to WTG sites and other project infrastructure components will be provided via existing internal farm gravel roads and tracks which will be upgraded to roads width of 4.5 m and road servitude of 13.5 m.

4.3 Primary Access Roads and Design Considerations

This section outlines design considerations for the proposed site access roads to the associated infrastructure. Primary site access roads will mainly fulfil the functional classification of a Class 4 & Class 5 Rural Roads.

Reference has been made to the following standards and guidelines for providing access roads, amongst others:

- Road Access Guidelines, Western Cape Provincial Roads Department.
- Draft TRH 20 – Unsealed Roads: Design, Construction and Maintenance.

A detailed route survey must be undertaken to analyze the geometry of internal existing roads and the proposed alignment of new internal routes, in addition to obstacles on the horizontal and vertical alignment with reference to the expected abnormal vehicles and turbine components.

Design considerations outlined in this section are not considered in great details. Thus, detailed design (adapted to the prevailing conditions) of primary access roads and improvements must be completed by the Principal Contractor once appointed and prior to construction. Examples of typical transportation are shown in Table 4-5.

Design Considerations

- **Site access junction improvements**
 - Widening of site access intersections to provide temporary junction overrun areas to accommodate adequate turning radii for anticipated abnormal loads/vehicle sizes.
 - Clearing and grubbing of existing vegetation, removal of obstacles within the visibility junction splay areas to ensure sufficient lines of sight for vehicles using the access.
- **Geometric design (vertical and horizontal alignment)**
 - The maximum permissible longitudinal grade at the centreline of the primary access roads must consider limitations of the equipment which will transport the project components to high-lying areas (i.e., must account for the expected heavy vehicle performance characteristics and weight of turbine components).
 - Cuts and fills will be required to create suitable grades where necessary.
 - Road sections of primary access roads with insufficient turning radii will need to be widened to minimum radius of 60 m.
 - Adequate stopping sight distance for design vehicles - both passenger car and heavy vehicles.
- **Cross drainage and structural design**
 - Road drainage improvements along primary access roads at locations of minor water courses to accommodate construction vehicles during rainy reasons.
 - Provision of low-level structures, concrete drifts, cut-off walls, bridge structures or culverts where required.
 - The design of drainage structures must accommodate the relevant design flood return period.
 - The design of drainage structures must accommodate the load bearing capacity to carry anticipated loads (weight over structures).
- **Pavement design**
 - The pavement structure of must be designed to carry expected traffic loads.
 - Material selection, fractured stone, sand and fine particles with binding characteristics.
- **General**
 - Traffic Management and Safety - Road signage as per the South African Road Traffic Signs Manual and Reduction in vehicle speed
 - Design and Construction Standard Plans as per Western Cape Province, Department of Infrastructure included in Appendix H – Standard Plans.

Table 4-5: Design Vehicles and Expected Infrastructure

 <p>Figure 1.2: Abnormal Load on a Long Wheelbase Trailer</p>  <p>Figure 1.3: Self-Supporting Load on a Steerable Dolly</p>	<p>Guideline: TRH 11 Dimensional and Mass Limitations and Other Requirements for Abnormal Load Vehicles</p>
	<p>Wind turbine components transported on roads in the Eastern Cape</p> <p>Motorists are hereby notified that today , the 19th of February 2024, wind turbine components will be transported as follows:</p> <ol style="list-style-type: none"> At 07:00 3 x abnormal loads (3 x Blades) will be escorted by 6 Traffic vehicles from the Coega Harbour in Gqeberha, via N2 (Nanaga), N10 (Olifantskop Pass) towards Cookhouse. The Olifantskop Pass will be closed for 1 hour when the blades pass through it. At 07:00 3 x abnormal loads (3 x Blades) will be escorted by 6 Traffic vehicles from the Coega Harbour in Gqeberha via Motherwell, through Kariega on the R75 towards Jansenville. We urge all road users to be patient and drive safely. Please expect delays in traffic.
	<p>Wind turbine blades transported through the Olifantskop pass towards Cookhouse</p> <p>On Wednesday, 13 March 2024 at 07:00am, three abnormal loads (Blades) will be escorted by 6 Traffic vehicles from the Koega Harbour in Gqeberha, via N2 (Nanaga), through the Olifantskop pass towards Cookhouse. The Olifantskop Pass will be closed for approximately one hour when the blades pass through it.</p> <p>&</p> <p>Tomorrow Wednesday, 13 March 2024 at 07:00 three abnormal loads (2 x Blades and 1 x Tower) will be escorted by 6 Traffic vehicles from the Koega Harbour in Gqeberha via Motherwell, through Kariega on the R75 towards Jansenville.</p>
	<p>Wind turbine blades transported on roads in the Eastern Cape</p> <p>According to reports several “Wind trucks” are traveling through Graaff-Reinet.They have travelled up from Coega and we assume they are on their way to the three Koruson 1 wind farm sites currently under construction outside Middelburg and Noupoort.</p> <p>Please BE PATIENT AND MOVE OUT OF THEIR WAY!“Turbine blades and other components for the project being transported from Coega port to the Koruson 1 wind farm sites outside Middelburg and Noupoort. The components, which will supply 26 turbines on three windfarms in the area, total 237 blades. Each blade is 81.35m long x 3.8 m high at rotor end x 5.0 m at the widest point, with a weight of 28 tons.”</p>
	<p>Four Nacelles of wind turbines transported on roads in the Eastern Cape</p> <p>Today, the 01st of March 2024 at 07:00, 4 abnormal loads (4 x Nacelles) will be escorted by a convoy of Traffic and routine road maintenance vehicles from the Coega harbour in Gqeberha, via Motherwell, though Kariega (Uitenhage) on the R75 towards Jansenville.</p> <p>(source: https://truckandfreight.co.za/).</p>

4.4 Sight Distance Assessment

To gauge the suitability of the proposed accesses, sight distances were evaluated based on a desktop assessment study using digital elevation modelling (DEM), viewshed analysis, to determine sight distances. Available sight distances are summarised in Table 4-6 with reference to the safe stopping sight distance criteria in Figure 4-2: Shoulder Sight Distance for Stop Condition. The digital elevation model results are shown in Appendix I – Sight Distance Assessment and indicates all points on the main road which are visible from a specific access point.

Sight distances were assessed based on the expected largest vehicle which represents the worst-case scenario. Thus, the primary typical vehicle configuration that was considered is a Single Unit Truck (crossing a road width of 7,5 m) which would access the development mainly during the construction phase through Main Road R318 (MR00295) from stop-controlled minor roads/access roads.

Table 4-6: Sight Distance Assessment

Proposed Access	Posted Speed on R318	Required Sight Distance	Measured Sight Distance (Left)	Measured Sight Distance (Right)	Comply Left	Comply Right
Access 1	100 km/h	380 m	300 m	270 m	N	N
Access 2	100 km/h	380 m	1300 m	850 m	Y	Y
Access 3	100 km/h	380 m	650 m	130 m	Y	N
Access 3 Alternative	100 km/h	380 m	400 m	350 m	Y	N
Access 4	100 km/h	380 m	190 m	120 m	N	N
Access 5	100 km/h	380 m	350 m	150 m	N	N

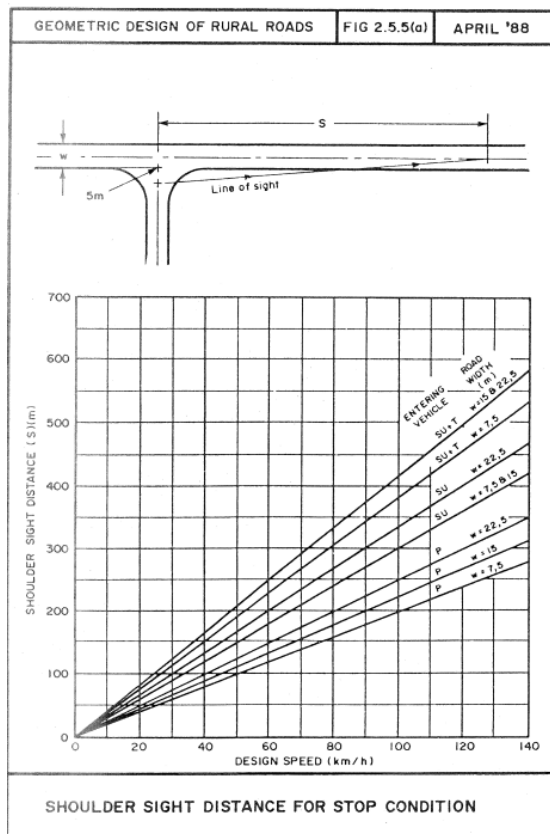


Figure 4-2: Shoulder Sight Distance for Stop Condition

Based on the sight distance assessment, it should be noted the terrain is rolling in nature providing limited opportunities for an access point that meets sight distance requirements in both directions. The vertical profile of the Main Road (MR00295) along the proposed site access consist of a rolling terrain with average gradients in the region of -1% to 7%. In light of the above, it is recommended that the proposed access be approved based on the following points:

1. Heavy vehicles in the form of articulated trucks are only expected during the construction phase of the development. The largest heavy vehicle expected during the operational phase is a single unit truck;
2. The Main Road R318 carries very low traffic volumes in peak hours (less than 20 vehicles) and less than 50 vehicles per day thus demand on the main road will largely comprise of development site traffic;
3. The arrival and departure of construction/ decommissioning vehicles should be staggered during off- peak periods to ensure a reduced impact during low volume traffic periods;
4. The Project Manager and Site Safety Officer should, during construction and decommissioning, ensure correct signage and safety precautions are in place for vehicles and pedestrians on-site and at the site access. These should include temporary regulatory signs such as speed prohibition signs, warning signs (slow moving heavy vehicle, construction vehicle crossing signage) and flagmen, and appoint traffic officials in managing traffic on the access road when abnormal loads are being moved to ensure traffic law enforcement; and
5. Adequate turning radii at access points should be provided to accommodate and allow for the safe turning manoeuvre of the expected articulated vehicles.

4.5 Recommended Alternative On-site Substation Access

Figure 4-3 shows the location of the preferred On-Site Sub-Station which is proposed to the west of Main Road R318 (MR00295). The substation location will also host the proposed Operations and Maintenance office. Further to this, a temporal construction base camp to be set up to host the construction activities including a concrete batching plant is proposed at the same location. The access point to the substation, construction base camp and the Operation and Maintenance building is proposed approximately 1.9 km south of the Main Road R318 and Minor Road OP5748 intersection.

Due to sight distance issues on the right approach at the current access position, it is recommended that access be provided at a position approximately 250 m north of the current proposed access at the existing farm access which is intended to the stopping sight distance and traffic safety. However, the new access position will still achieve a sight distance of 350m, 30 m less than the recommended 380 m. It must be noted that this location will be centrally located providing a clear line of sight from the access point as shown in the viewshed Appendix H – S.



Figure 4-3: Recommended Alternative Access

It is proposed that the recommended alternative access be approved from the traffic and transportation engineering point of view based on the following:

1. There are less than 20 vehicles per direction currently along the Main Road R318;
2. The Sidra analysis results indicated that the intersection will have sufficient capacity during the construction and decommissioning phases of the development without any capacity upgrades required. These phases are anticipated to generate more traffic than the operational phase. To guard against site traffic obstructing through traffic along R318, an exclusive right turn lane as shown in Figure 4-4 is proposed. The right turn lane is proposed to further improve safety at this intersection; and
3. A 60 m acceleration lane provided on the exit side of the north approach is aimed at improving safety at this intersection (See Figure 4-4).

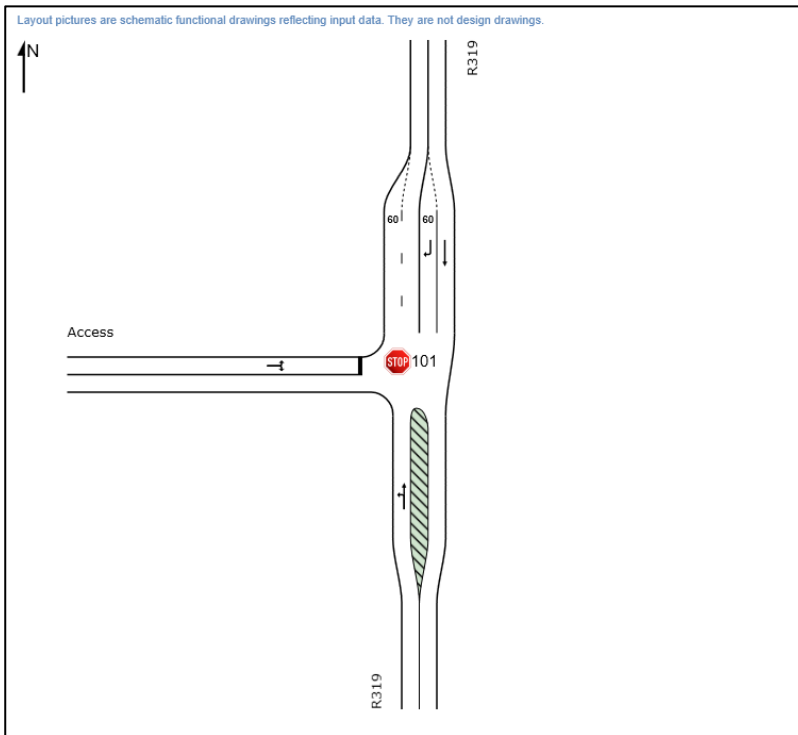


Figure 4-4: Proposed Access Layout

5 Transportation Route

5.1 Port of Entry

It is anticipated that some wind turbine components and equipment, including blades and nacelles, for construction and operation of the WEF will be imported through seaports. There are three seaports in the Western Cape which are operated by Transnet National Ports Authority that could be used for the delivery of turbine components and equipment:

- Port of Cape Town;
- Port of Mossel Bay; and
- Port of Saldanha Bay.

Each seaport has its own advantages and disadvantages, depending on the type, size, and quantity of the equipment, as well as the distance, cost, and availability of the transport services. In considering possible routes to be used to transport abnormal loads, the following factors were considered:

- Avoidance of large cities and towns;
- Distance from the port of entry to the development site;
- Availability of high order roads to be used to haul abnormal loads; and
- Mountain passes which present challenging vertical curve profile and horizontal curve alignment for the expected abnormal heavy vehicles and loads.

It is recommended that a full route determination study should be completed and appropriate approvals from relevant authorities should be obtained before abnormal vehicles are finally routed.

5.1.1 Route Option 1 from Port of Cape Town

This is a 160 km journey route from the Port of Cape Town to site (See Figure 5-1). The greater extent of this route comprises of the N1 National Road which is ideal for hauling abnormal loads as generally National roads are of high quality and many of the structures have been assessed for load bearing capacity and height clearance. However, this route passes through the Huguenot Tunnel and the Hexrivier Pass which may present logistical challenges given the nature of the abnormal loads being transported. The height of the tunnel in comparison to the height of the load as well as other potential constraints the route will have to be assessed at a later stage by a competent professional to be appointed to design the hauling route to be used for abnormal deliveries.

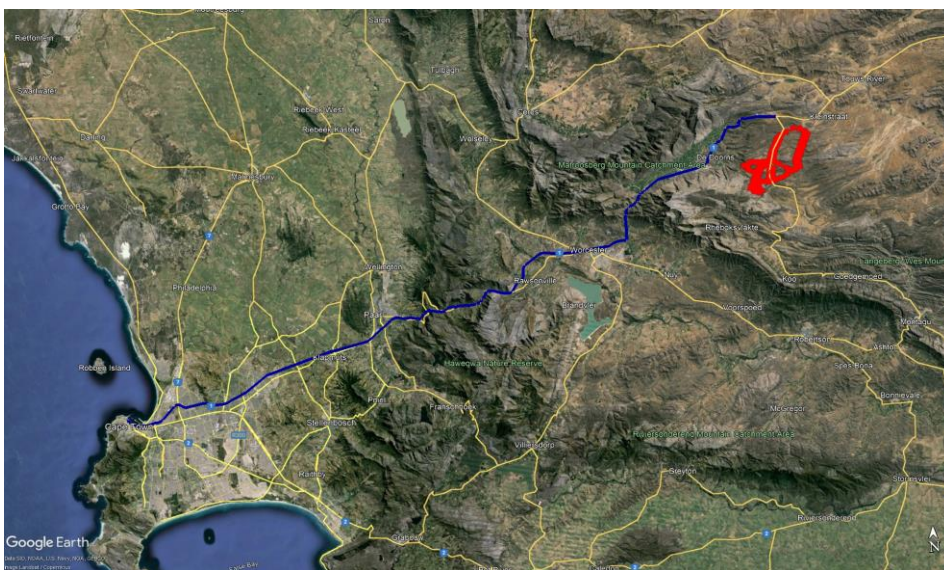


Figure 5-1: Option 1 Route (Source: Google Earth Pro)

The route is narrated as follows:

Follow S Arm Rd and Dock Rd to Nelson Mandela Blvd/N1/N2 (5 min: 1.4 km)

1. Head southwest toward S Arm Rd;
2. Turn left onto S Arm Rd;
3. Turn right to stay on S Arm Rd;
4. At the roundabout, continue straight to stay on S Arm Rd;
5. Continue onto Dock Rd;

Continue to N1 (1 hr 29 min: 132 km)

6. Use the left 3 lanes to turn left onto Nelson Mandela Blvd/N1/N2 (signs for Paarl/Cape Town International Airport/Somerset);
7. Keep left to continue on N1, follow signs for Paarl/Bellville/R27/Milnetron;

Follow N1 to R318 (19 min: 27.7 km)

8. Continue straight to stay on N1;
9. Turn right onto R318;

5.1.2 Route Option 2 from Port of Mossel Bay

This is a 300 km journey route from the Port of Mossel Bay to site. A significant section of this journey comprises of the N2 National Road, with lower class roads such as the R60, R62 and R318. Mossel Bay and Swellendam are the two major towns the route traverses (See Figure 4 2). The suitability of mountain pass found on this route, Burgerspas, Rooihoogstepas, Kogmanskloofpas, will have to be assessed at a later stage by a competent professional to be appointed to design the hauling route to be used for abnormal deliveries.

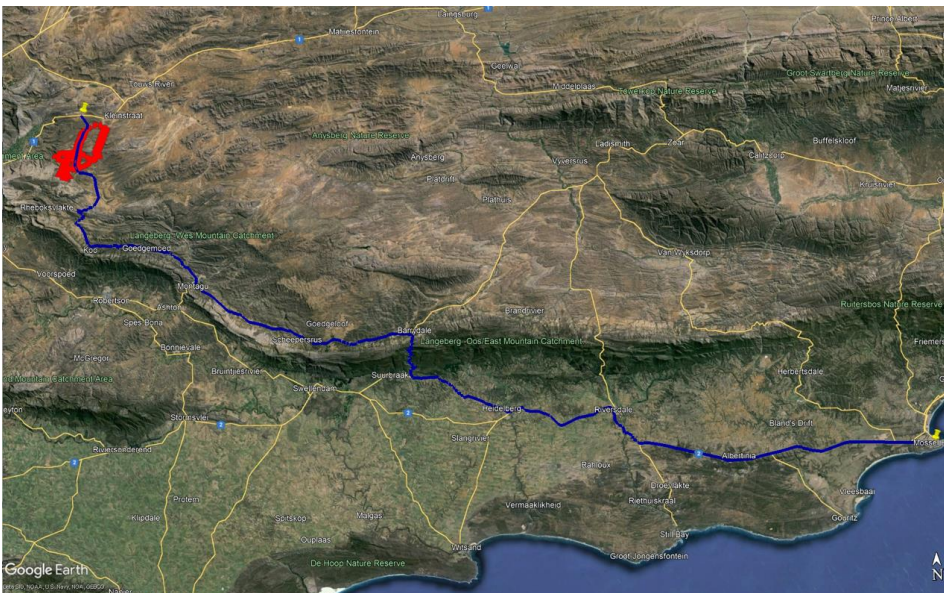


Figure 5-2: Option 2 Route (Source: Google Earth Pro)

The route is narrated as follows:

1. Head west on Louis Fourie Rd/R102 toward Louis Fourie Rd/R102;
2. Continue onto N2;
3. Turn right onto R60;
4. Turn right onto R62;

5. Turn left onto Cross St/R318;
6. Turn right at the 1st cross street onto Bath St/Main Rd/R318;

5.1.3 Route Option 3 from Port of Saldanha Bay

This is a 560 km journey route from the Port of Saldanha Bay to the proposed Hugo WEF site. It comprises of high order and lower order routes through rural towns and farming communities (See Figure 5-3). Several mountain passes namely, Nuwekloofpas, Michell's Pass, Theronsbergpas and Molteno Pass are found along this route. The feasibility of hauling abnormal loads through this route will have to be verified at a later stage by a competent professional to be appointed to develop the transportation solution.

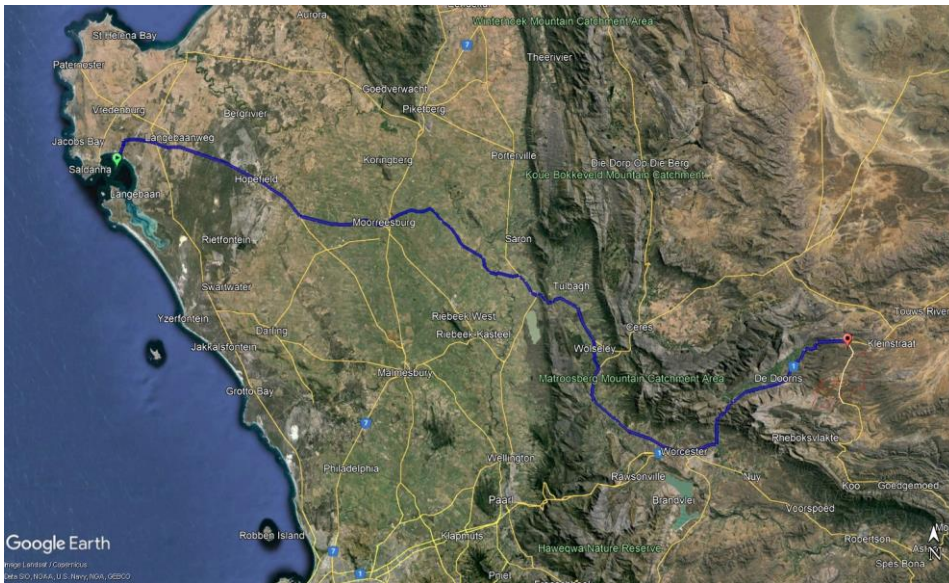


Figure 5-3: Option 3 Route (Source: Google Earth Pro)

The route is narrated as follows:

Take Harbour Rd and Saldanha Rd to Main Rd/R399 (6 min: 2.7 km)

1. Head southeast;
2. Slight left towards Harbour Rd;
3. Turn left onto Harbour Rd;
4. Harbour Rd turns right and becomes Saldanha Rd;

Follow Main Rd/R399 to West Coast Peninsula (5 min: 6.2 km)

5. Continue onto Main Rd/R399;
6. At the roundabout, take the first exit and stay on Main Rd/R399;

Continue to R45 (13 min: 18.7 km)

7. Turn right at Jacobsbaai Rd;
8. Continue onto Saldanha Steel Langebaan;
9. Continue onto TR8501;
10. Continue straight;

Continue on R45 to Moorreesburg (31 min: 53 km)

11. Continue onto R45;
12. Turn left onto R311;

Follow Gouda Rd to R44 (33 min: 40.8 km)

13. Turn left onto Main St;
14. Continue onto Piketberg Rd;
15. Continue straight onto Gouda Rd;

Take R46, R43 and N1 to R318 (1 hr 25 min: 121 km)

16. Turn right onto R44;
17. Turn left onto R4;
18. Turn right onto Voortrekker S;
19. Turn right onto R43;
20. Continue straight to stay on R43;
21. Turn left onto N1/R43;
22. Continue straight to stay on N1;
23. Turn right onto R318;

6 Identification of Transport Impact

6.1 Trip Generation

The trips generated at the Karoo WEF will vary during the different phases of project implementation. Project phases are usually defined as follows:

Pre-construction	Construction	Operational	Decommissioning	Closure
<ul style="list-style-type: none"> •Site survey and preparation 	<ul style="list-style-type: none"> •All construction and installation related activities until contractor leaves the site such as component, equipment and material truck deliveries. 	<ul style="list-style-type: none"> •All activities after construction and installation of WEF, such as operation, maintenance and other services related activities. 	<ul style="list-style-type: none"> •Withdrawal and site rehabilitation 	<ul style="list-style-type: none"> •Closure of site

Figure 6-1: Project Phases

Generally, Wind Energy Facilities generate traffic during three phases or categories, namely:

- Phase 1: Construction Traffic;
- Phase 2: Operation Traffic; and
- Phase 3: Decommission Traffic.

6.1.1 Construction Phase Traffic

The construction phase traffic can be attributed to two aspects, namely:

- Material and equipment delivery; and
- Transportation of labour.

6.1.1.1 Material and Equipment Delivery

Trips generated during the construction phase will primarily comprise of transporting equipment, turbine components, personnel, construction, and other facility materials comprising of normal, heavy, and abnormal load vehicles. It is expected that the construction phase will have the highest traffic impact of all the phases. The following assumptions were made to calculate trips generated during the construction phase.

- It was estimated that the construction period will last approximately 2 years with a 5-day working week resulting in 480 working days over 24 months.
- The Hugo WEF will most likely be constructed from components that will need to be shipped to South Africa via the preferred seaport and be transported to site via road transportation using heavy and abnormal load vehicles. It is also assumed that the turbine component delivery period will be over a course of consecutive 9 months.
- Different abnormal vehicle options, similar to the ones listed in Figure 6-2 to Figure 6-5, as found in the TRH11 (2009), may be selected depending on the logistic service provider used to transport wind turbine components. The remainder of the facility components and construction equipment will use standard transport vehicles and therefore will not require abnormal vehicles.

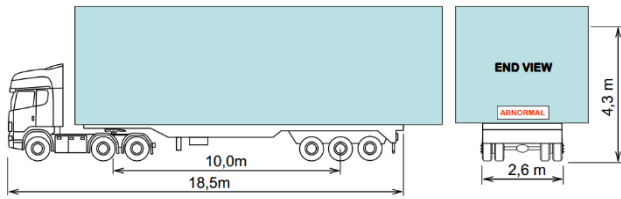


Figure 6-2: Abnormal Load on a Legal Combination

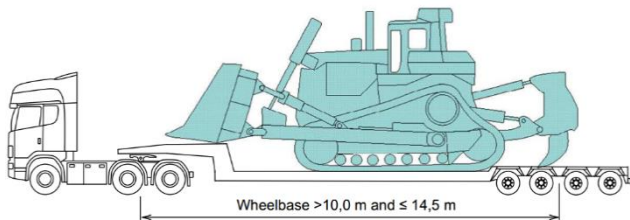


Figure 6-3: Abnormal Load on a Long Wheelbase Trailer

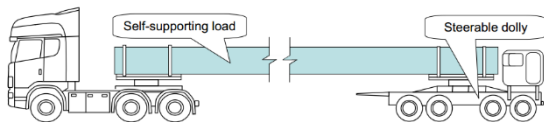


Figure 6-4: Self-Supporting Load on a Steerable Dolly



Figure 6-5: Heavy Loads on Multi-axle or Modular Trailers

- Wind Turbine components and associated details as provided by the client are presented in Table 6-1.

Table 6-1: WEF Components to be transported

Component	Details	Comments and Assumptions
Tower	Length: 150 m	3 Tower sections/WTG Abnormal vehicle required to transport component
Rotor	Blade Length: 100 m	3 Blades/WTG Abnormal vehicle required to transport component
Hub	Weight: Varies 7 to 14 tons	1 Hub Securing 3 Blades/WTG Abnormal vehicle required to transport component
Nacelle	Weight: 68.3 tons	1 Nacelle/WTG Abnormal vehicle required to transport component
WTG Foundation (assumption)	Foundation depth: 5 m Diameter 30 m Volume of concrete: 1885 m ³	Reinforced Concrete Heavy vehicle to transport materials
Crane Platform and	Area: 1 ha (10000m ²)	Levelled and compacted Heavy vehicle to transport materials

Hard Stand Areas		
Electrical Cabling	33 kV Electrical network Underground/ Overhead	Concrete, steel or wood monopoles Guy line supported steel structures Free standing metal lattice towers; or Multi-pole structures such as H-towers or K-towers. Heavy vehicle to transport materials
	132 KV	Lattice Steel Pylons Cables, Connectors and Transformers; and Normal load vehicle to transport
Switching Station	Area: 2.5 ha (25000 m ²)	Transformers Switch gear O&M buildings (1 ha) Control rooms, grid control yards Heavy vehicle to transport materials

- Average “component per turbine” rate of 8 will be used (sum of abnormal components per WTG), therefore over the course of the turbine component delivery period, a maximum of approximately 336 abnormal vehicle loads to construct 42 Wind Turbines, will be delivered to the project site.
- 90 truckloads per Wind Turbine for road layer works will be delivered to the site (3780 truckloads for the project).
- Water for construction purposes (e.g., mass earthworks, dust suppression and roads) will be transferred from the source to the point of use on the site via tanker. Assume that 1 tanker will make two round trips per day (one round trip at the start and one round trip at the start end of the day). Expected water demand: ±26500 m³, Assumption: 14 m³ Capacity (single water tanker truck)
- Some of the aggregate required for the construction of the on-site tracks may be sourced from cut and fill operations within the site with additional material be obtained from borrow pits or imported from quarries as required.
- 30 trips per Wind Turbines for construction, crane vehicles, switching gear and other substation equipment.

6.1.1.2 Transportation of Labour

Another contributor to trips generated to the site will be daily commuters/workers expected during construction. It has been assumed that a total labour force of approximately 360 workers will be required during construction. The majority of the labour force is expected to be sourced from towns in close proximities such as De Doorns, Worcester, Touws River with the remainder coming from other areas such as Montagu.

It is further assumed that approximately 55% of the labour force will be made up of low skilled workers (labourers, security), 30% semi-skilled (professional drivers – drive cars and light duty trucks on site) and 15% skilled personnel (engineers and technicians). The breakdown of the labour is anticipated as shown in Figure 6-6.

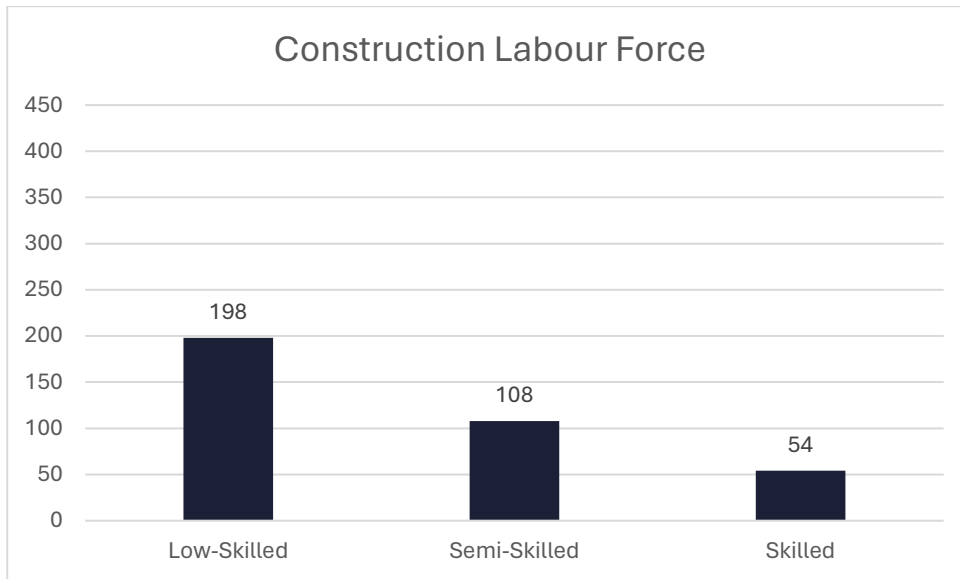


Figure 6-6: Construction Labour Force Breakdown

6.1.1.3 Summary of All Construction Traffic

Based on the above, it was assumed that the skilled labour force will drive to site using cars while a portion (35%) of the semi-skilled group will drive cars and the remaining portion (65%) will use buses to site. The low skilled component of the labour force is expected to be transported to site by bus. The above means that 25% (skilled 100% + 30% semi-skilled) is anticipated to use cars to site and 75% (100% low-skilled + 65% semi-skilled) to be bussed to site. The number of vehicles using a vehicle occupancy factor of 1.2 and 60 for car and bus respectively is expected to be 77 cars and 5 buses during construction. For the purposes of this report, it was assumed that these vehicles will travel during the AM and PM Peak hours and were applied as such during the analysis. A summary of all construction related trip generation trips is shown in Table 6-2.

Table 6-2: Construction Period Trip Generation

Activity	Period (days)	Components	Loads /Turbine	Total 1-way Trips	Daily Trips	Peak Hours Trips	PCU/day
Transportation of WT Components	180	Blade (abnormal)	3	126	1	1	4
		Tower (abnormal)	3	126	1	1	4
		Hub (abnormal)	1	42	1	1	4
		Nacelle (abnormal)	1	42	1	1	4
		Reinforced Concrete works	157	6594	37	18	55
		Road Layer works	90	3780	21	11	33
132 KV Line	180	Cabling and other Pylon Equipment	0	4	4	4	12
Site Work Activities	480	Construction Vehicles & Water Tanker	75	3150	7	3	10
		Crane Transport	2	4	0	0	0

		Labour Transport (Passenger Vehicles)	77	77	154	77	77
		Labour Transport (Bus)	5	5	10	5	15
Total			414	13950	236	122	216

Table 6-2 shows that the total traffic anticipated for the construction phase of the development is a total 122 vehicles per hour. To evaluate capacity requirements, the vehicles were converted to PCU using a factor of 3 car equivalent units for buses and trucks. A car equivalent factor of 4 for abnormal trucks was used. The total number of 216 PCU per day was used as true reflection of the anticipated construction traffic for the development.

6.1.2 Operational Phase Traffic

The operational phase is expected to have comparatively minimal traffic impact as the only transport required will be associated with monitoring, operation, and maintenance. For the operational phase of the wind farm, the following assumptions were made:

- The wind farm will be in operation over a 20-year lifespan.
- Activities on the wind farm include maintenance on an ongoing basis.
- Approximately 42 permanent staff will be working on the site consisting of operational and maintenance technicians, rehabilitation of vegetation, bird and bat post construction monitoring. The labour force will be made up of approximately 15% of skilled, 30% semi-skilled and 55% low skilled. This essentially means 23 of the staff will be low-skilled, 13 semi-skilled and 6 will be fully skilled.
- Skilled staff will likely make use of passenger vehicles and light duty trucks (i.e., Bakkie/4x4) to commute to site daily. Low-skilled and semi-skilled staff are expected to be transported to site by minibus taxis or by bus.
- There will be a possibility for excavations, planned and emergency maintenance, replacement or service of a WT components requiring the use of the above mentioned heavy and abnormal vehicles travelling from nearby areas.
- It is assumed during a maintenance/service or repair event, at least 3 trucks will be expected on site: 1 abnormal vehicle and 2 Heavy vehicles (equipment trucks).

A summary of all operational related trip generation trips is shown in Table 6-3.

Table 6-3: Operation Phase Trip Generation

Activity	Period (Years)	Components	Loads/ Turbine	Total way Trips	Daily	Peak Hours Trips	PCU/day
1 Repair Event	20	Abnormal Truck	1	1	2	1	4
		Trucks	2	2	4	2	6
Daily Operation Activities	20	Labour Transport (Passenger Vehicles)		9	18	9	9
		Minibus		3	6	3	3
Total			3	15	30	15	22

The operational phase of the development is expected to generate approximately 15 vehicles per hour. About 3 of these vehicles are heavy vehicles including an abnormal vehicle. Using a car equivalent factor of 4 for abnormal and 3 for normal trucks, the development will generate approximately 22 Passenger Car Units during the peak hours and were used as such during the analysis.

6.1.3 Decommissioning Phase Traffic

There are three possibilities for the decommissioning phase of the project as listed below.

1. After the 20-year lifespan of the Wind Energy Facility, the need for continued generation of electricity through wind energy is still required and the facility is renovated with new towers on the existing foundation in order to serve another 20 years.
2. The Wind Energy Facility is converted into another alternative renewable energy facility. The specifications around this are unknown.
3. There is no longer an economical / technical basis for an energy plant and the Wind Energy Facility is decommissioned and the land is rehabilitated.

For trip generation purposes, the third possibility was considered as a conservative assumption. Therefore, the relevant assumption made in the construction phase was used here as it will take about 2 years to decommission and rehabilitate the site. About 360 people will be needed with similar transport in the construction phase. All parts will be either reused or recycled and would most likely make their way back to the applicable Port. The decommissioning phase is expected to generate the second highest traffic impact after construction as a result of the need to remove the infrastructure and rehabilitate the site. A summary of all decommissioning trips generated is presented in Table 6-4.

Table 6-4: Decommissioning Trips Generated

Activity	Period (days)	Components	Loads /Turbine	Total 1 way Trips	Daily	Peak Hours Trips	PCU/day
Recycling of WT Components	180	Blade (abnormal)	8	336	4	4	16
Rubble removal and flattening	480	Construction Vehicles & Water Tanker	75	3150	7	3	10
Labour Transport		Labour Transport (Passenger Vehicles)	77	77	154	77	77
		Labour Transport (Bus)	5	5	10	5	15
Total			165	3568	175	89	118

The decommissioning phase of the development is expected to generate approximately 89 vehicles per hour. About 4 of these vehicles are abnormal vehicles. Using a car equivalent factor of 4 for abnormal and 3 for normal trucks, the development will generate approximately 118 Passenger Car Units during the peak hours and were used as such during the analysis.

6.2 Trip Distribution

The trip distribution and assignment of the development trips is shown in Figure J2 to Figure J8 in Appendix J – Traffic Flow Diagrams.

6.3 Traffic Analysis Results

6.3.1 Background

It is required to grow background traffic flow to an acceptable horizon year to ensure that the future road network would be able to operate adequately. In the absence of historical data, the COTO, TMH17 Volume 1 Manual provides typical growth rates to be used for growth areas based on the existing/anticipated rate of growth. Typical traffic growth rates are illustrated in Table 6-5.

Table 6-5: Typical Traffic Growth Rates

Development Area	Growth Rate
Low Growth Areas	0% - 3%
Average Growth Areas	3% - 4%
Above Average Growth Areas	4% - 6%
Fast Growing Areas	6% - 8%
Exceptionally High Growth Areas	> 8%

The site area was considered to be a low growth area. Taking into account the additional WEF being developed in the area, a 3% per annum growth rate was assumed to represent the expected traffic growth for the short to medium term (2022 to 2027). A low 1% per annum was used to forecast the traffic long term (2027 to 2042) in order to investigate capacity requirements for the decommissioning phase. This is due to unknowns on the long-term prospects of the area. Further to this, it is not advisable to project over 20 years without detailed land use information informed by the SDF and the SDP of the wider area. It is therefore proposed that a detailed traffic impact study for the decommissioning phase be undertaken prior to the decommissioning stage commencing. To identify any shortcomings in the road-based capacity, the following scenarios were analysed:

1. Existing 2024 AM and PM Peak hour Traffic;
2. Existing 2024 + Construction Phase AM and PM Peak hour Traffic;
3. Background 2029 + Operation Phase AM and PM Peak hour Traffic; and
4. Horizon 2046 + Decommissioning Phase AM and PM Peak hour Traffic.

6.3.2 Intersection Capacity Operation Analysis

The operational performance of an intersection is defined by the level of service (LOS) for each approach to the intersection. These definitions, as defined in the Highway Capacity Manual (HCM) (Reference 5), relate average delays at intersections for individual turning movements, for each approach and for the overall intersection to a Level of Service (LoS) ranging from A to F, as shown in Table 6-6.

Table 6-6: Intersection Capacity Based Level of Service Criteria

Level of Service	Control Delay per Vehicle in Seconds (d)	
	Signals and Roundabouts	Stop Signs and Yield Signs
A	$d \leq 10$	$d \leq 10$
B	$10 < d \leq 20$	$10 < d \leq 15$
C	$20 < d \leq 35$	$15 < d \leq 25$
D	$35 < d \leq 55$	$25 < d \leq 35$
E	$55 < d \leq 80$	$35 < d \leq 50$
F	$80 < d$	$50 < d$

During the peak hours, the road infrastructure capacity provided should ensure that the intersection approach level of service should ideally not exceed LOS D. Because the site is located in a rural part of the country, the acceptable LOS for Rural class 1-2 roads is LOS B on normal days and LOS C on abnormal days.

It should be noted that overall Intersection LOS and Major Road Approach LOS values are not applicable for two-way priority/stop control since the average delay is not a good LOS measure due to zero delays associated with major road movements, however, results will give an indication of delay and LOS for the minor road approaching the major road.

Intersection capacity analysis results for all scenarios are outlined in the following subsections.

6.3.2.1 Scenario 1: Existing 2024 AM and PM Peak hour Traffic

The traffic volumes representing this scenario are included in Figure J1, Appendix J. All intersections are currently operating at acceptable level of service (LOS A). Capacity analysis results for this scenario are summarised in Table 6-7.

Table 6-7: 2024 Existing AM and PM Peak Hour Results

Intersection		AM Peak Hour				PM Peak Hour			
Name	Approach	Demand (veh/h)	V/C (ratio)	Delay (sec)	LOS	Demand (veh/h)	V/C (ratio)	Delay (sec)	LOS
Intersection 1: R318 and N1	South	7	0.011	10.1	B	3	0.005	10.6	B
	East	93	0.058	0.3	A	254	0.137	0.1	A
	North	3	0.004	7.2	A	3	0.004	7.4	A
	West	222	0.086	0.2	A	136	0.0068	0.3	A
	Overall	325	0.086	0.5	A	396	0.137	0.3	A
Intersection 2: R318 and DR01442 (Access to Matroosbergstasie)	South	6	0.003	0.9	A	2	0.001	2.8	A
	North	5	0.003	1.1	A	7	0.004	0.8	A
	West	5	0.003	5.5	A	2	0.001	5.5	A
	Overall	17	0.003	2.4	A	12	0.004	2	A
Intersection 3: R318 and OP05749 (Nadini Access road)	South	5	0.003	1.1	A	4	0.002	1.4	A
	East	2	0.001	5.5	A	2	0.001	5.5	A
	North	4	0.002	1.4	A	7	0.004	0.8	A
	Overall	12	0.003	2	A	14	0.004	1.7	A
Intersection 4: R318 and OP05748 access road to Middelberg	South	5	0.003	1.1	A	4	0.003	1.4	A
	North	5	0.003	1.1	A	7	0.004	0.8	A
	West	2	0.001	5.5	A	2	0.001	5.5	A
	Overall	13	0.003	1.8	A	14	0.004	1.7	A

6.3.2.2 Scenario 2: Existing 2024 + Construction Phase AM and PM Peak hour Traffic

The traffic volumes representing this scenario are included in Figure J6, Appendix J. All intersections are currently operating at acceptable level of service (LOS A). Capacity analysis results for this scenario are summarised in Table 6-8.

Table 6-8: 2024 Existing + Construction Phase AM and PM Peak Hour Results

Intersection		AM Peak Hour				PM Peak Hour			
Name	Approach	Demand (veh/h)	V/C (ratio)	Delay (sec)	LOS	Demand (veh/h)	V/C (ratio)	Delay (sec)	LOS
Intersection 1: R318 and N1	South	96	0.138	10.4	B	93	0.155	11.5	B
	East	133	0.083	2.1	A	286	0.163	1.0	A
	North	3	0.005	10.7	B	3	0.006	13.0	B
	West	272	0.115	1.6	A	190	0.098	2.6	A
	Overall	504	0.138	3.5	A	572	0.163	3.3	A
Intersection 2: R318 and DR01442 (Access to Matroosbergstasie)	South	97	0.059	0.1	A	97	0.052	0.1	A
	North	114	0.072	0.1	A	114	0.062	0.1	A
	West	5	0.004	5.9	A	5	0.004	5.9	A
	Overall	216	0.072	0.2	A	216	0.062	0.2	A
Intersection 3: R318 and OP05749 (Nadini Access road)	South	96	0.058	0.1	A	95	0.060	0.1	A
	East	2	0.002	6.1	A	2	0.002	6.0	A
	North	111	0.070	0.1	A	113	0.062	0.1	A
	Overall	209	0.070	0.1	A	178	0.063	0.1	A
Access: Proposed Associated infrastructure	South	13	0.007	3.8	A	10	0.006	5.0	A
	North	111	0.066	5.3	A	112	0.066	5.4	A
	West	100	0.076	8.0	A	100	0.069	5.6	A
	Overall	224	0.076	6.4	A	238	0.069	5.5	A
Intersection 4: R318 and OP05748 access road to Middelberg	South	14	0.009	0.4	A	13	0.008	0.4	A
	North	14	0.009	0.4	A	16	0.009	0.3	A
	West	2	0.001	5.6	A	2	0.001	5.6	A
	Overall	30	0.009	0.7	A	178	0.009	0.7	A

6.3.2.3 Scenario 3: Existing 2029 + Operation Phase AM and PM Peak hour Traffic

The traffic volumes representing this scenario are included in Figure J7, Appendix J. All intersections are currently operating at acceptable level of service (LOS A). Capacity analysis results for this scenario are summarised in Table 6-9.

Table 6-9: 2029 Background + Construction Phase AM and PM Peak Hour Results

Intersection		AM Peak Hour				PM Peak Hour			
Name	Approach	Demand (veh/h)	V/C (ratio)	Delay (sec)	LOS	Demand (veh/h)	V/C (ratio)	Delay (sec)	LOS
Intersection 1: R318 and N1	South	15	0.024	10.5	B	13	0.022	11.2	B
	East	106	0.069	0.6	A	284	0.162	0.2	A
	North	3	0.005	11.8	B	3	0.005	12.7	B
	West	249	0.102	0.3	A	154	0.162	0.5	A
	Overall	373	0.102	0.9	A	454	0.162	0.7	A
Intersection 2: R318 and DR01442 (Access to Matroosbergstasie)	South	16	0.010	0.3	A	11	0.007	0.5	A
	North	17	0.011	0.3	A	17	0.009	0.3	A
	West	6	0.004	5.6	A	2	0.001	5.6	A
	Overall	39	0.011	1.1	A	30	0.009	0.7	A
Intersection 3: R318 and OP05749 (Nadini Access road)	South	14	0.009	0.4	A	13	0.008	0.4	A
	East	2	0.001	5.6	A	2	0.001	5.6	A
	North	13	0.007	0.4	A	17	0.009	0.3	A
	Overall	29	0.009	0.8	A	32	0.009	0.7	A
Access: Proposed Associated infrastructure	South	7	0.004	1.6	A	5	0.003	2.2	A
	North	14	0.008	3.5	A	16	0.009	3.1	A
	West	11	0.008	7.9	A	11	0.008	7.9	A
	Overall	32	0.008	4.6	A	23	0.009	4.6	A
Intersection 4: R318 and OP05748 access road to Middelberg	South	8	0.005	0.7	A	7	0.004	1.8	A
	North	8	0.005	0.7	A	10	0.005	1.8	A
	West	2	0.001	5.5	A	2	0.001	5.5	A
	Overall	18	0.005	1.2	A	19	0.005	1.2	A

6.3.2.4 Scenario 4: Horizon 2046 + Decommission Phase AM and PM Peak hour Traffic

The traffic volumes representing this scenario are included in Figure J8, Appendix J. All intersections are currently operating at acceptable level of service (LOS A). Capacity analysis results for this scenario are summarised in Table 6-10.

Table 6-10: 2046 Background + Decommission Phase AM and PM Peak Hour Results

Intersection		AM Peak Hour				PM Peak Hour			
Name	Approach	Demand (veh/h)	V/C (ratio)	Delay (sec)	LOS	Demand (veh/h)	V/C (ratio)	Delay (sec)	LOS
Intersection 1: R318 and N1	South	50	0.085	11.3	B	45	0.189	12.7	B
	East	141	0.091	1.1	A	330	0.188	0.1	A
	North	3	0.006	13.0	B	3	0.007	14.2	B
	West	327	0.006	1.0	A	214	0.111	1.7	A
	Overall	521	0.136	2.1	A	592	0.188	1.7	A
Intersection 2: R318 and DR01442 (Access to Matroosbergstasie)	South	50	0.031	0.1	A	44	0.024	0.1	A
	North	67	0.045	0.1	A	67	0.036	0.1	A
	West	6	0.004	5.7	A	2	0.002	5.7	A
	Overall	123	0.045	0.4	A	113	0.036	0.2	A
Intersection 3: R318 and OP05749 (Nadini Access road)	South	48	0.031	0.1	A	47	0.031	0.1	A
	East	2	0.002	5.8	A	2	0.002	5.8	A
	North	63	0.043	0.1	A	63	0.034	0.1	A
	Overall	113	0.043	0.2	A	112	0.034	0.2	A
Access: Proposed Associated infrastructure	South	10	0.006	5	A	14	0.006	5	A
	North	81	0.048	5.4	A	81	0.048	5.4	A
	West	73	0.049	5.6	A	73	0.049	5.6	A
	Overall	164	0.049	5.5	A	164	0.049	5.5	A
Intersection 4: R318 and OP05748 access road to Middelberg	South	16	0.010	0.3	A	14	0.008	0.4	A
	North	16	0.010	0.3	A	18	0.010	0.3	A
	West	2	0.001	5.6	A	2	0.001	5.6	A
	Overall	34	0.010	0.7	A	34	0.010	0.7	A

7 Transport Management Plan

The section discusses traffic management techniques, vehicle requirements, and stakeholder collaboration for the construction and operation of wind energy facilities. Temporary signage, speed limits, road closures, diversions, and traffic signals are all addressed. Road authorities, municipalities, police, emergency services, communities, landowners, contractors, and suppliers are among the key stakeholders to be engaged.

7.1 Abnormal Weights and Dimension

7.1.1 Evaluation of Abnormal Weights and Dimensions

Transport requirements for the Wind Energy Facility project will require the use of abnormal load vehicles as stipulated in TRH 11, especially in the construction phase of the project for the delivery of construction materials and turbine components. Very little to no special transport will be required during the remainder of the development phases, as conventional transport will be used.

All wind turbine components are considered to be abnormal loads, either through length, weight, or height, usually comprising of 3 tower sections, 1 hub, 1 nacelle, and 3 blades. These require different truck and trailer combinations and configurations to be transported. These issues will be investigated at a later stage when the transporting contractor and the plant hire companies apply for the necessary permits from the permit-issuing authorities. The heaviest component of a wind turbine is the nacelle (approximately 67 to 85 tons, depending on the manufacturer and design of the unit). Combined with road-based transport, it has a total vehicle mass of approximately 130 000 kg (for the 85-ton unit). Route clearances and permits will be required for transporting the nacelle by road-based transport.

Blades are the longest component at 100m and need to be transported on a specially imported extendible blade transport trailer or in a rigid container with rear steerable dollies. The blades can be transported individually, in pairs, or in threes, although different manufacturers have different methods of packaging and transporting the blades. Where required, existing public roads may need to be upgraded along the proposed equipment transport route to allow for the transportation and delivery of wind turbine components and other associated infrastructure components. The national roads on the potential national access routes are generally of high standard, and many of the structures have been assessed for load-bearing capacity and height clearance in the past. The turbine supplier or contractors selected for implementation would be responsible for the transportation of wind turbine components to the site. A complete transportation management plan should be undertaken prior to construction, should the project be awarded preferred bidder status.

7.1.2 Permit Requirements

In the transportation of loads, the following guidelines are available: According to TRH 11, the expected load dimensions are classified as abnormal loads; therefore, an exemption permit for each province where the load has to transit is required. Provision for the type of abnormal loads in this development is made in the National Road Transport Act (NRTA), and specifically in Section 81 of the NRTA, which reads as follows:

“Vehicle and load may be exempted from provisions of Act

An MEC may, subject to such conditions as upon payment of such fees or charges as he or she may determine, authorise in writing, either generally or specifically, the operation on a public road of a vehicle which does not comply with the provisions of this Act or the conveyance on a public road of passengers or any load otherwise that in accordance with the provisions of this Act.”

When the movement of an abnormal load is considered to be in the country's economic and/or social interest, an exemption permit may be provided to allow a vehicle(s) conveying such an abnormal load to operate on a public road for a limited time. The essential principles that will guide this procedure are as follows:

- An exemption permit for an abnormal load will only be considered for an indivisible load, abnormal in dimension and/or mass, where there is no possibility of transporting the load in a legal manner;

- The risks to other users must be reduced to a level equivalent to what it would be without the presence of the abnormal vehicle on the road; and
- The conditions imposed must take the economic and/or social interest of the country and public at large into account.

7.1.3 Types of Abnormalities

The Wind Energy Facility is anticipated to carry loads that are considered to be indivisible and can be abnormal either dimensionally, abnormal in mass, or abnormal both dimensionally and in mass. The following is the legally permissible maximum dimension or mass.

Length: Truck and Semi-Trailer (Tri-Axle) Overall length of combination (including load projections) - 18.50 m
 Superlink (6 m + 12 m trailers) Overall length of combination (no load projections)- 22.00 m.

Width: 2.60 m

Height: 4.30 m measured from the ground. The height of a conventional trailer is 1.60 m from the ground to the trailer deck; therefore, the permissible height of the load is 2.70 m.

Weight: 13.50 m Tri-Axle 28 Ton/15.00 m Tri-Axle 30 Ton Superlink 34 Ton Gross (6.00 m–10/12 Ton & 12 m–24/22 Ton)

The Wind Energy Facility components are classified as abnormal loads and will necessitate an application to the Department of Transport and Public Works for a permit authorizing the conveyance of said load. With the required permits in place, the following escort vehicles (whether they are the client's own escort vehicles or provincial traffic officers) will be necessary to escort the transportation of abnormal loads. The anticipated escort vehicles are presented in Table 7-1.

It must be noted Loads with a height of 4.70 m measured from the ground require –1 x Own Escort vehicle. For loads of 5.50 m + high Telkom & Eskom Clearances are required for the lifting of overhead lines. Upon final selection of wind turbine models to be used, the exact amount of escort vehicles can be determined.

Table 7-1: Escort Vehicles

Component	Details	Escort Vehicles
Tower	Length: 150 m	3 Tower sections/WT 2 x Provincial Traffic Escorts (subject to width of load)
Rotor	Blade Length: 100 m Hub	Blades/WT Connected to 1 Hub/WT 2 x Provincial Traffic Escorts (subject to width of load)

7.2 Impact on Road Users

There is potential for the transportation of components and construction materials to have an impact on the general traffic and local community. The presence of the heavy vehicles required during the construction and decommissioning phase may also cause noise and dust impacts which impact local residence located close to the Wind Energy Facility site. These impacts may be minimised by:

- Scheduling abnormal and heavy vehicle transport by proper distribution of arrivals and departure to avoid high numbers of vehicles arriving at once;
- Additional traffic management control measures at site accesses to limit impact, i.e., signage; and
- Traffic accommodation during any upgrades on access points, i.e., Stop-go system. An example of a Stop-go operation is presented in Figure 7-1.

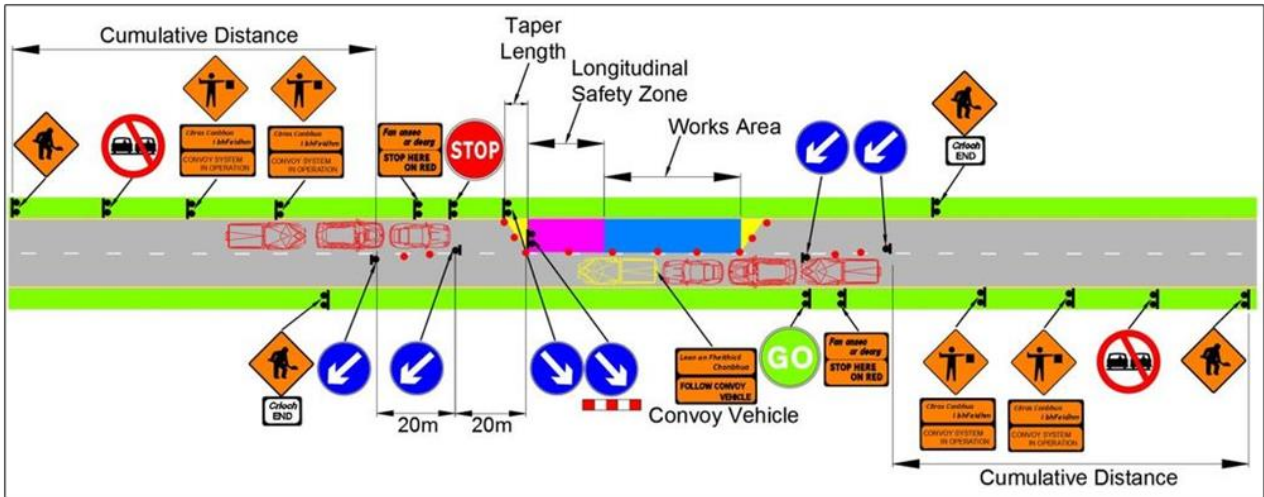


Figure 7-1: Stop-Go Operation (Source: Temporary Traffic Management Design Guidance)

8 Traffic Impact Ratings

This section describes the impact assessment methodology used to assess the anticipated traffic and transportation related impacts. The impact assessment methodology which was used in this assessment was developed by ERM – Environmental Resources Management and involves a 7-step approach for determining the significance of potential impacts in accordance with the requirements of Appendix 3 of the EIA Regulations, 2014 (as amended).

The overall approach in calculating the impact score starts with the identification and prediction of an impact whereby impact criteria such as the extent (E), duration (D), magnitude (M), reversibility (R), probability (P) of the identified impact (nature (N)), are rated from a scale of 1 to 5 based on degree of occurrence and factored to calculate the significance (S) of each impact. Detailed description of the rating (1-5) definition and impact criteria are provided in Appendix K – Impact Assessment Methodology. The associated significance (S) score of the impact is then determined by the following mathematical relationship:

- $S = (E+D+M+R) * P.$

Furthermore, other factors, including cumulative impacts and potential for irreplaceable loss of resources are considered. The overall signification (S) ranging from 1 through to 100 is categorised as follows:

- 0 – 30: Low (i.e., where this impact is unlikely to be a significant environmental risk);
- 31 - 60: Moderate (i.e., where the impact could have a significant environmental risk); and
- 61 - 100: High (i.e., where the impact will have a significant environmental risk resulting in substantial deterioration or exceeding recommended levels).

The significance of environmental impact is calculated for each impact prior and post mitigation measures to assess the effectiveness of impact management plans. In addition, the assessment is undertaken for each development phase i.e., construction, operation, and decommissioning.

Table 8-1 provides a high-level summary of the impact criteria and assessment methodology.

Table 8-1: ERM Impact Assessment Methodology

Impact Criteria	Significance	Final Score					
Extent (E)	Significance = (E+D+M+R) * P	Significance is deemed Negative (-)			Significance is deemed Positive (+)		
Duration (D)		0 - 30	31 - 60	61 - 100	0 - 30	31 - 60	61 - 100
Magnitude (M)		Low	Moderate	High	Low	Moderate	High
Reversibility (R)							
Probability (P)							
Status (S)	Negative (-) or Positive (+) or Neutral						
Nature (N)	Name of Impact						

8.1 Assumptions and Limitations

The assessment has been prepared based on the information provided by the Client and the following assumptions, amongst others:

- It was assumed that the construction period will last approximately 2 years with a 5-day working week resulting in 480 working days over 24 months.
- Construction trips were estimated without a detailed construction schedule programme.
- For the assessment of cumulative impacts, a conservative approach was adopted by assuming that all wind energy facilities within 30 km currently approved, planned or proposed would be constructed concurrently.

- WTG components will be imported and transported with abnormal vehicles from the most feasible port of entry/harbour.
- Haulage will occur on surfaced national and provincial roads and existing site access gravel roads.
- Construction material and labour force will be sourced locally.

8.1.1 Impact Significance for Construction Phase

The construction phase is expected to generate the highest number of vehicles over the construction period of approximately 2 years.

Table 8-2 to Table 8-5 indicate the identified nature of impact and impact significance associated with the construction phase.

Table 8-2: Impact Summary Table for Construction Phase – Increased General Traffic

Impact Phase: Construction					
Nature of the impact: Increase in general peak hour traffic volumes					
<p>Description of Impact: Increased traffic on the route and access points to site - Potential to be greater than what the existing road capacity of the local road network can handle in order to operate at an acceptable level of service.</p> <p>This impact relates to potential disruption of traffic on local, regional and national roads. The severity of the impacts will depend on the order of the road (how many lanes, lanes width, length, turns, etc.), the receiving environment and vicinity of land uses and towns.</p> <p>Additional traffic on the road network could result in changes to the operations of that road network, intersection capacity, such as increased congestion, delays, and accidents.</p>					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Regional	Short Term	Recoverable	Low	Probable
Score	3	2	3	2	3
With Mitigation	Local	Short Term	Reversible	Very Low	Probable
Score	2	2	1	1	3
Significance Calculation	Without Mitigation		With Mitigation		
S=(E+D+R+M)*P	Low Negative Impact (30)		Low Negative Impact (18)		
Was public comment received?	YES/NO. If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/NO, if NO then WHY? If YES then HOW/WHERE				
<p>Mitigation measures to reduce residual risk or enhance opportunities:</p> <p><i>Implementation of the Traffic Management Plan and Road Safety Measures</i></p> <p><i>Limit use of private cars</i></p> <p><i>Schedule development traffic movements to not coincide with existing peaks where possible</i></p> <p><i>Encourage use of public/staff transportation</i></p>					
Residual impact	Negative, moderate and temporary				

Table 8-3: Impact Summary Table for Construction Phase – Abnormal Heavy Traffic

Impact Phase: Construction					
Nature of the impact: Increase in abnormal traffic volumes					
<p>Description of Impact: Additional heavy vehicles/E80's/Abnormal vehicles on the external road network- Potential to require additional road rehabilitation.</p> <p>The impact of abnormal loads on public roads is expected to cause journey time delays and traffic congestion due to low travelling speeds of heavy vehicles transporting abnormal loads. These often occupy two standard traffic lanes and can potentially lead to incidents when travelling on single carriageways with a single lane per direction and without traffic police escorts.</p>					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	National	Short Term	Recoverable	High	Probable
Score	4	2	3	4	3
With Mitigation	National	Short Term	Recoverable	Moderate	Probable
Score	4	2	3	3	3
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Moderate Negative Impact (39)			Moderate Negative Impact (36)	
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
<p>Mitigation measures to reduce residual risk or enhance opportunities:</p> <p><i>Implementation of the Traffic Management Plan and Road Safety Measures</i></p> <p><i>Compliance to permissible heavy vehicle dimensions, permissible axle mass load on vehicles (no overloading)</i></p> <p><i>Transportation scheduling to consider the time of day when the abnormal loads would be moved</i></p> <p><i>Other alternative modes of transportation (rail where feasible) should be considered</i></p>					
Residual impact	Negative, moderate and temporary				

Table 8-4: Impact Summary Table for Construction Phase – Dust Generation

Impact Phase: Construction					
Nature of the impact: Impact of dust along gravel site access roads					
Description of Impact: Heavy vehicles are expected to cause dust along unpaved access roads to the site. This can affect the air quality and visibility for nearby residents and road users. Larger vehicles generate more dust which can limit the ability of other vehicles to overtake due to poor visibility.					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Site	Immediate	Recoverable	Moderate	Probable
Score	1	1	3	3	3
With Mitigation	Site	Immediate	Reversible	Low	Low Probability
Score	1	1	1	2	2
Significance Calculation	Without Mitigation		With Mitigation		
S=(E+D+R+M)*P	Low Negative Impact (24)		Low Negative Impact (14)		
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
Mitigation measures to reduce residual risk or enhance opportunities: <i>Dust control measures such as regular wet grading and wetting for dust suppression to minimize the negative impact</i>					
Residual impact	Yes, but acceptable.				

Table 8-5: Impact Summary Table for Construction Phase – Deterioration of Surrounding Road Network

Impact Phase: Construction					
Nature of the impact: Deterioration of surrounding road network					
<p>Description of Impact: Heavy vehicle traffic during construction of the development is expected to cause additional wear and tear on the surrounding road network. Gravel access roads to the sites are also expected to sustain damage during the construction phase of the project.</p> <p>Abnormal loads can exert more pressure on road surfaces and infrastructure, leading to increased maintenance costs and reduced road network lifespan.</p>					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Local	Short Term	Recoverable	Moderate	Probable
Score	2	2	3	3	3
With Mitigation	Site	Immediate	Reversible	Low	Low Probability
Score	1	1	1	2	2
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Low Negative Impact (30)			Low Negative Impact (10)	
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
<p>Mitigation measures to reduce residual risk or enhance opportunities:</p> <p><i>Limiting the number and frequency of heavy and overloaded vehicles where possible</i></p> <p><i>Undertaking regular maintenance, rehabilitation and upgrading substandard pavement conditions</i></p>					
Residual impact	<i>Positive, roads will remain in better conditions post implementation of mitigation measures</i>				

8.1.2 Impact Significance for Operation Phase

The operational phase of the development is expected to generate the least number of vehicles over the project lifespan of approximately 20 years.

Thus, the operational phase is expected to have comparatively minimal environmental impact as only the transport required will be associated with monitoring, operation, and maintenance.

Table 8-6 to Table 8-9 indicate the identified nature of impact and impact significance associated with the operational phase.

Table 8-6: Impact Summary Table for Operational Phase – Increased General Traffic

Impact Phase: Operation					
Nature of the impact: Increase in general peak hour traffic volumes					
Description of Impact: Increased traffic on the route and access points to site - Potential to be greater than what the existing road capacity of the local road network can handle in order to operate at an acceptable level of service.					
This impact relates to potential disruption of traffic on local, regional and national roads. The severity of the impacts will depend on the order of the road (how many lanes, lanes width, length, turns, etc.), the receiving environment and vicinity of land uses and towns.					
Additional traffic on the road network could result in changes to the operations of that road network, intersection capacity, such as increased congestion, delays, and accidents.					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Site	Immediate	Reversible	Very Low	Low Probability
Score	1	1	1	1	2
With Mitigation	Site	Immediate	Reversible	Very Low	Low Probability
Score	1	1	1	1	2
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Low Negative Impact (8)			Low Negative Impact (8)	
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
Mitigation measures to reduce residual risk or enhance opportunities: <i>Implementation of the Traffic Management Plan and Road Safety Measures</i> <i>Limit use of private cars</i> <i>Schedule development traffic movements to not coincide with existing peaks where possible</i> <i>Encourage use of public/staff transportation</i>					
Residual impact	<i>Moderate and temporary</i>				

Table 8-7: Impact Summary Table for Operational Phase – Abnormal Heavy Traffic

Impact Phase: Operation					
Nature of the impact: Increase in abnormal traffic volumes					
Description of Impact: Additional heavy vehicles/E80's/Abnormal vehicles on the external road network- Potential to require additional road rehabilitation.					
<p>The impact of abnormal loads on public roads is expected to cause journey time delays and traffic congestion due to low travelling speeds of heavy vehicles transporting abnormal loads. These often occupy two standard traffic lanes and can potentially lead to incidents when travelling on single carriageways with a single lane per direction and without traffic police escorts.</p>					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Regional	Immediate	Recoverable	Moderate	Probable
Score	3	1	3	3	3
With Mitigation	Regional	Immediate	Recoverable	Moderate	Low Probability
Score	3	1	3	3	2
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Low Negative Impact (30)			Low Negative Impact (20)	
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
<p>Mitigation measures to reduce residual risk or enhance opportunities: <i>Implementation of the Traffic Management Plan and Road Safety Measures</i> <i>Compliance to permissible heavy vehicle dimensions, permissible axle mass load on vehicles (no overloading)</i> <i>Transportation scheduling to consider the time of day when the abnormal loads would be moved</i> <i>Other alternative modes of transportation (rail where feasible) should be considered</i></p>					
Residual impact	Negative, moderate and temporary				

Table 8-8: Impact Summary Table for Operational Phase – Dust Generation

Impact Phase: Operation					
Nature of the impact: Impact of dust along gravel site access roads					
Description of Impact: Heavy vehicles are expected to cause dust along unpaved access roads to the site. This can affect the air quality and visibility for nearby residents and road users. Larger vehicles generate more dust which can limit the ability of other vehicles to overtake due to poor visibility.					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Site	Immediate	Recoverable	Low	Low Probability
Score	1	1	3	2	2
With Mitigation	Site	Immediate	Reversible	Very Low	Improbable
Score	1	1	1	1	1
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Low Negative Impact (10)			Low Negative Impact (4)	
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
Mitigation measures to reduce residual risk or enhance opportunities: <i>Dust control measures such as regular wet grading and wetting for dust suppression to minimize the negative impact</i>					
Residual impact	<i>Negligible</i>				

Table 8-9: Impact Summary Table for Operational Phase – Deterioration of Surrounding Road Network

Impact Phase: Operation					
Nature of the impact: Deterioration of surrounding road network					
<p>Description of Impact: Heavy vehicle traffic during construction of the development is expected to cause additional wear and tear on the surrounding road network. Gravel access roads to the sites are also expected to sustain damage during the construction phase of the project.</p> <p>Abnormal loads can exert more pressure on road surfaces and infrastructure, leading to increased maintenance costs and reduced road network lifespan.</p>					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Site	Immediate	Reversible	Low	Low Probability
Score	1	1	1	1	2
With Mitigation	Site	Immediate	Reversible	Low	Low Probability
Score	1	1	1	1	2
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Low Negative Impact (8)			Low Negative Impact (8)	
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
<p>Mitigation measures to reduce residual risk or enhance opportunities:</p> <p><i>Limiting the number and frequency of heavy and overloaded vehicles where possible</i></p> <p><i>Undertaking regular maintenance, rehabilitation and upgrading substandard pavement conditions</i></p>					
Residual impact	<i>Positive, roads will remain in better conditions post implementation of mitigation measures</i>				

8.1.3 Impact Significance for Decommissioning Phase

It is expected that the decommissioning phase will have similar transport requirements in the construction phase. Thus, the decommissioning phases will generate the second highest traffic impact after construction as a result of the need to remove infrastructure and rehabilitate the site.

Table 8-10 to Table 8-13 indicate the identified nature of impact and impact significance associated with the decommission phase.

Table 8-10: Impact Summary Table for Decommission Phase – Increased General Traffic

Impact Phase: Decommission					
Nature of the impact: Increase in general peak hour traffic volumes					
<p>Description of Impact: Increased traffic on the route and access points to site - Potential to be greater than what the existing road capacity of the local road network can handle in order to operate at an acceptable level of service.</p> <p>This impact relates to potential disruption of traffic on local, regional and national roads. The severity of the impacts will depend on the order of the road (how many lanes, lanes width, length, turns, etc.), the receiving environment and vicinity of land uses and towns.</p> <p>Additional traffic on the road network could result in changes to the operations of that road network, intersection capacity, such as increased congestion, delays, and accidents.</p>					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Regional	Short Term	Recoverable	Low	Probable
Score	3	2	3	2	3
With Mitigation	Local	Short Term	Reversible	Very Low	Probable
Score	2	2	1	1	3
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Low Negative Impact (30)			Low Negative Impact (18)	
Was public comment received?	YES/NO. If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/NO, if NO then WHY? If YES then HOW/WHERE				
<p>Mitigation measures to reduce residual risk or enhance opportunities:</p> <p><i>Implementation of the Traffic Management Plan and Road Safety Measures</i></p> <p><i>Limit use of private cars</i></p> <p><i>Schedule development traffic movements to not coincide with existing peaks where possible</i></p> <p><i>Encourage use of public/staff transportation</i></p>					
Residual impact	Negative, moderate and temporary				

Table 8-11: Impact Summary Table for Decommission Phase – Abnormal Heavy Traffic

Impact Phase: Decommission					
Nature of the impact: Increase in abnormal traffic volumes					
<p>Description of Impact: Additional heavy vehicles/E80's/Abnormal vehicles on the external road network- Potential to require additional road rehabilitation.</p> <p>The impact of abnormal loads on public roads is expected to cause journey time delays and traffic congestion due to low travelling speeds of heavy vehicles transporting abnormal loads. These often occupy two standard traffic lanes and can potentially lead to incidents when travelling on single carriageways with a single lane per direction and without traffic police escorts.</p>					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	National	Short Term	Recoverable	High	Probable
Score	4	2	3	4	3
With Mitigation	National	Short Term	Recoverable	Moderate	Probable
Score	4	2	3	3	3
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Moderate Negative Impact (39)			Moderate Negative Impact (36)	
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
<p>Mitigation measures to reduce residual risk or enhance opportunities:</p> <p><i>Implementation of the Traffic Management Plan and Road Safety Measures</i></p> <p><i>Compliance to permissible heavy vehicle dimensions, permissible axle mass load on vehicles (no overloading)</i></p> <p><i>Transportation scheduling to consider the time of day when the abnormal loads would be moved</i></p> <p><i>Other alternative modes of transportation (rail where feasible) should be considered</i></p>					
Residual impact	Negative, moderate and temporary				

Table 8-12: Impact Summary Table for Decommission Phase – Dust Generation

Impact Phase: Decommission					
Nature of the impact: Impact of dust along gravel site access roads					
Description of Impact: Heavy vehicles are expected to cause dust along unpaved access roads to the site. This can affect the air quality and visibility for nearby residents and road users. Larger vehicles generate more dust which can limit the ability of other vehicles to overtake due to poor visibility.					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Site	Immediate	Recoverable	Moderate	Probable
Score	1	1	3	3	3
With Mitigation	Site	Immediate	Reversible	Low	Low Probability
Score	1	1	1	2	2
Significance Calculation	Without Mitigation		With Mitigation		
S=(E+D+R+M)*P	Low Negative Impact (24)		Low Negative Impact (14)		
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
Mitigation measures to reduce residual risk or enhance opportunities: <i>Dust control measures such as regular wet grading and wetting for dust suppression to minimize the negative impact</i>					
Residual impact	Yes, but acceptable.				

Table 8-13: Impact Summary Table for Decommission Phase – Deterioration of Surrounding Road Network

Impact Phase: Decommission					
Nature of the impact: Deterioration of surrounding road network					
<p>Description of Impact: Heavy vehicle traffic during construction of the development is expected to cause additional wear and tear on the surrounding road network. Gravel access roads to the sites are also expected to sustain damage during the construction phase of the project.</p> <p>Abnormal loads can exert more pressure on road surfaces and infrastructure, leading to increased maintenance costs and reduced road network lifespan.</p>					
Impact Status: Negative					
	E	D	R	M	P
Without Mitigation	Local	Short Term	Recoverable	Moderate	Probable
Score	2	2	3	3	3
With Mitigation	Site	Immediate	Reversible	Low	Low Probability
Score	1	1	1	2	2
Significance Calculation	Without Mitigation			With Mitigation	
S=(E+D+R+M)*P	Low Negative Impact (30)			Low Negative Impact (10)	
Was public comment received?	YES/ NO . If yes, provide a bullet summary of main concerns.				
Has public comment been included in mitigation measures?	YES/ NO , if NO then WHY? If YES then HOW/WHERE				
<p>Mitigation measures to reduce residual risk or enhance opportunities:</p> <p><i>Limiting the number and frequency of heavy and overloaded vehicles where possible</i></p> <p><i>Undertaking regular maintenance, rehabilitation and upgrading substandard pavement conditions</i></p>					
Residual impact	<i>Positive, roads will remain in better conditions post implementation of mitigation measures</i>				

8.2 Assessment of Cumulative Development Impacts

As per the NEMA EIA Reg GN R982 of 2014, in relation to an activity, cumulative impact means “the past, current and reasonably foreseeable future impact of an activity, considered together with the impact of activities associated with that activity, that in itself may not be significant, but may be significant when added to the existing and reasonably foreseeable impacts eventuating from similar or diverse activities”.

Table 8-14 and Figure 8-1 indicate wind and solar developments with an approved Environmental Authorisation or applications under consideration and proposed developments within 30 km of the proposed area. Cumulative impacts of these are assessed in the following subsections.

Table 8-14: Wind and Solar developments with an approved Environmental Authorisation or Application

No.	EIA Reference No	Classification	Status of Application	Distance from proposed area (km)
1	14/12/16/3/3/2/810	Solar PV	Approved	20.5
2	12/12/20/2210	Solar PV	Approved	23.9
3	12/12/20/2019	Solar PV	Approved	26.2
4	12/12/20/2210/AM 2	Solar PV	Approved	23.9
5	12/12/20/1956	Solar PV	Approved	16.4
6	N/A	Solar PV	Proposed	9.5
7	N/A	Wind	Proposed	13.5

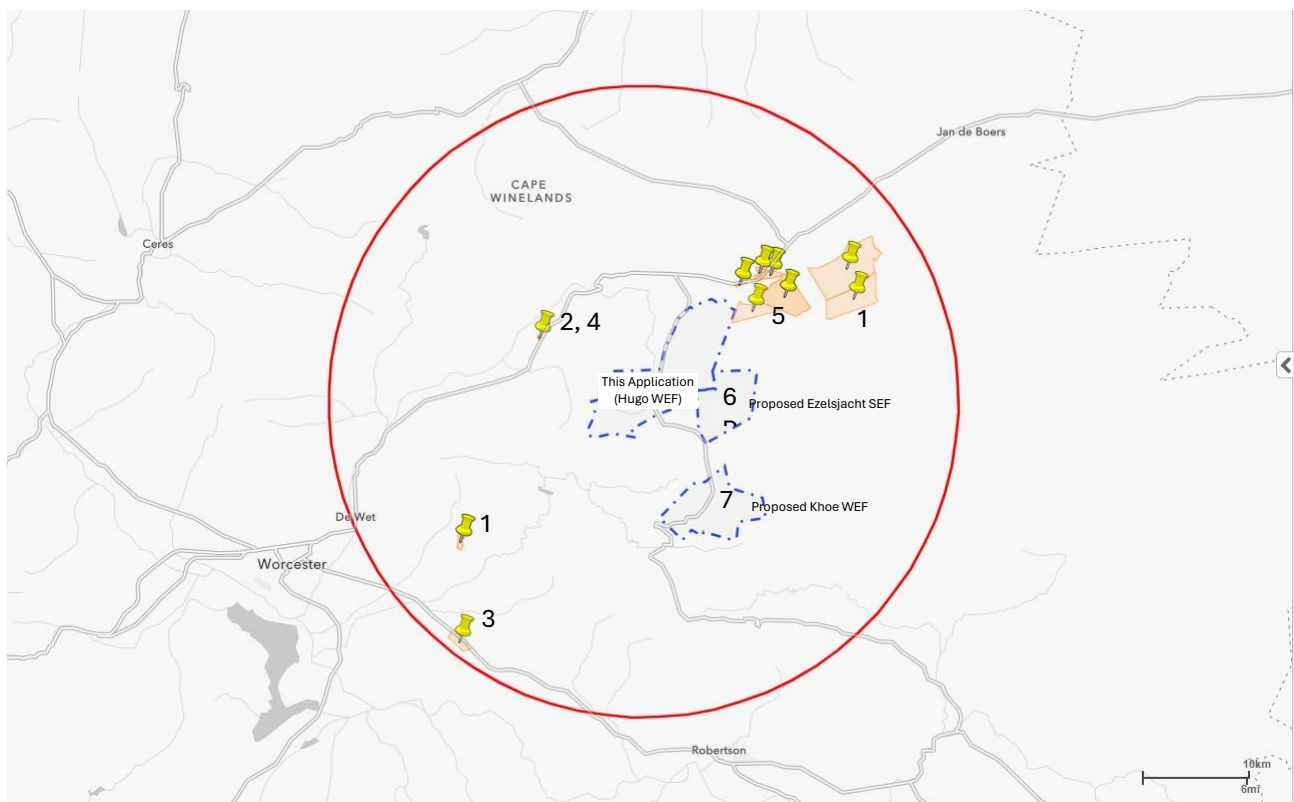


Figure 8-1: Wind and Solar developments with an approved Environmental Authorisation or Applications under consideration within 30 km of the proposed area

Table 8-15: Cumulative Impact – Increased General Traffic

Cumulative Impact: Increase in general peak hour traffic volumes					
<p>Description of Cumulative Impact: Increased traffic on the route and access points to site - Potential to be greater than what the existing road capacity of the local road network can handle in order to operate at an acceptable level of service.</p> <p>This impact relates to potential disruption of traffic on local, regional and national roads. The severity of the impacts will depend on the order of the road (how many lanes, lanes width, length, turns, etc.), the receiving environment and vicinity of land uses and towns.</p> <p>Additional traffic on the road network could result in changes to the operations of that road network, intersection capacity, such as increased congestion, delays, and accidents.</p>					
Impact Status: Detail of the impact is Positive, Neutral or Negative					
	E	D	R	M	P
Without Enhancement	Regional	Short Term	Recoverable	Probable	Probable
Score	3	2	3	3	3
With Enhancement	Local	Short Term	Recoverable	Probable	Probable
Score	2	2	3	3	3
Significance Calculation	Without Enhancement			With Enhancement	
S=(E+D+R+M)*P	Moderate Negative Impact (33)			Low Negative Impact (30)	
Can Impacts be Enhanced?	YES/NO and HOW/WHY				
<p>Enhancement:</p> <p><i>Implementation of the Traffic Management Plan and Road Safety Measures</i></p> <p><i>Limit use of private cars</i></p> <p><i>Schedule development traffic movements to not coincide with existing peaks where possible</i></p> <p><i>Encourage use of public/staff transportation</i></p>					
Residual impact	<i>Negative to Significant</i>				

Table 8-16: Cumulative Impact – Abnormal Heavy Traffic

Cumulative Impact: Increase in abnormal traffic volumes					
Description of Cumulative Impact: Additional heavy vehicles/E80's/Abnormal vehicles on the external road network- Potential to require additional road rehabilitation.					
The impact of abnormal loads on public roads is expected to cause journey time delays and traffic congestion due to low travelling speeds of heavy vehicles transporting abnormal loads. These often occupy two standard traffic lanes and can potentially lead to incidents when travelling on single carriageways with a single lane per direction and without traffic police escorts.					
Impact Status: Detail of the impact is Positive, Neutral or Negative					
	E	D	R	M	P
Without Enhancement	Regional	Short Term	Recoverable	High	Highly Probable
Score	4	2	3	4	4
With Enhancement	Regional	Short Term	Recoverable	Probable	Probable
Score	3	2	3	3	3
Significance Calculation	Without Enhancement		With Enhancement		
S=(E+D+R+M)*P	Moderate Negative Impact (39)		Moderate Negative Impact (33)		
Can Impacts be Enhanced?	YES/NO and HOW/WHY				
Enhancement: <i>Implementation of the Traffic Management Plan and Road Safety Measures</i> <i>Compliance to permissible heavy vehicle dimensions, permissible axle mass load on vehicles (no overloading)</i> <i>Transportation scheduling to consider the time of day when the abnormal loads would be moved</i> <i>Other alternative modes of transportation (rail where feasible) should be considered</i>					
Residual impact	Negative to Very Significant				

Table 8-17: Cumulative Impact – Dust

Cumulative Impact: Impact of dust along gravel site access roads					
Description of Cumulative Impact: Heavy vehicles are expected to cause dust along unpaved access roads to the site. This can affect the air quality and visibility for nearby residents and road users. Larger vehicles generate more dust which can limit the ability of other vehicles to overtake due to poor visibility.					
Impact Status: Detail of the impact is Positive, Neutral or Negative					
	E	D	R	M	P
Without Enhancement	Site	Immediate	Recoverable	Moderate	Probable
Score	1	1	3	3	3
With Enhancement	Site	Immediate	Recoverable	Low	Low Probability
Score	1	1	1	2	2
Significance Calculation	Without Enhancement			With Enhancement	
S=(E+D+R+M)*P	Low Negative Impact (24)			Low Negative Impact (10)	
Can Impacts be Enhanced?	YES/NO and HOW/WHY				
Enhancement: <i>Dust control measures such as regular wet grading and wetting for dust suppression to minimize the negative impact</i>					
Residual impact	<i>Negligible</i>				

Table 8-18: Cumulative Impact – Deterioration of surrounding road network

Cumulative Impact: Deterioration of surrounding road network					
Description of Cumulative Impact: Heavy vehicle traffic during construction of the development is expected to cause additional wear and tear on the surrounding road network. Gravel access roads to the sites are also expected to sustain damage during the construction phase of the project. Abnormal loads can exert more pressure on road surfaces and infrastructure, leading to increased maintenance costs and reduced road network lifespan.					
Impact Status: Detail of the impact is Positive, Neutral or Negative					
	E	D	R	M	P
Without Enhancement	Regional	Short Term	Recoverable	Moderate	Probable
Score	1	1	3	4	3
With Enhancement	Local	Short Term	Recoverable	Low	Probable
Score	1	1	2	3	3
Significance Calculation	Without Enhancement			With Enhancement	
S=(E+D+R+M)*P	Low Negative Impact (27)			Low Negative Impact (21)	
Can Impacts be Enhanced?	YES/NO and HOW/WHY				
Enhancement: <i>Limiting the number and frequency of heavy and overloaded vehicles where possible Undertaking regular maintenance, rehabilitation and upgrading substandard pavement conditions</i>					

9 Conclusions and Recommendations

Based on the information detailed in this report, the following conclusions are drawn:

- The proposed development and final layout can be supported from a traffic engineering point of view.
- The base year and forecast year road capacity has indicated that the proposed development will have little to no significant impact on the existing road network capacity and intersection operational performance.
- Given the findings of this report, it is recommended that the proposed development be considered favourably from a traffic engineering point of view as the intended construction will have no significant negative impact on the surrounding road network.

The following recommendations are made:

- A comprehensive route assessment of the entire transportation route to verify clearance, load bearing and sweeping radius distances is recommended.
- The substation access is recommended as the access position, based on safety considerations and mitigation measures outlined in the report. This is essentially a proposal to relocate the proposed existing access in order to meet the required sight distance requirements for the class of vehicle that will be using the access.
- It is recommended that the access points be priority controlled and widened to allow for acceleration lane and dedicated right turn lane off the main road, which will incorporate the turning characteristics of the expected abnormal vehicles.
- Clearance permits will be required for the transport of the WT components.
- It is recommended that applications for Abnormal Permits be lodged to the Department of Transport and Public Works, Eskom, and Telkom (where affected) at the time of construction.

Appendix A – Project Description: Hugo

SPECIFICATIONS OF PROPOSED DEVELOPMENT



WEF Technical Details Components	Description / Dimensions - Hugo	Description / Dimensions - Khoe
Maximum Generation Capacity	up to 360MW	up to 290MW
Type of technology	Onshore Wind	Onshore Wind
Number of Turbines	Up to 48	Up to 38
WTG Hub Height from ground level	up to 150m	up to 150m
Blade Length	up to 100m	up to 100m
Rotor Diameter	up to 200m	up to 200m
Structure height (Tip Height)	up to 250m	up to 250m
Structure orientation	Wind regiment dependant	Wind regiment dependant
Area occupied by both permanent and construction laydown areas	See layout	See layout
Operations and maintenance buildings (O&M building) with parking area	up to 1 HA	up to 1 HA
Site Access	Via the R318	Via the R318
Area occupied by inverter transformer stations/substations	up to 2.5 HA	up to 2.5 HA

WEF Technical Details Components	Description / Dimensions - Hugo	Description / Dimensions - Khoe
Capacity of on-site substation	132/33kv	132/33kv
Battery Energy Storage System footprint	up to 5 HA	up to 5 HA
BESS type	Lithium-ion or Redox-flow technology, depending on the most feasible at the time of implementation	Lithium-ion or Redox-flow technology, depending on the most feasible at the time of implementation
BESS Alternatives (site, technology, design and layout)	Same as above. See layout for design and position	Same as above. See layout for design and position
Length of internal roads	TBD	TBD
Width of internal roads	Access roads to the site and between project components with a width of approximately 4.5 m and a servitude of 13.5 m.	Access roads to the site and between project components with a width of approximately 4.5 m and a servitude of 13.5 m.
Proximity to grid connection	TBD	TBD
Internal Cabling	Cabling between the turbines, to be laid underground where practical.	Cabling between the turbines, to be laid underground where practical.
Height of fencing	TBD	TBD
Type of fencing	TBD	TBD
Water supply, volumes required	±26500m ³ for the construction, commissioning and test phase (±26 months), the majority being consumed during year-one of the construction. ±90m ³ /annum for the life-of-WEF (20-25 years)	±24500m ³ for the construction, commissioning and test phase (±26 months), the majority being consumed during year-one of the construction. ±90m ³ /annum for the life-of-WEF (20-25 years)
Waste Management, waste volumes, and how will it be managed	To be determined at a later stage- either through Municipal channels or private	To be determined at a later stage- either through Municipal channels or private

WEF Technical Details Components	Description / Dimensions - Hugo	Description / Dimensions - Khoe
Details on where material and equipment will be sourced for construction	To be determined upon construction and latest market availability	To be determined upon construction and latest market availability
Employment opportunities during construction and operations (maintenance) Skilled, semi-skilled, unskilled employees	Low skilled: up to (\pm 55%) Semi-skilled: up to (\pm 30%) Skilled: up to (\pm 15%)	Low skilled: up to (\pm 55%) Semi-skilled: up to (\pm 30%) Skilled: up to (\pm 15%)

PROJECT DESCRIPTION

Hugo WEF

The proposed Hugo WEF will comprise up to 48 turbines with a maximum output capacity of up to 360 MW with an anticipated lifespan of xxx years. The WEF will be located on the following land parcels: RE 147; RE/172; 0/173; RE/174; and 9/148 (See table below). The final design which will be requested for approval in the EA, will be determined based on the outcome of the specialist studies undertaken for the EIA phase of the development. The proposed turbine footprint and associated facility infrastructure will cover an area of up to 7900 ha, depending on the final design.

It is proposed that an on-site substation with a capacity up 132 kV with an up to 33 kV overhead / underground powerline will be installed. It is unknown at this stage how long the connection to the grid will be, or what route the cabling will be installed.

Khoe WEF

The proposed Khoe WEF will comprise up to 38 turbines with a maximum output capacity of up to 290 MW with an anticipated lifespan of xxx years. The WEF will be located on the following land parcels: 1/38; 2/38; 11/38; 193; and RE/37 (see table below). The final design which will be requested for approval in the EA, will be determined based on the outcome of the specialist studies undertaken for the EIA phase of the development. The proposed turbine footprint and associated facility infrastructure will cover an area of up to 4113 ha, depending on the final design.

It is proposed that an on-site substation with a capacity up 132 kV with an up to 33 kV overhead / underground powerline will be installed. It is unknown at this stage how long the connection to the grid will be, or what route the cabling will be installed.

LANDOWNER INFORMATION

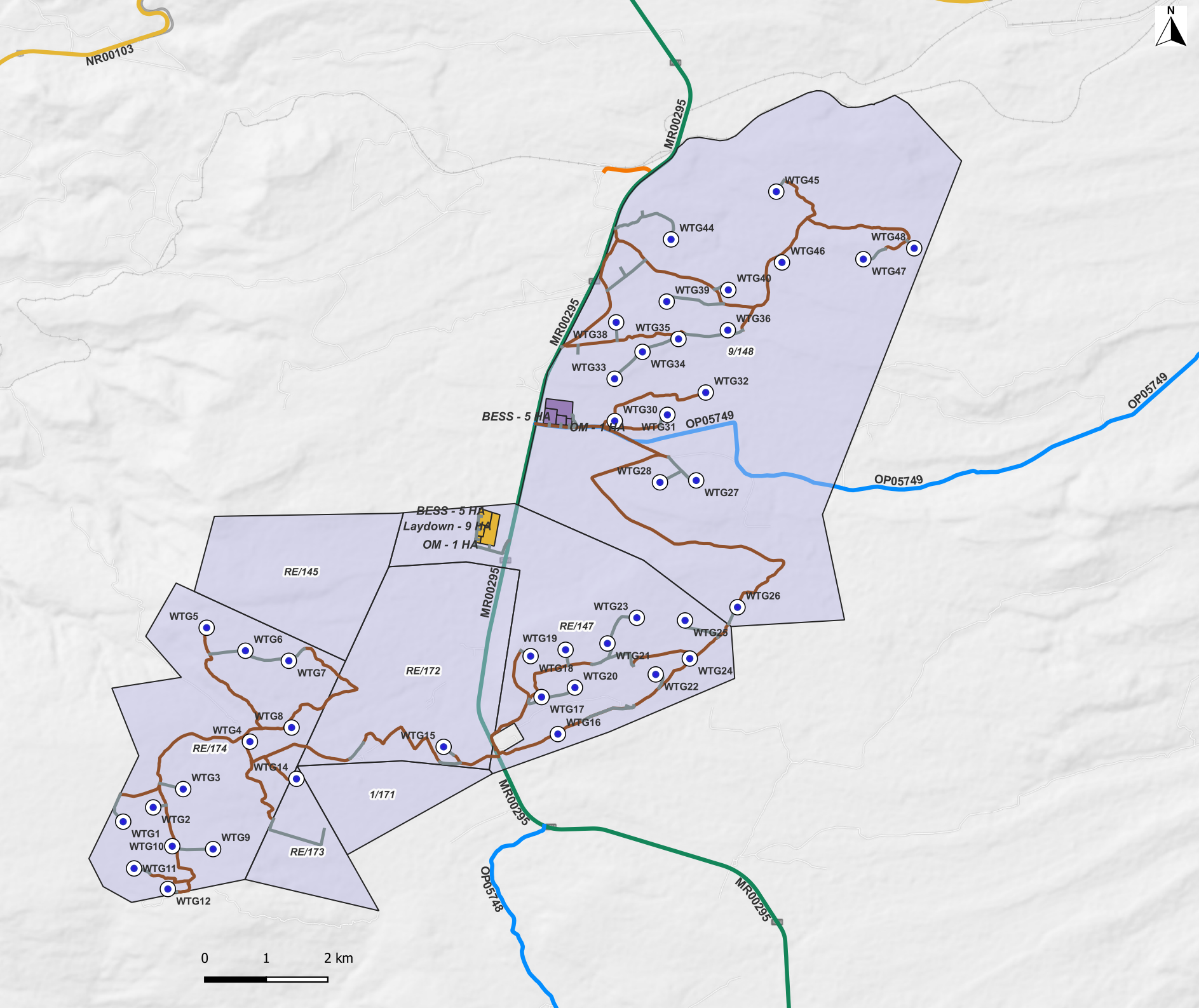
Hugo WEF

Landowner	Farm Name	Farm No.	Portion No.	SG Code
Blue Dot Prop 424	Ou de Kraal	145	RE	
Blue Dot Prop 424	Stinkfonteins Berg	147	RE	
Blue Dot Prop 424	Stinkfontein	172	RE	
Marius Hugo	Driehoek	173	0	
Marius Hugo	Presents Kraal	174	RE	
Dirk Uys Boerdery PTY LTD	Helpmakeer	148	9	
Overhead Transmission Line				
Marius Hugo	Presents Kraal	174	RE	
Dirk Uys	Helpmakeer	148	9	

Khoe WEF

Landowner	Farm Name	Farm No.	Portion No.	SG Code
Sandvlei Trust	Eendragt	38	1	
Hennie De Kock	Eendragt	38	2	
Hennie De Kock	Eendragt	38	11	
Johan Le Roux	Plaas 193	193		
Sophia Le Roux	Eendragt	37	RE	
Overhead Transmission Line				
Hennie De Kock	Eendragt	38	11	
Johan Le Roux	Plaas 193	193	9	
Sophia Le Roux	Eendragt	37	RE	

Appendix B – WTG Layout Hugo WEF



Legend

- Project boundary
- WTGs
- National Road (N1)
- Internal Roads**
 - Existing Roads
 - New Road
- Provincial Road Network**
 - Main Roads**
 - MR00295 (R318)
 - Divisional Roads**
 - DR01428
 - DR01402
 - Minor Roads**
 - OP05748
 - OP05958
 - OP05959
 - OP05960
 - OP05961
 - OP05962
 - OP05963
 - OP05964
 - OP05965
 - OP06039
 - OP06041
- Source Esri Street

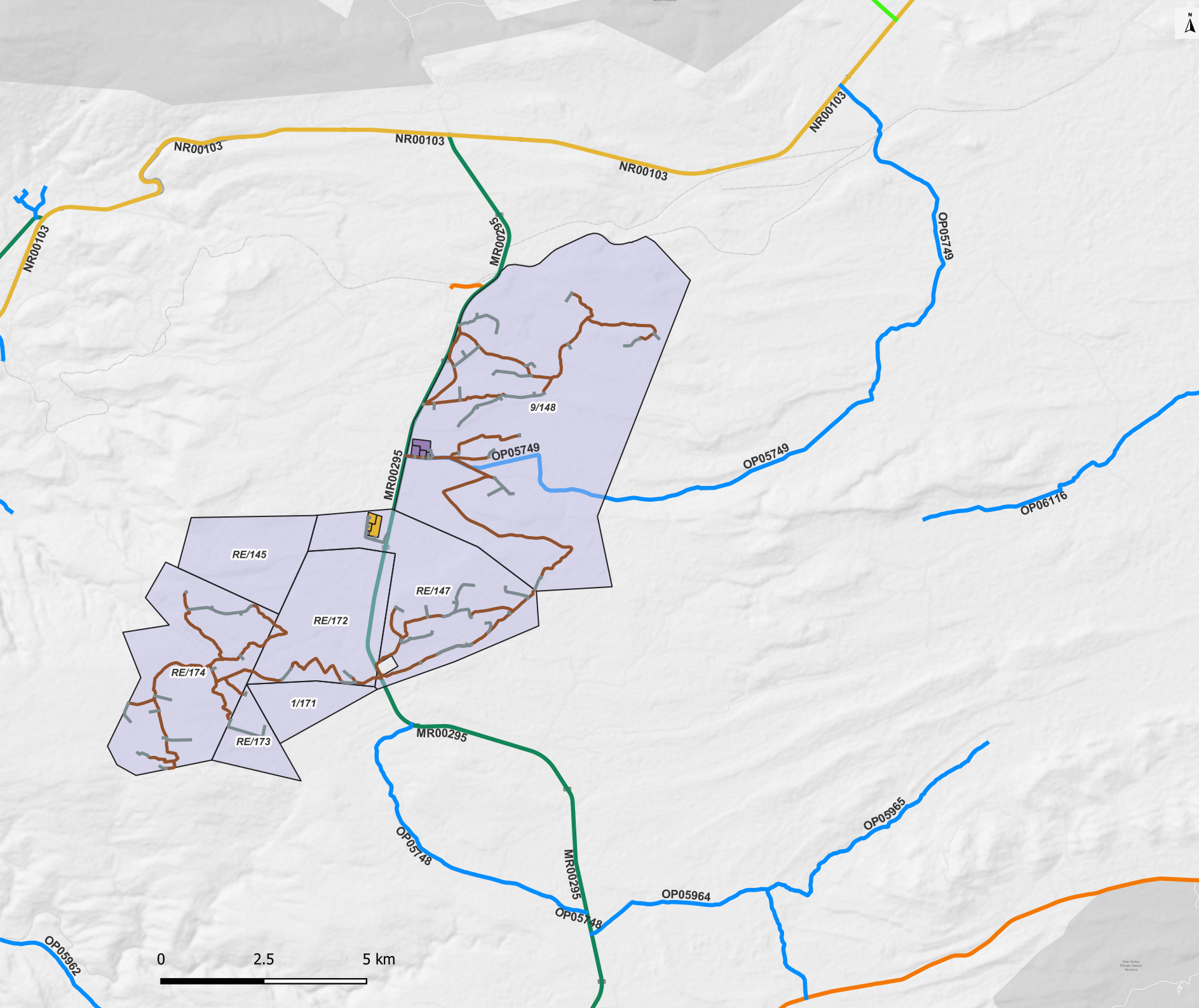
Distance from ALL proclaimed road reserve boundaries
 Min required toppling distance plus 5m
 (250+5m = 255m)

WTG No.	Distance (m)	Road Name
1	6055.482	OP05748
2	5946.816	MR00295
3	4939.055	MR00295
4	3761.797	MR00295
5	4553.349	MR00295
6	3886.786	MR00295
7	3098.33	MR00295
8	3010.229	MR00295
9	4531.754	OP05748
10	5245.448	OP05748
11	5864.377	OP05748
12	5292.634	OP05748
14	3270.898	MR00295
15	736.075	MR00295
16	1000.23	MR00295
17	1062.02	MR00295
18	745.247	MR00295
19	1284.296	MR00295
20	1538.816	MR00295
21	2008.326	MR00295
22	2995.111	MR00295
23	2243.856	MR00295
24	3266.195	MR00295
25	3050.112	MR00295
26	2104.795	OP05749
27	741.3	OP05749
28	743.486	OP05749
30	170.314	OP05749
31	322.913	OP05749
32	515.639	OP05749
33	1349.957	OP05749
34	574.471	MR00295
35	1410.441	OP05749
36	1486.246	OP05749
38	627.31	MR00295
39	1276.813	MR00295
40	2088.523	MR00295
44	977.229	MR00295
45	1811.564	MR00295
46	2752.612	MR00295
47	3646.407	OP05749
48	3732.127	OP05749

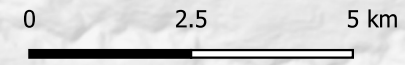
Hugo WTG Layout



Appendix C – Existing Surrounding Road Network



- Legend**
- Project boundary
 - WTGs
 - National Road (N1)
 - Internal Roads**
 - Existing Roads
 - New Road
 - Provincial Road Network**
 - Main Roads**
 - MR00295 (R318)
 - Divisional Roads**
 - DR01428
 - DR01402
 - Minor Roads**
 - OP05748
 - OP05958
 - OP05959
 - OP05960
 - OP05961
 - OP05962
 - OP05963
 - OP05964
 - OP05965
 - OP06039
 - OP06041
 - Source Esri Street



Hugo Road Network



1. N1 National Road



2. R318 (MR00295) Provincial Main Road



3. DR01442 Provincial Divisional Road



4. OP05749 Provincial Minor Road



5. OP05748 Provincial Minor Road



Appendix D – Existing Intersections

1. Intersection N1 and R381 (MR00295)



2. Intersection R318 (MR00295) and DR01442



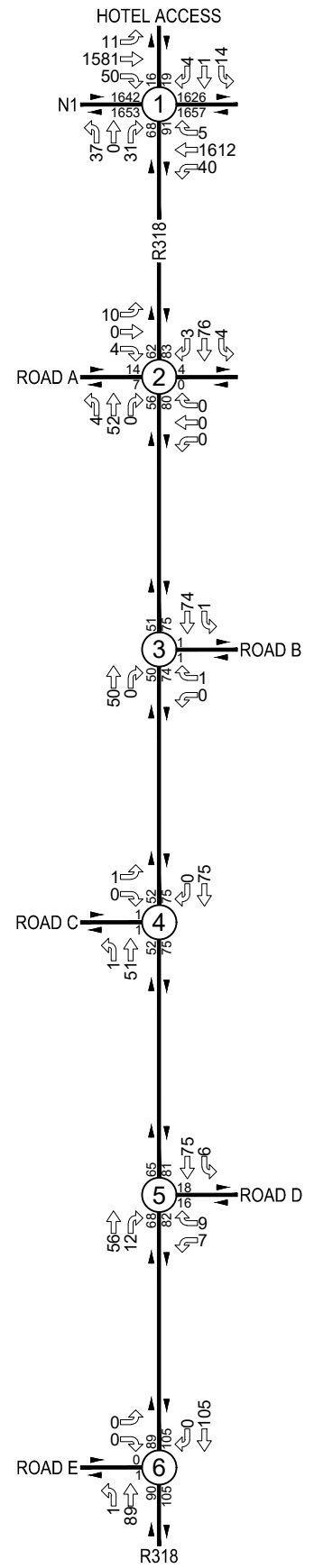
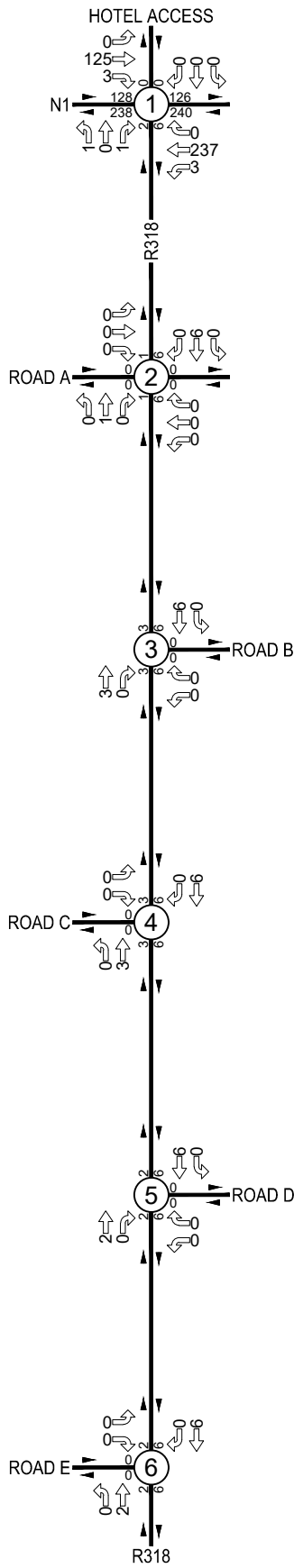
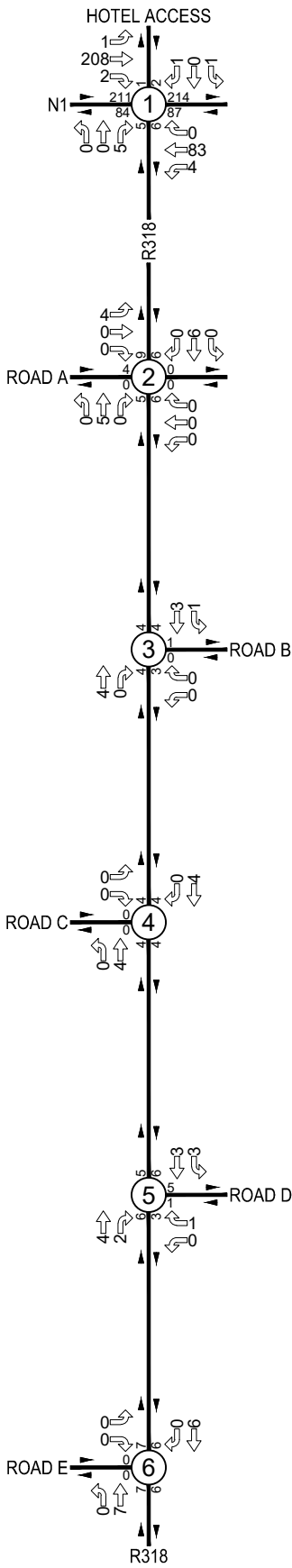
3. Intersection R318 (MR00295) and OP05749



4. Intersection R318 (MR00295) and OP05748



Appendix E – Existing Traffic



Appendix F – Provincial Roads and SANRAL Counts

-- Start --				-- End --				Link Volumes have been projected to current year						
Station	km	Date	AADT	Station	km	Date	AADT	Intersection (Start Km)	Scale Bar	Light	Heavy	Taxis	Buses	Total
4416C	73.26	22-02-02	1051	4417A	75.49	22-02-02	1457	Montagu Municipal	79.26	1044	103	10	11	1168
				4416A	73.26	22-02-02	801	DR1387 Baden	71.34	599	67	4	7	677
4415C	66.35	22-02-02	634	4415A	66.35	22-02-02	550	DR1392 Pietersfontn	63.41					
									55.49	524	59	4	5	592
4414C	44.18	22-02-02	594	4414A	44.18	22-02-02	425	DR1402 Versameling	47.56	346	40	2	2	390
4983C	38.52	22-02-03	368	4983A	38.52	22-02-03	304	Surfaced Open	39.63	251	35	3	2	291
				4983A	38.52	22-02-03	304	Gravel Open	31.71	183	29	2	1	215
4985C	32.31	22-02-03	183	4985A	32.31	22-02-03	177	OP05962 Keerom	23.78	147	25	2	1	175
4412C	26.76	22-02-03	180	4412A	26.76	22-02-03	164	DR1428 Leeubosfntn	15.85	169	27	3	1	200
4411C	4.37	21-11-16	216	4411A	4.37	21-11-16	236	DR1442 Matroosbrg Stn	7.93	206	34	6	2	248
4410C	0.00	21-11-16	228					NR1/3 Touws River N1 NR1/3 De Doorns N1	0.00					

Western Cape Government

Print

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1 of 1

MR00295

Next>

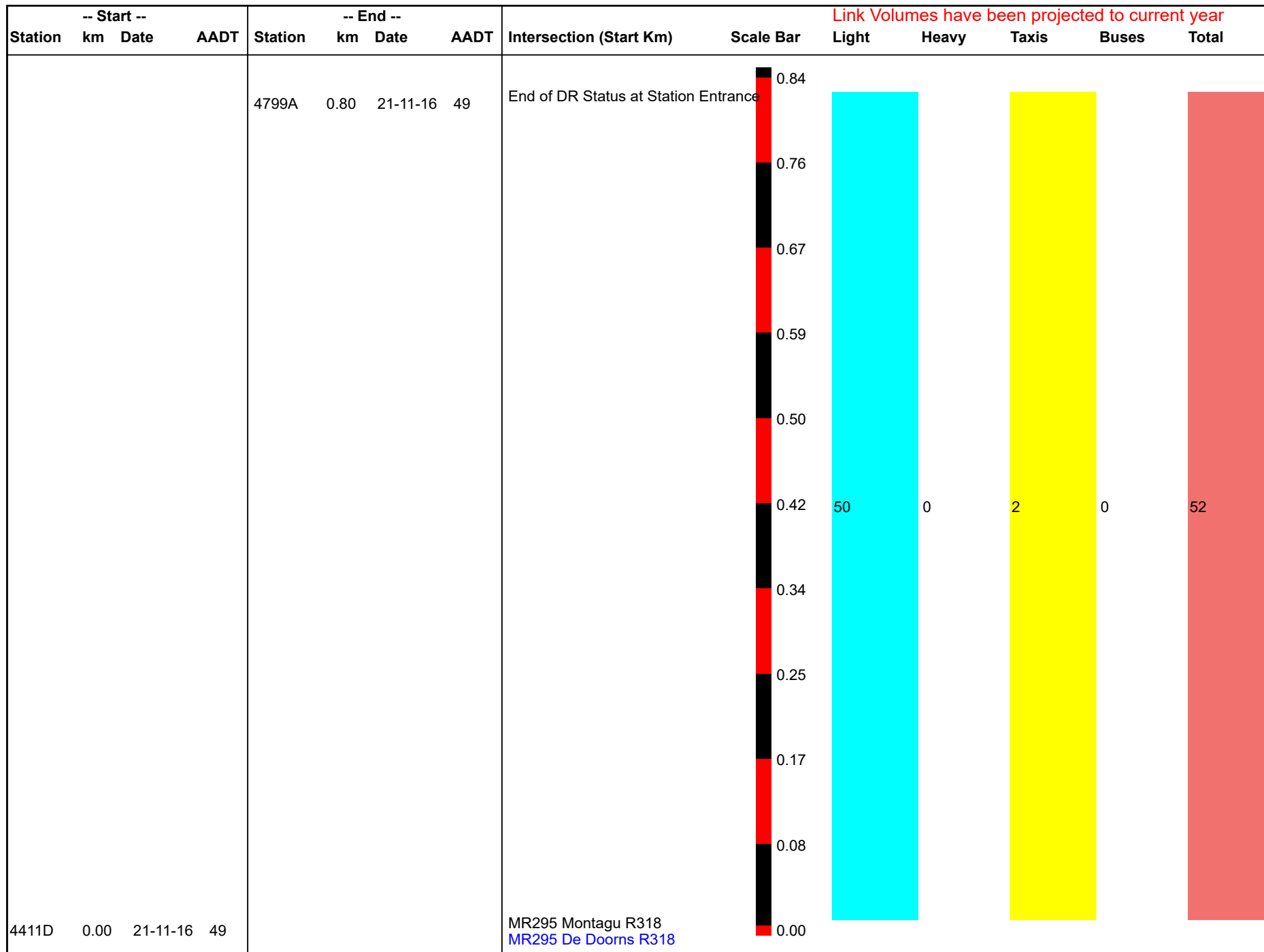
Zoom

S:

E:

No Zoom

Exit



Western Cape Government

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1 of 1

DR01442 ▾

Next>

Zoom

S:

E:

No Zoom

Exit

Station Information

Site Number	18017	Site Identifier	26709
Site Name	ST-J_N001_03_50-4		
Site Description	Between De Doorns & R318 Montagu T/O		
Site Type	Secondary (Temp)	Owner	SANRAL
Physical Lanes	2	Responsibility	NON-TOLL
Logical Lanes	2	Installation Date	2015-08-26
GPS Longitude	19.805935	Termination Date	
GPS Latitude	-33.395485	Status	In Use
Region	West	Companion Site	
Road	N001	Speed Limit	120
Route	N001	Count Type	Normal Traffic Counting Station
Section	03	Distance	50.39
Authority	SANRAL	Contract No	NRA 53000/141/2
Contract Org	Mikros Traffic Monitoring (Pty) Ltd	Station History Type	Full Site
System Type	C1		

Lane No	Lane Description	Stream No	Stream Description	Direction	Reverse Lane No	Pos
1	To Touws River	1	To Touws River	North	2	1
2	To Worcester	2	To Worcester	South	1	1

PHOTO



Direction 1

To Touws River

PHOTO



Direction 2

To Worcester

PHOTO



As Built

Traffic Highlights of Site: ST-J_N001_03_50-4 (18017)

Site No	18017
Site Name	ST-J_N001_03_50-4
Site Description	Between De Doorns & R318 Montagu T/O
Road Description	Route : N001 Section : 03N Distance : 50.39 km
GPS Position	Latitude: -33.395485 Longitude: 19.805935
Number of Lanes	2
Station Type	Secondary (Temp)

Requested Data Period	01 Jan 2019 - 31 Dec 2019
First and Last Data Dates	02 Apr 2019 - 07 May 2019
Data Available for Requested Period as Percentage	10%

Last Full Day Count for ADT and ADTT	06 May 2019
Number of Full Days in Requested Period	34

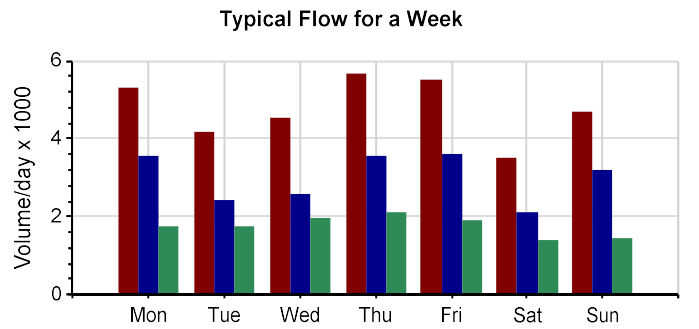
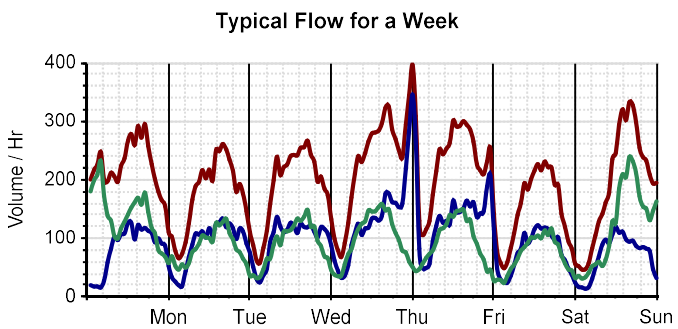
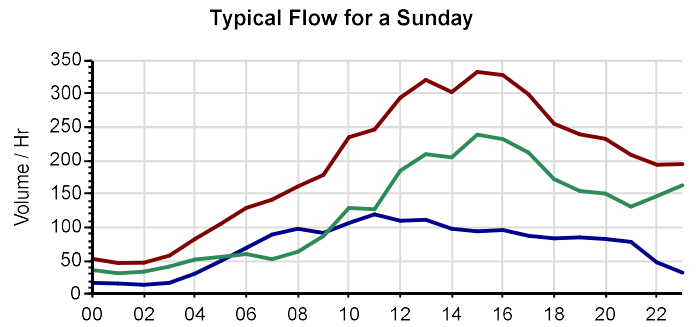
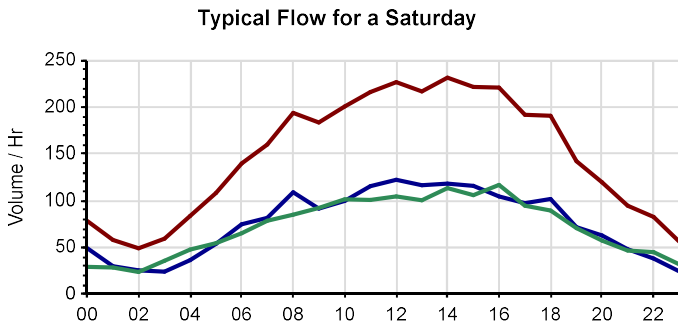
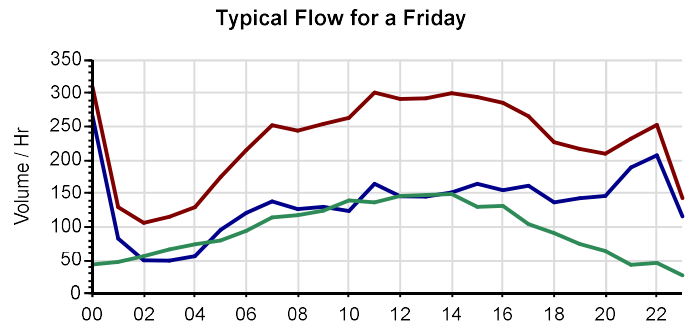
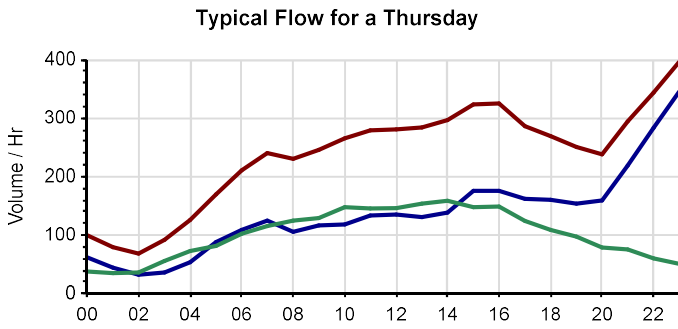
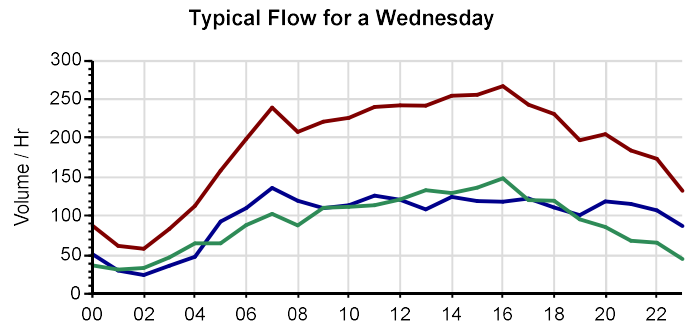
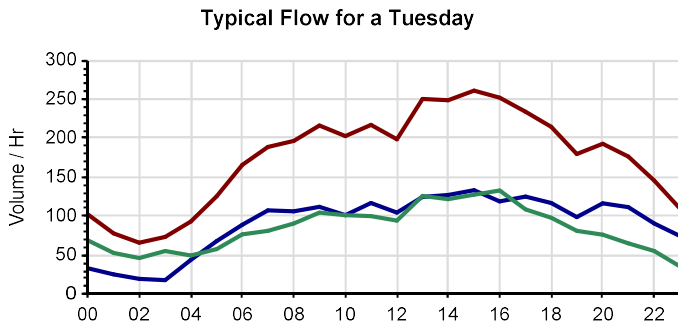
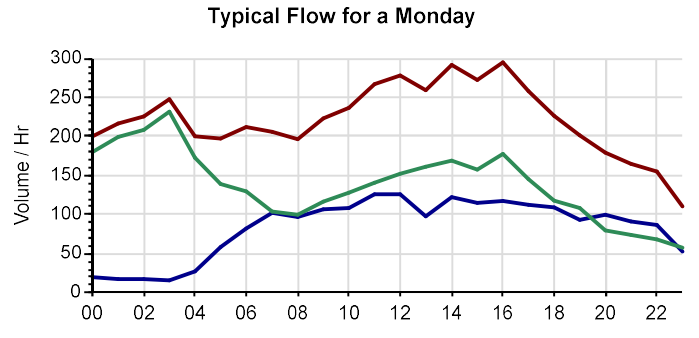
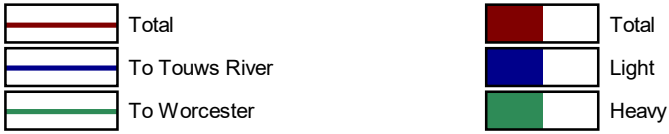
Highlights per Stream		Str 1: To Touws River	Str 2: To Worcester	Value
1.1	Total Number of Vehicles	82,509	83,815	166,324
1.2	Average Daily Traffic (ADT)	2,387	2,428	4,815
1.3	Average Daily Truck Traffic (ADTT)	846	926	1,772
1.4	Percentage of Trucks	35.7 %	38.3 %	37.0 %
1.5	Truck Split % (Short : Medium : Long)	23 : 11 : 66	21 : 10 : 69	22 : 10 : 68
1.6	Percentage of Night Traffic [20h00 - 6h00)	31.2 %	29.1 %	30.1 %
2.1	Speed Limit			120
2.2	Average Speed (km/hr)	100.3	96.4	98.4
2.3	Average Speed - Light Vehicles (km/hr)	110.1	105.8	108.0
2.4	Average Speed - Heavy Vehicles (km/hr)	82.3	83.2	82.8
2.5	Average Night Speed (km/hr)	96.3	93.6	95.0
2.6	15th Centile Speed (km/hr)	77.3	76.2	76.8
2.7	85th Centile Speed (km/hr)	124.3	119.2	121.8
2.8	Percentage of Vehicles in Excess of Speed Limit	40.8 %	40.3 %	40.6 %
3.1	Percentage Vehicles in Flows Over 600 (vehs/hr)	2.9 %	0 %	1.53%
3.2	Percentage of Vehicles less than 2s behind vehicle ahead	0 %	0 %	0 %

4.1	Total Number of Heavy Vehicles	29,446	32,116	61,562
4.2	Estimated Average Number of axles per Truck	5.6	5.8	5.7
4.3	Estimated Truck Mass (Ton/Truck)	32.2	32.9	32.6
4.4	Estimated Average E80 / Truck	2.9	3.0	2.95
4.5	Estimated Daily E80 on the Road			3,823.0
4.6	Estimated Daily E80 in the North Direction			5,486.0
4.7	Estimated Daily E80 in the South Direction			5,984.0
4.8	Estimated Daily E80 in the Worst North Lane			5,486.0
4.9	Estimated Daily E80 in the Worst South Lane			5,984.0
5.1	ASSUMPTION on Axles/Truck (Short:Medium:Long)			(2.0 : 5.0 : 7.0)
5.2	ASSUMPTION on Mass/Truck (Short:Medium:Long)			(10.9 : 31.5 : 39.8)
5.3	ASSUMPTION on E80s/Truck (Short:Medium:Long)			(0.5 : 2.1 : 3.9)

Traffic Volumes		Date and Time	Value
6.1	Highest Volume on the Road (vehs/hr)	19 Apr 2019 (00:00 - 01:00)	935
6.2	Highest Volume in the North (vehs/hr)	19 Apr 2019 (00:00 - 01:00)	891
6.3	Highest Volume in the South (vehs/hr)	22 Apr 2019 (16:00 - 17:00)	477
6.4	Highest Volume in a Lane (vehs/hr)	19 Apr 2019 (00:00 - 01:00)	891
6.5	15th Highest Volume on the Road (vehs/hr)	18 Apr 2019 (13:00 - 14:00)	464
6.6	15th Highest Volume in the North Direction (vehs/hr)	03 May 2019 (22:00 - 23:00)	253
6.7	15th Highest Volume in the South Direction (vehs/hr)	05 May 2019 (14:00 - 15:00)	298
6.8	30th Highest Volume on the Road (vehs/hr)	05 May 2019 (12:00 - 13:00)	386
6.9	30th Highest Volume in the North Direction (vehs/hr)	12 Apr 2019 (22:00 - 23:00)	212
6.10	30th Highest Volume in the South Direction (vehs/hr)	06 May 2019 (02:00 - 03:00)	239




Station Typical Flow Graphs

Site	18017 - ST-J_N001_03_50-4
Region	West
Actual Period	02 Apr 2019 - 07 May 2019
Classification	RSA Ext Lgt/Hvy
Day Type	Normal Day & Fixed Public Holiday+

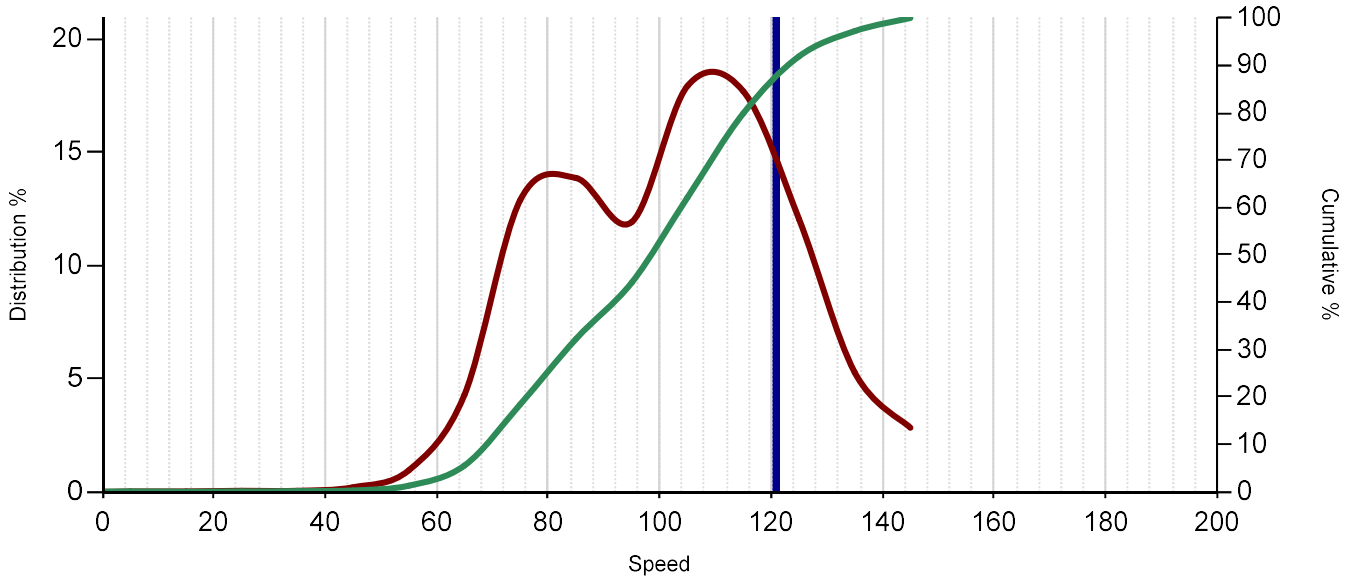


Station Speed Distribution

Site	18017 - ST-J_N001_03_50-4
Speed Limit	120 km/hr
Period	01 Jan 2019 - 31 Dec 2019




	Distribution
	Cumulative
	Speed Limit

Lane 1 - To Touws River

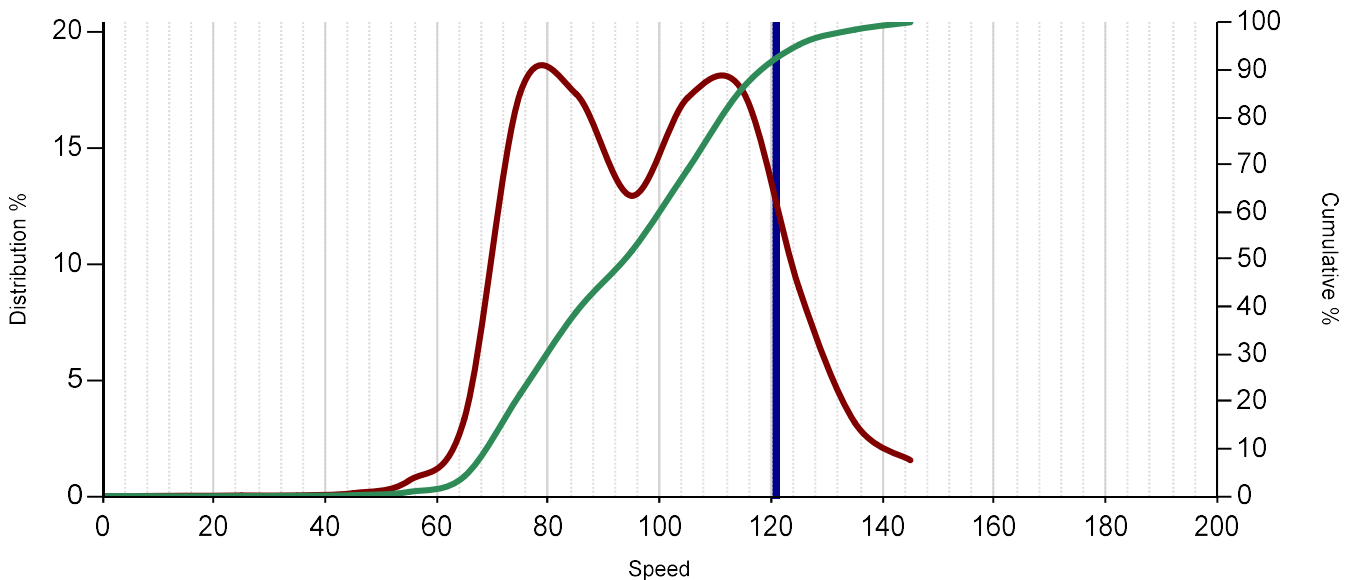


Station Speed Distribution

Site	18017 - ST-J_N001_03_50-4
Speed Limit	120 km/hr
Period	01 Jan 2019 - 31 Dec 2019

	Distribution
	Cumulative
	Speed Limit

Lane 2 - To Worcester



Station Information

Site Number	18018	Site Identifier	26710
Site Name	ST-J_N001_03_65-2		
Site Description	R318 Montagu T/O & R46 Ceres T/O		
Site Type	Secondary (Temp)	Owner	SANRAL
Physical Lanes	2	Responsibility	NON-TOLL
Logical Lanes	2	Installation Date	2015-10-26
GPS Longitude	19.950054	Termination Date	
GPS Latitude	-33.375847	Status	In Use
Region	West	Companion Site	
Road	N001	Speed Limit	100
Route	N001	Count Type	Normal Traffic Counting Station
Section	03	Distance	65.22
Authority	SANRAL	Contract No	NRA 53000/141/2
Contract Org	Mikros Traffic Monitoring (Pty) Ltd	Station History Type	Full Site
System Type	C1		

Lane No	Lane Description	Stream No	Stream Description	Direction	Reverse Lane No	Pos
1	To Touws River	1	To Touws River	North	2	1
2	To Worcester	2	To Worcester	South	1	1

PHOTO



Direction 1

To Touws River

PHOTO



Direction 2

To Worcester

PHOTO



As Built

Traffic Highlights of Site: ST-J_N001_03_65-2 (18018)

Site No	18018
Site Name	ST-J_N001_03_65-2
Site Description	R318 Montagu T/O & R46 Ceres T/O
Road Description	Route : N001 Section : 03N Distance : 65.22 km
GPS Position	Latitude: -33.375847 Longitude: 19.950054
Number of Lanes	2
Station Type	Secondary (Temp)

Requested Data Period	01 Jan 2019 - 31 Dec 2019
First and Last Data Dates	07 May 2019 - 29 May 2019
Data Available for Requested Period as Percentage	6%

Last Full Day Count for ADT and ADTT	28 May 2019
Number of Full Days in Requested Period	21

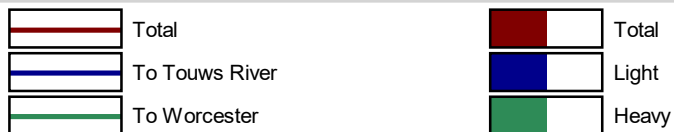
Highlights per Stream		Str 1: To Touws River	Str 2: To Worcester	Value
1.1	Total Number of Vehicles	41,256	41,314	82,570
1.2	Average Daily Traffic (ADT)	1,878	1,894	3,772
1.3	Average Daily Truck Traffic (ADTT)	758	832	1,590
1.4	Percentage of Trucks	41.0 %	44.1 %	42.5 %
1.5	Truck Split % (Short : Medium : Long)	13 : 11 : 76	13 : 10 : 77	13 : 10 : 76
1.6	Percentage of Night Traffic [20h00 - 6h00)	29.4 %	29.0 %	29.2 %
2.1	Speed Limit			100
2.2	Average Speed (km/hr)	101.7	93.3	97.5
2.3	Average Speed - Light Vehicles (km/hr)	112.3	103.3	107.8
2.4	Average Speed - Heavy Vehicles (km/hr)	85.5	81.4	83.5
2.5	Average Night Speed (km/hr)	100.2	92.0	96.1
2.6	15th Centile Speed (km/hr)	79.5	74.1	76.8
2.7	85th Centile Speed (km/hr)	124.5	116.4	120.5
2.8	Percentage of Vehicles in Excess of Speed Limit	67.1 %	61.9 %	64.5 %
3.1	Percentage Vehicles in Flows Over 600 (vehs/hr)	0 %	0 %	0.00%
3.2	Percentage of Vehicles less than 2s behind vehicle ahead	0 %	0 %	0 %

4.1	Total Number of Heavy Vehicles	16,898	18,214	35,112
4.2	Estimated Average Number of axles per Truck	6.1	6.2	6.2
4.3	Estimated Truck Mass (Ton/Truck)	35.1	35.2	35.2
4.4	Estimated Average E80 / Truck	3.3	3.3	3.30
4.5	Estimated Daily E80 on the Road			3,466.0
4.6	Estimated Daily E80 in the North Direction			5,004.0
4.7	Estimated Daily E80 in the South Direction			5,394.0
4.8	Estimated Daily E80 in the Worst North Lane			5,004.0
4.9	Estimated Daily E80 in the Worst South Lane			5,394.0
5.1	ASSUMPTION on Axles/Truck (Short:Medium:Long)			(2.0 : 5.0 : 7.0)
5.2	ASSUMPTION on Mass/Truck (Short:Medium:Long)			(10.9 : 31.5 : 39.8)
5.3	ASSUMPTION on E80s/Truck (Short:Medium:Long)			(0.5 : 2.1 : 3.9)

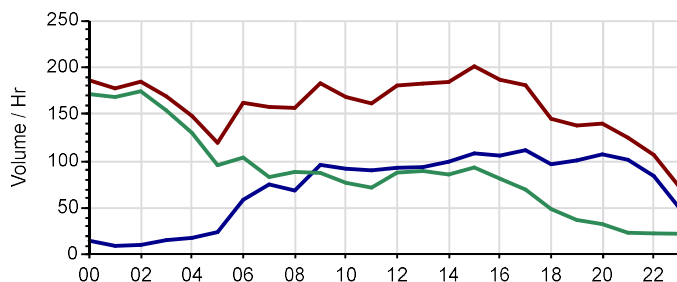
Traffic Volumes		Date and Time	Value
6.1	Highest Volume on the Road (vehs/hr)	10 May 2019 (16:00 - 17:00)	304
6.2	Highest Volume in the North (vehs/hr)	17 May 2019 (21:00 - 22:00)	244
6.3	Highest Volume in the South (vehs/hr)	19 May 2019 (16:00 - 17:00)	231
6.4	Highest Volume in a Lane (vehs/hr)	17 May 2019 (21:00 - 22:00)	244
6.5	15th Highest Volume on the Road (vehs/hr)	12 May 2019 (17:00 - 18:00)	268
6.6	15th Highest Volume in the North Direction (vehs/hr)	09 May 2019 (22:00 - 23:00)	172
6.7	15th Highest Volume in the South Direction (vehs/hr)	12 May 2019 (15:00 - 16:00)	174
6.8	30th Highest Volume on the Road (vehs/hr)	24 May 2019 (21:00 - 22:00)	252
6.9	30th Highest Volume in the North Direction (vehs/hr)	24 May 2019 (12:00 - 13:00)	147
6.10	30th Highest Volume in the South Direction (vehs/hr)	19 May 2019 (12:00 - 13:00)	151

Station Typical Flow Graphs

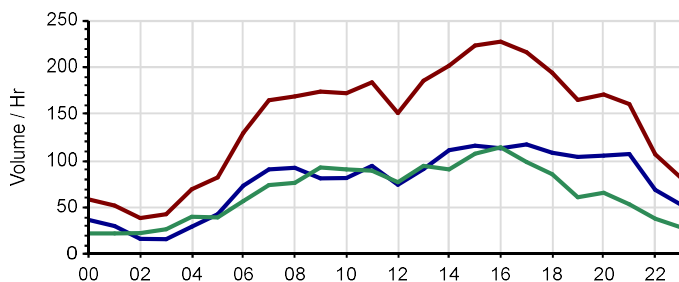
Site	18018 - ST-J_N001_03_65-2
Region	West
Actual Period	07 May 2019 - 29 May 2019
Classification	RSA Ext Lgt/Hvy
Day Type	Normal Day & Fixed Public Holiday+



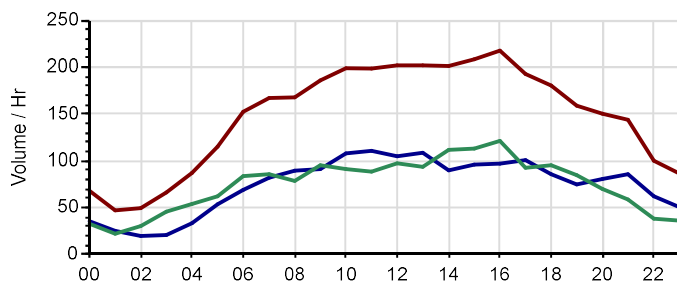
Typical Flow for a Monday



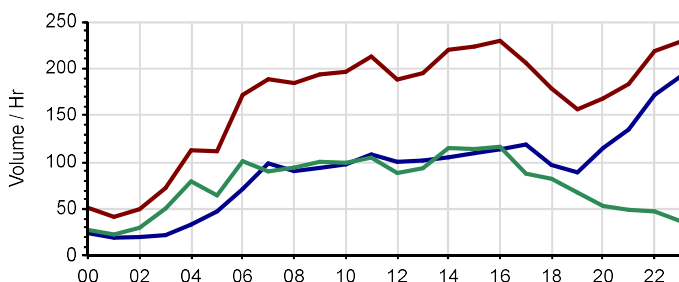
Typical Flow for a Tuesday



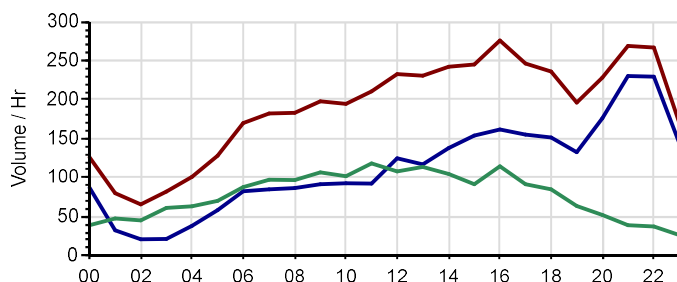
Typical Flow for a Wednesday



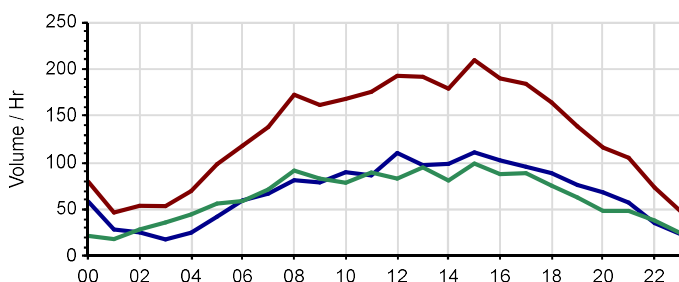
Typical Flow for a Thursday



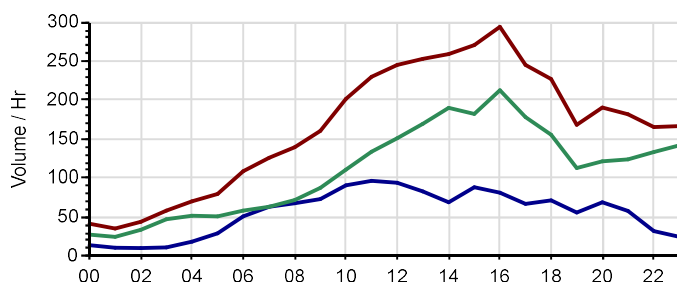
Typical Flow for a Friday



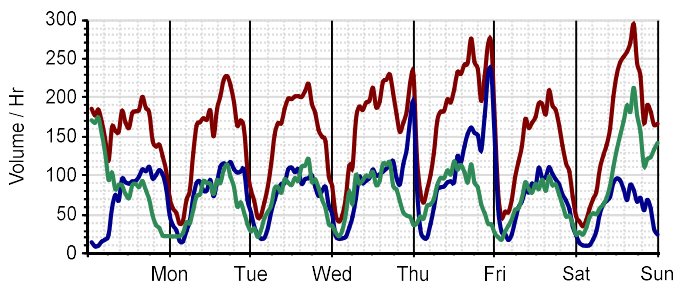
Typical Flow for a Saturday



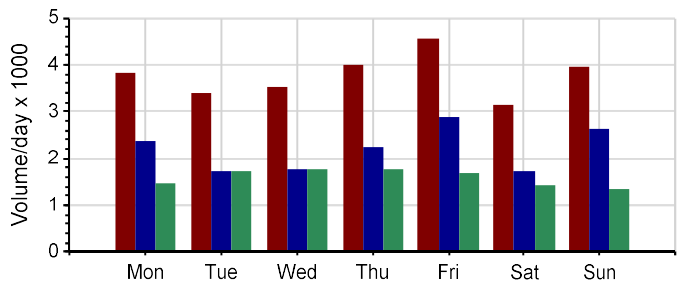
Typical Flow for a Sunday



Typical Flow for a Week






Typical Flow for a Week

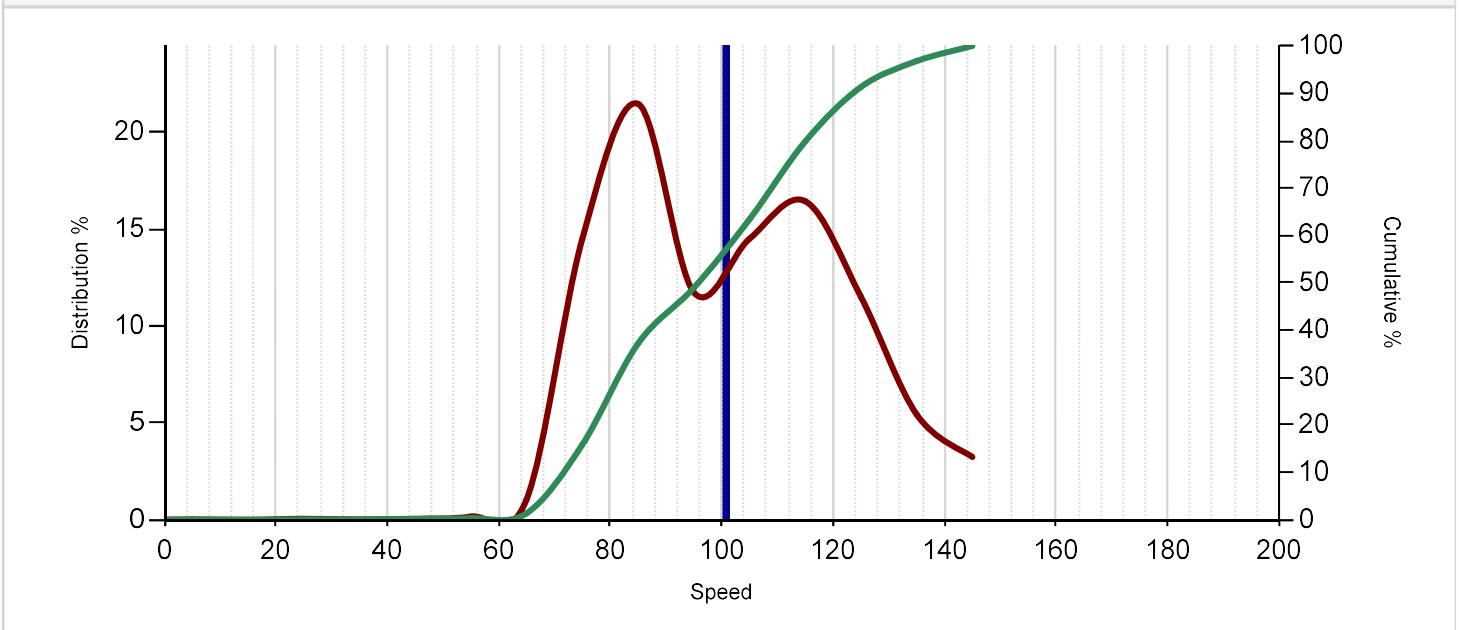


Station Speed Distribution

Site	18018 - ST-J_N001_03_65-2
Speed Limit	100 km/hr
Period	01 Jan 2019 - 31 Dec 2019




	Distribution
	Cumulative
	Speed Limit

Lane 1 - To Touws River

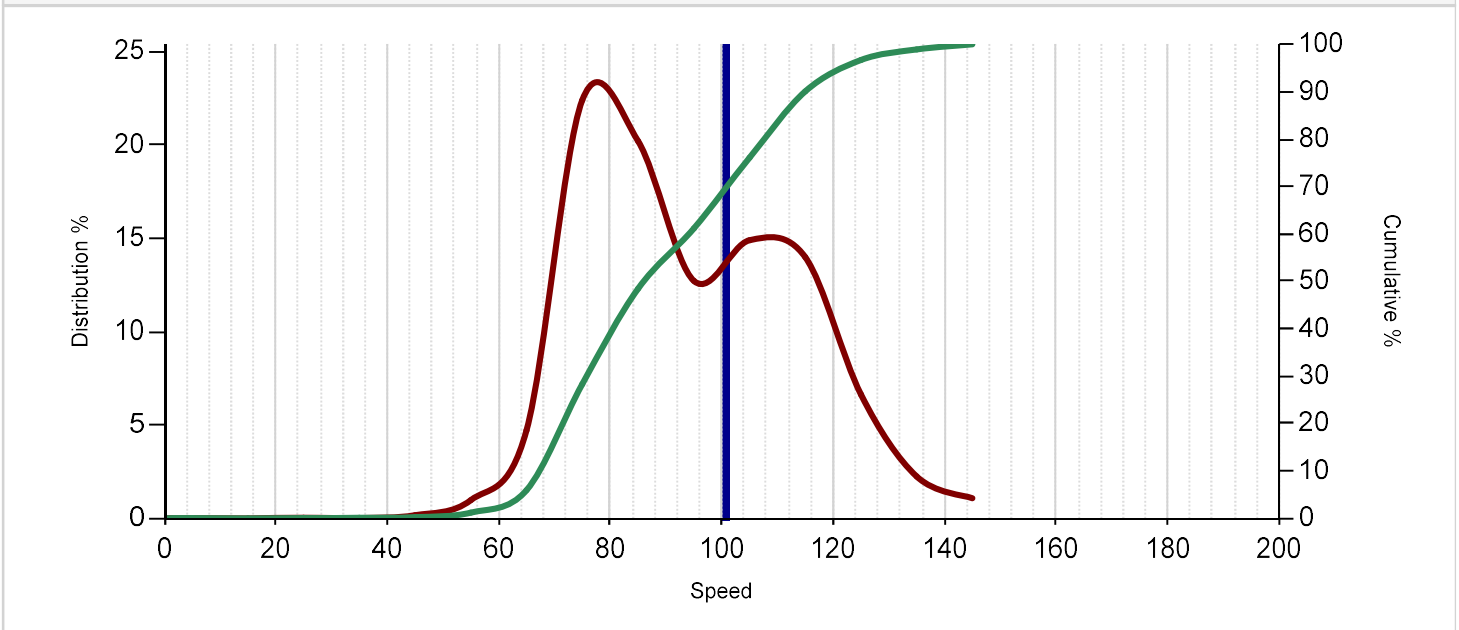


Station Speed Distribution

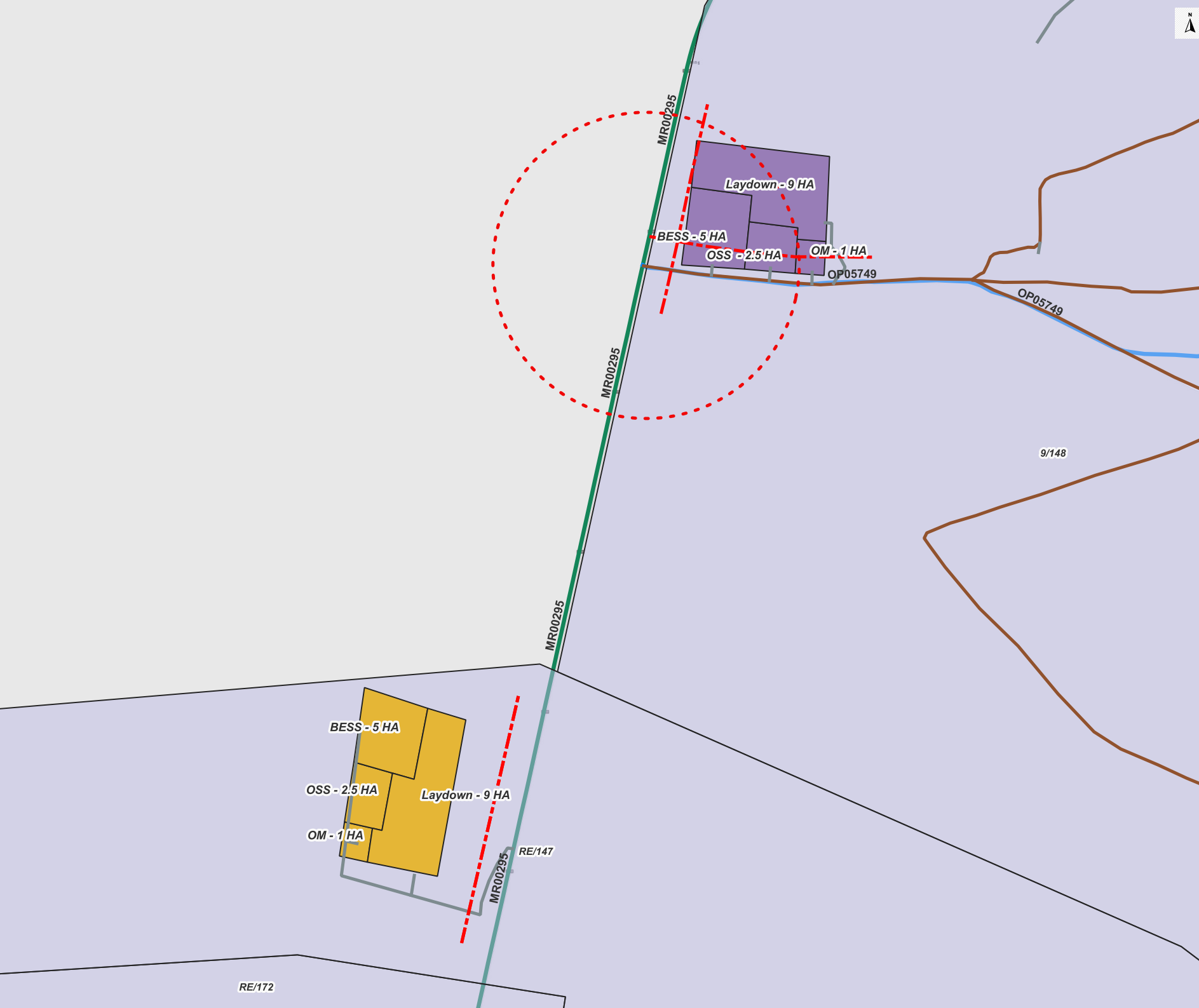
Site	18018 - ST-J_N001_03_65-2
Speed Limit	100 km/hr
Period	01 Jan 2019 - 31 Dec 2019

	Distribution
	Cumulative
	Speed Limit

Lane 2 - To Worcester



Appendix G – Building Lines



Legend

- Associated Infrastructure – Preferred
- Associated Infrastructure – Alternative

Internal Roads

- Existing Roads
- New Road

Provincial Road Network

- Main Roads
- Minor Roads

Building restrictions

- Building Restriction Line (500m) from the centreline's of intersecting trunk, main, and divisional roads; and where these roads intersect other roads.
- Building Restriction Line (95m) from Centreline of the Road Reserve

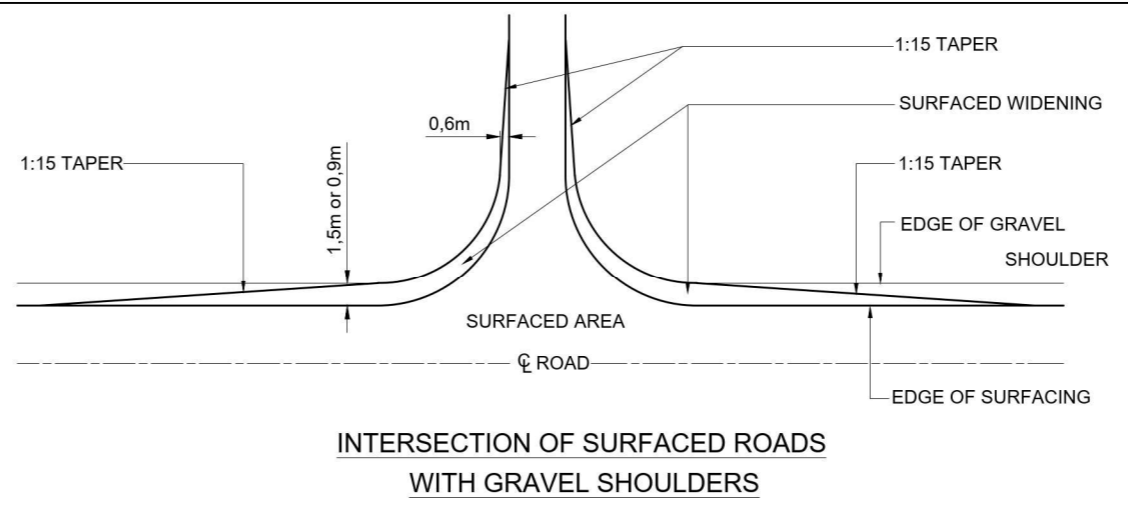
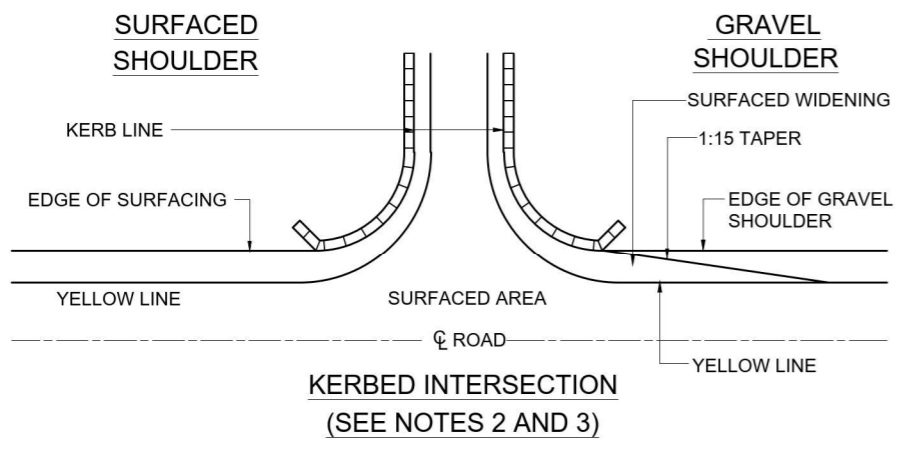
Source Esri Street

0 250 500 m

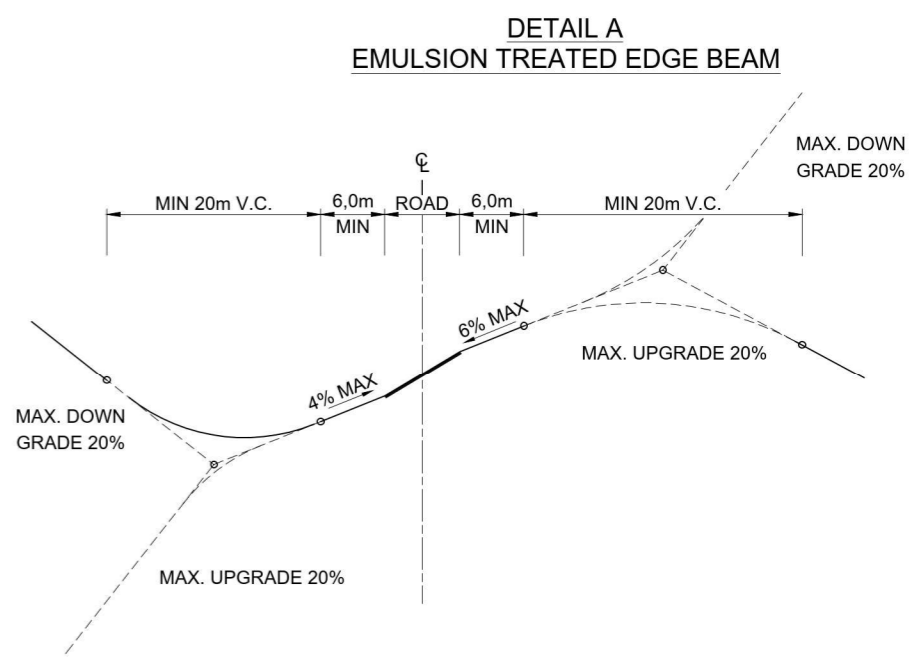
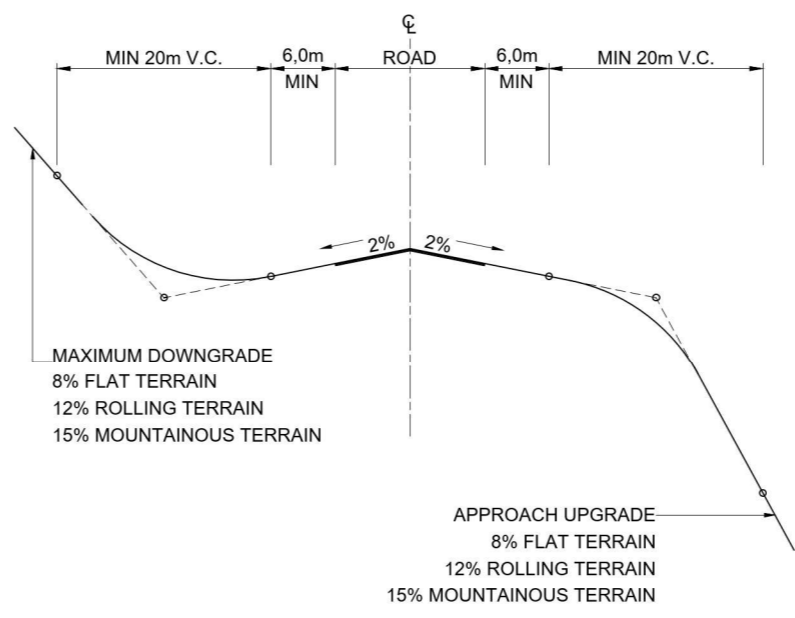
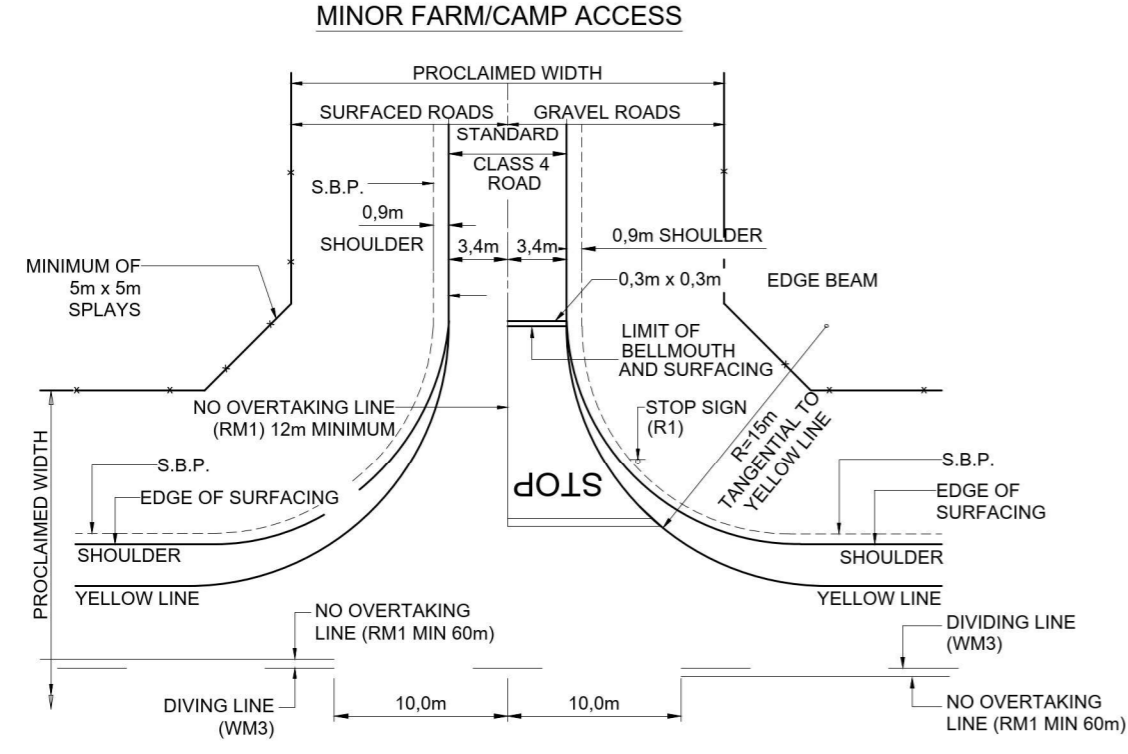
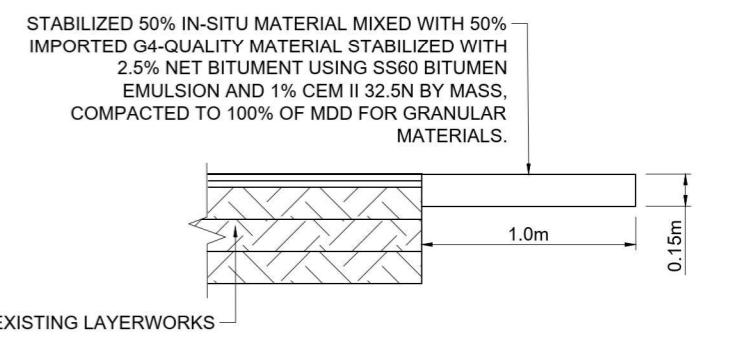
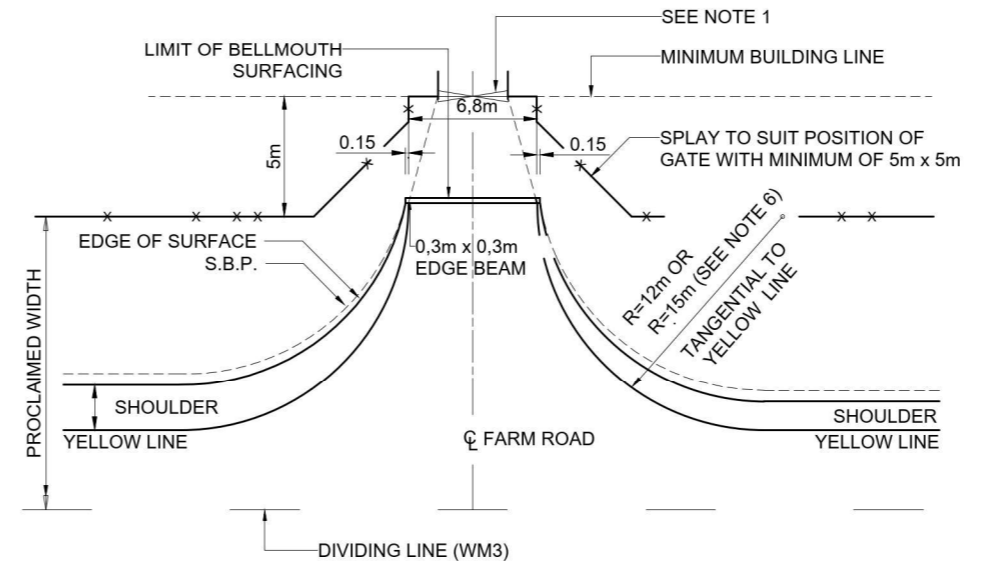
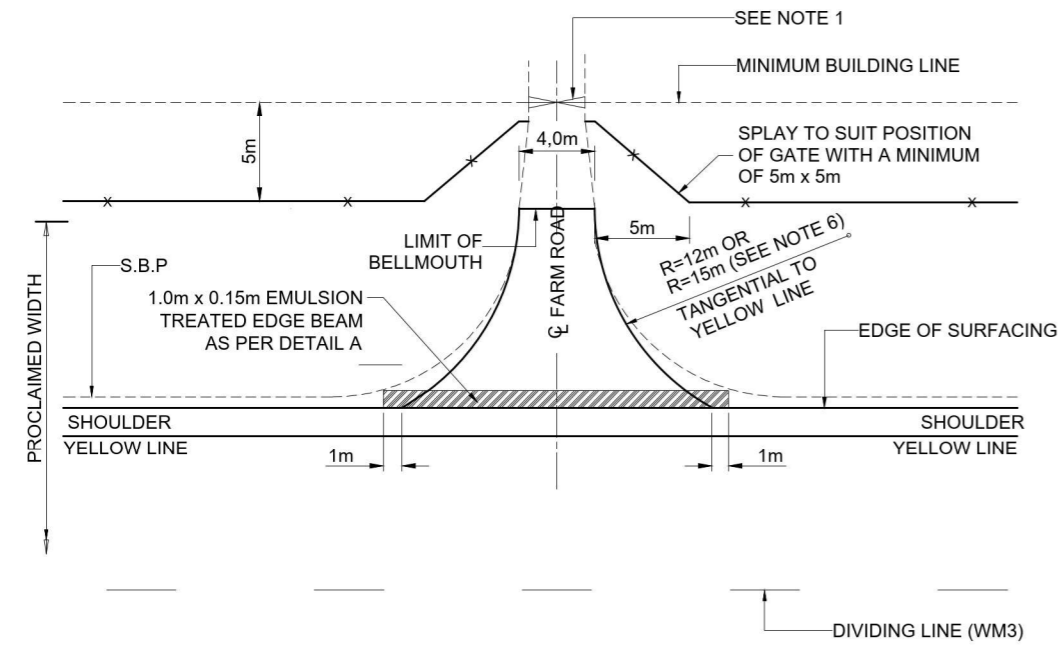
Laydown Area & Buildings



Appendix H – Standard Plans



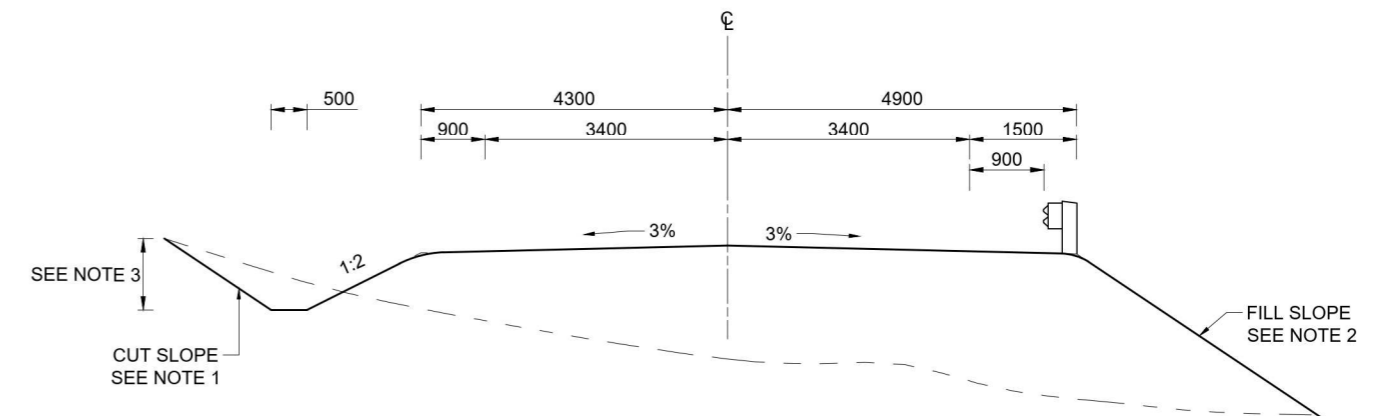
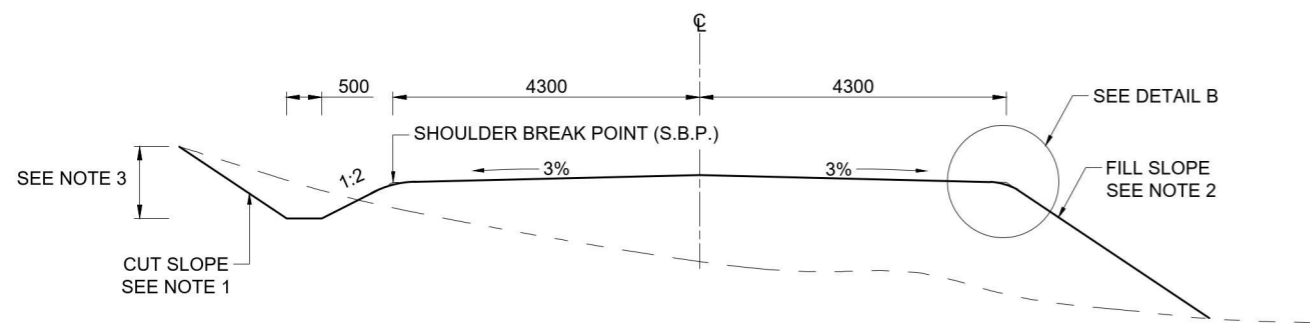
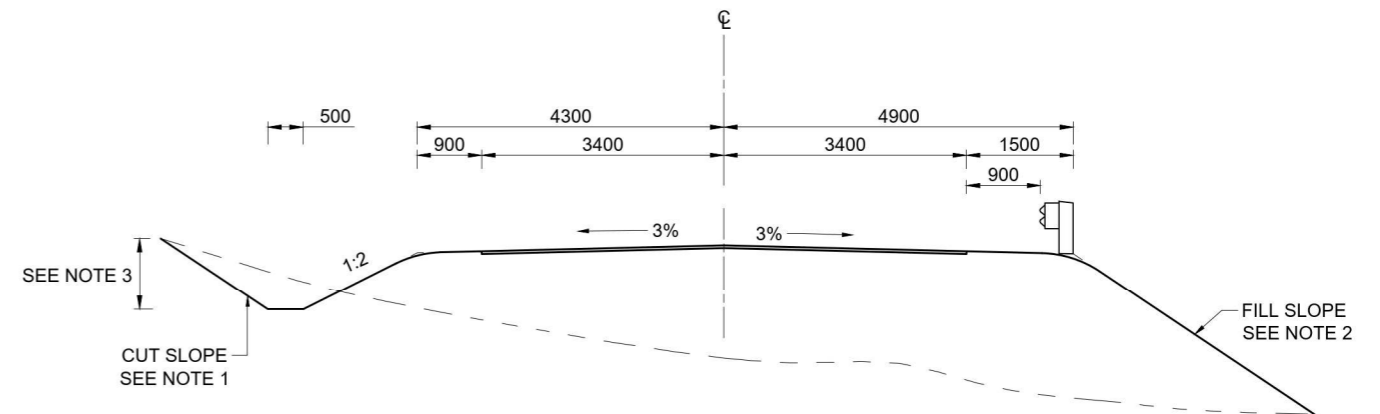
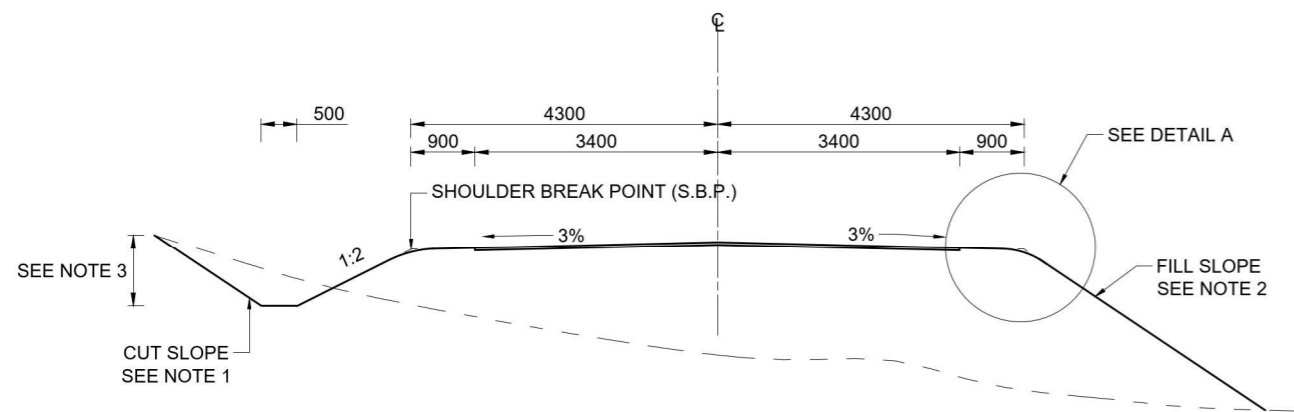
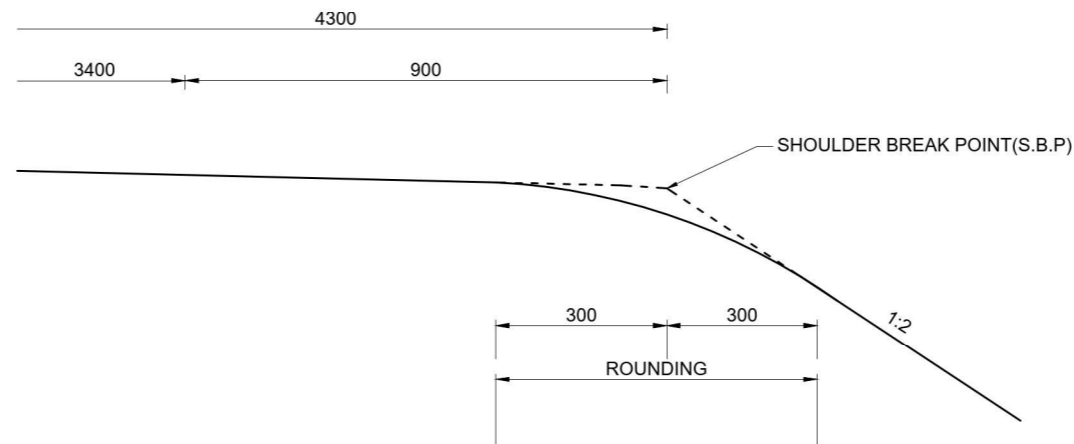
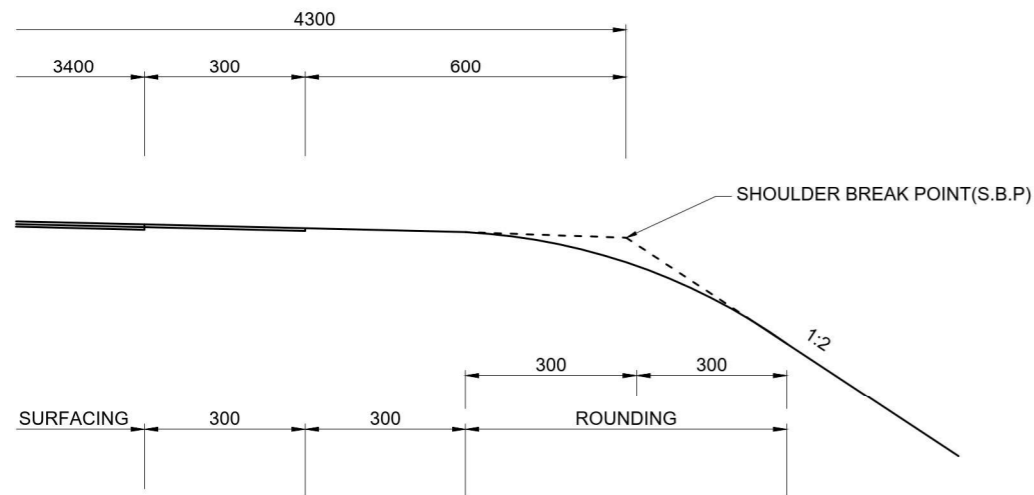
- NOTES :
1. THE STANDARD GATE IS TO BE LOCATED AT END OF RAMP IN FILL AND AT THE BUILDING LINE IN CUT. THE WIDTH OF THE GATE TO SUIT FARM EQUIPMENT.
 2. FOR ROADS WITH SURFACED SHOULDERS THE KERB LAYOUT MUST BE DESIGNED AND CONSTRUCTED SO THAT THE KERBS LINE UP WITH THE EDGE OF SURFACING.
 3. FOR ROADS WITH GRAVEL SHOULDERS THE KERB LAYOUT MUST BE DESIGNED AND CONSTRUCTED SO THAT THE KERBS LINE UP WITH THE OUTSIDE EDGE OF USABLE SHOULDER WITH A SURFACED TAPER EXTENDING BEYOND THE KERB TO THE NORMAL CARRIAGEWAY SURFACED WIDTH.
 4. WHERE TWO ROADS INTERSECT THE NUMERICAL DIFFERENCE OF THE GRADIENTS (ROLL OVER) SHOULD NOT EXCEED 10% WITH A MAXIMUM SUPERELEVATION OF 6% ON THE MAIN ROAD.
 5. MAXIMUM APPROACH GRADIENT TO BE 4% UPGRADE AND 6% DOWNGRADE.
 6. THE BELLMOUTH RADIUS OF 15m IS ONLY APPLICABLE WHERE SIGNIFICANT SU + T VEHICLES USE THE ACCESS.



No.	DATE	ADDITIONS AND AMENDMENTS
0	OCT - 2023	ORIGINAL VERSION

STANDARD PLANS	WESTERN CAPE GOVERNMENT DEPARTMENT OF INFRASTRUCTURE TRANSPORT INFRASTRUCTURE BRANCH	INTERSECTION	SCALE : N.T.S.	INDEX NO. WCS/11/2/C1
		INTERSECTION AND FARM ACCESS DETAIL	A2 ORIGINAL	PLAN NO. SHEET 1 OF 1

- NOTES :**
- CUT SLOPE :**
 1:0,25 IN ROCK
 1:1 IN SOFT ROCK
 1:1,50 IN SOFT MATERIAL OR AS DIRECTED
 WHERE CUTS ARE DEEPER THAN 4m, BENCHES
 MAY BE REQUIRED AS DIRECTED.
 FOR CUTS DEEPER THAN 6m IN CLAY, REFER
 TO MATERIALS ENGINEER.
 - FILL SLOPES :**
 1:2 FILL LESS THAN 4,0m IN HEIGHT
 1:1,5 FILL GREATER THAN 4,0m IN HEIGHT
 OR AS DIRECTED
 FILLS GREATER THAN 6m IN CLAY SHALL BE
 REFERRED TO MATERIALS ENGINEER
 BENCHES IN FILL TO BE CONSTRUCTED AT
 8m INTERVALS BELOW S.B.P.
 FILLS GREATER THAN 3,5m WITH 1:1,5
 SLOPES TO BE EVALUATED FOR GUARDRAIL
 WARRANTS
 - SIDE DRAIN DEPTH :**
 LAYERWORK DEPTH PLUS 200mm OR AS DIRECTED
 BY MATERIALS ENGINEER.



No.	DATE	ADDITIONS AND AMENDMENTS
0	OCT - 2023	ORIGINAL VERSION

STANDARD PLANS

WESTERN CAPE GOVERNMENT
 DEPARTMENT OF INFRASTRUCTURE
 TRANSPORT INFRASTRUCTURE BRANCH

CROSS SECTIONS

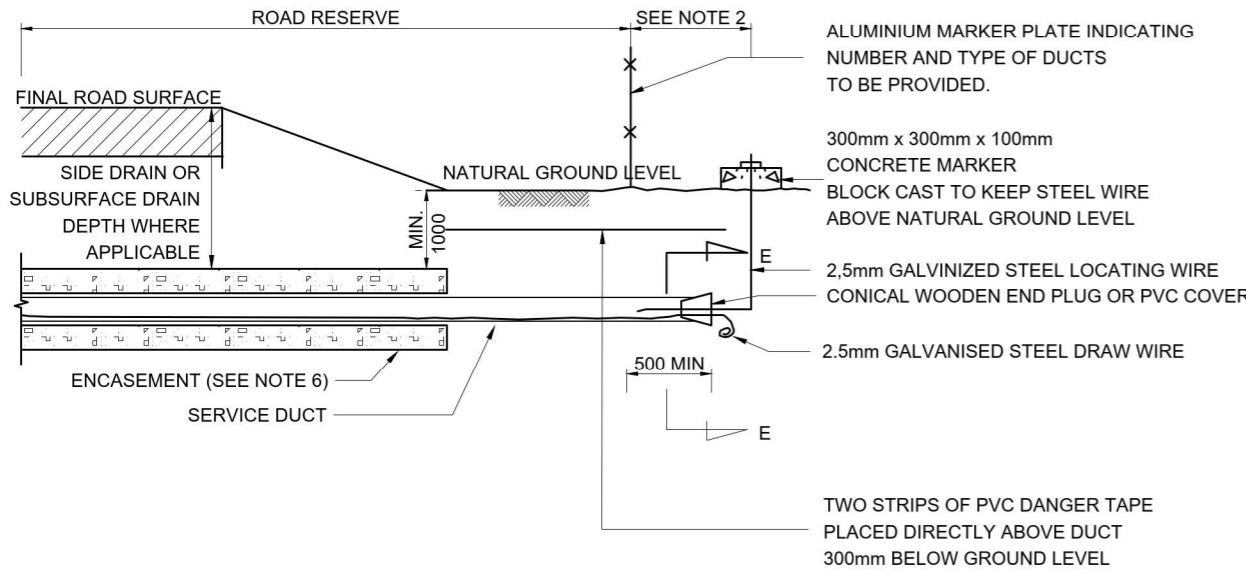
STANDARD LOW VOLUME CROSS SECTIONS

SCALE : N.T.S.

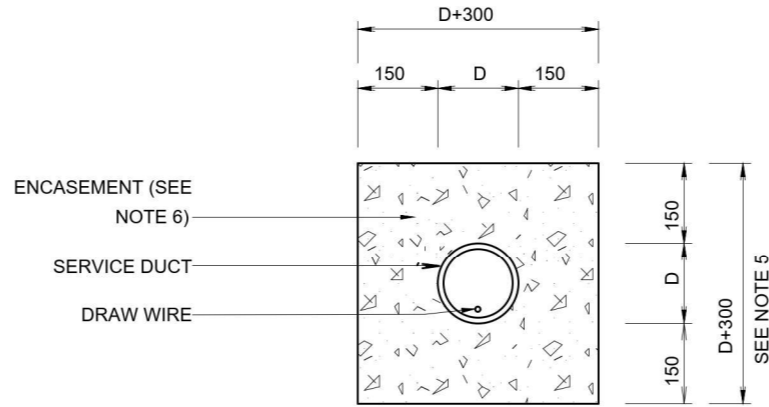
A2 ORIGINAL

INDEX NO.
WCS/11/1/D2

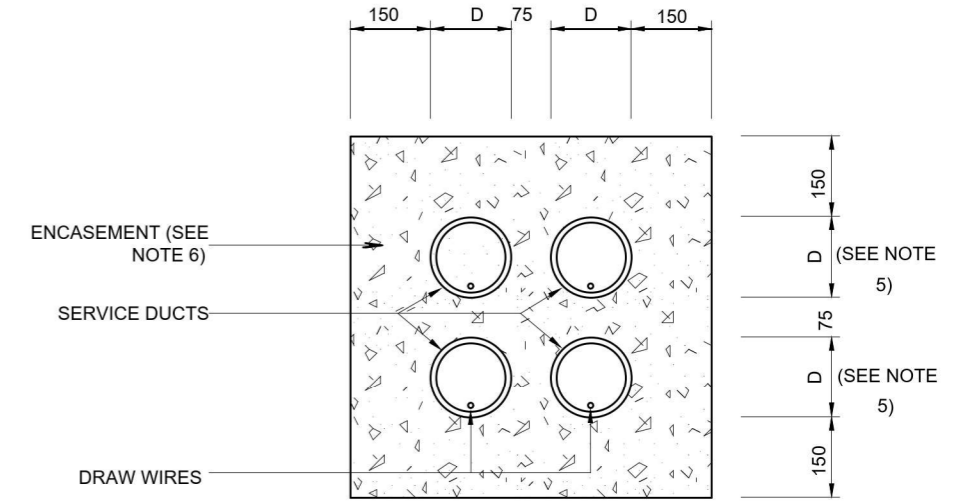
PLAN NO.
 SHEET 2 OF 2



LONGITUDINAL SECTION OF SERVICE DUCT

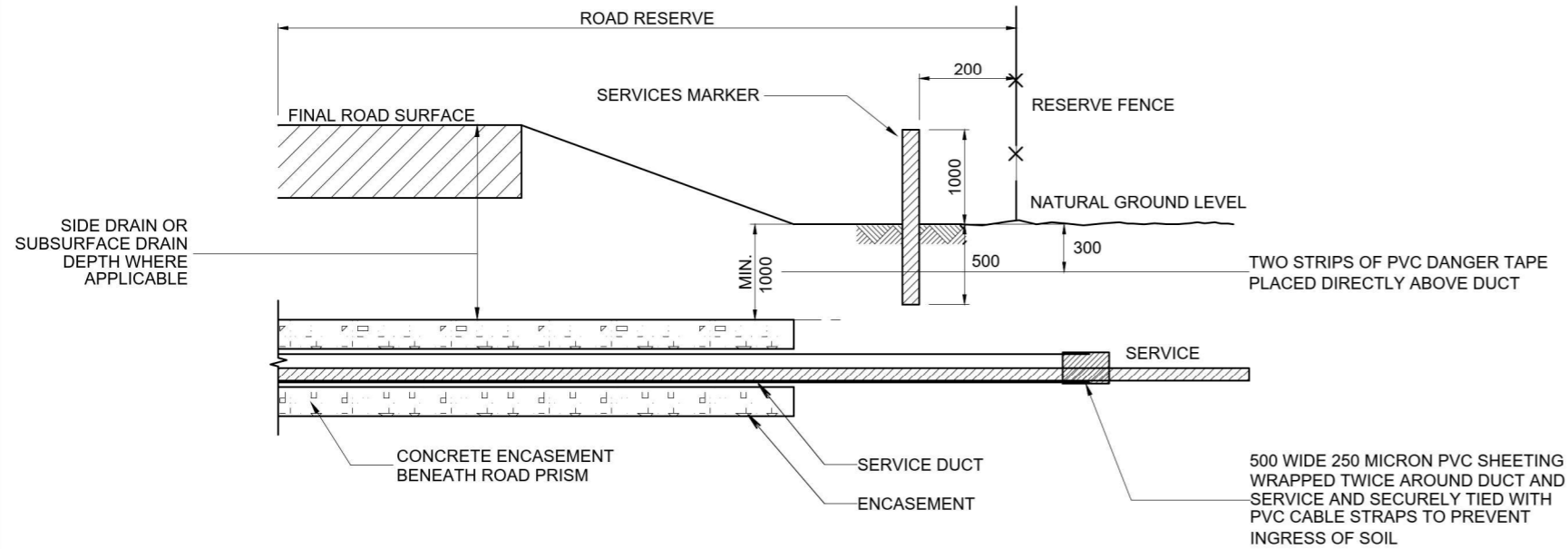


SECTION E-E



TYPICAL CROSS-SECTION OF MULTIPLE SERVICE DUCT

DUCTS WITHOUT INSTALLED SERVICE



DUCT WITH INSTALLED SERVICE

NOTES :

1. P.V.C. SERVICE DUCT PIPES MUST COMPLY WITH SANS 791.
2. DUCTS MUST EXTEND BEYOND ROAD RESERVE BOUNDARIES, 1000mm
3. SERVICE DUCT TO BE LAID AT A MIN. SLOPE OF 1%.
4. FOR POSITIONS AND SIZES OF SERVICE DUCTS REFER TO LAYOUT PLANS.
5. D MAXIMUM = 200mm.
6. ENCASEMENT FOR DEPTH <2,0m : CONCRETE CLASS 20/20
ENCASEMENT FOR DEPTH >2,0m : SOILCRETE (1:12 CEMENT:SOIL)

No.	DATE	ADDITIONS AND AMENDMENTS
0	OCT - 2023	ORIGINAL VERSION

STANDARD PLANS

WESTERN CAPE GOVERNMENT
DEPARTMENT OF INFRASTRUCTURE
TRANSPORT INFRASTRUCTURE BRANCH

SERVICE DUCTS

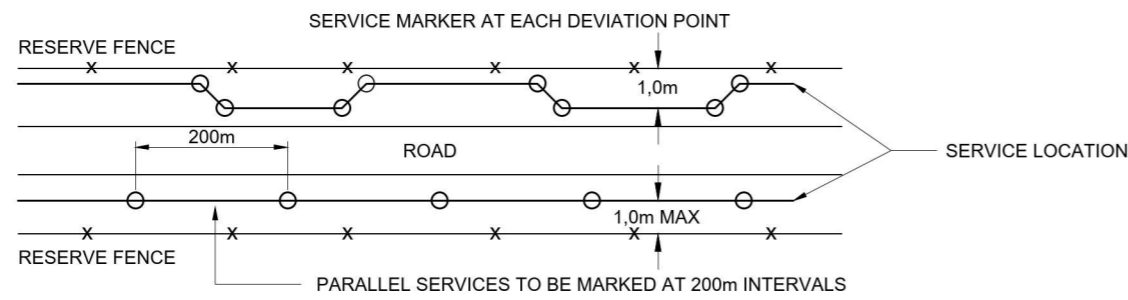
DETAILS OF SERVICES DUCTS FOR RURAL ROADS

SCALE : N.T.S.

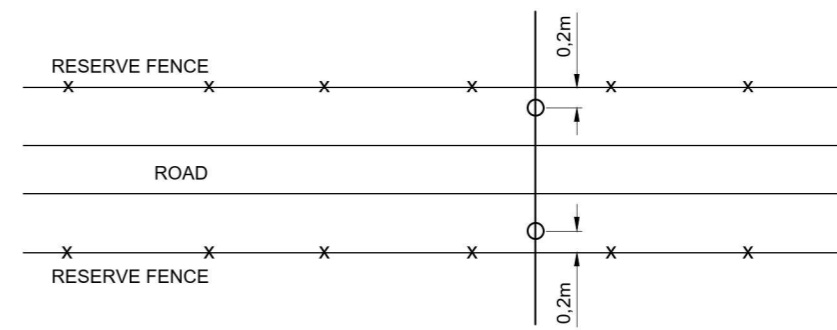
A2 ORIGINAL

INDEX NO.
WCS/22/4/C1

PLAN NO.
SHEET 1 OF 2

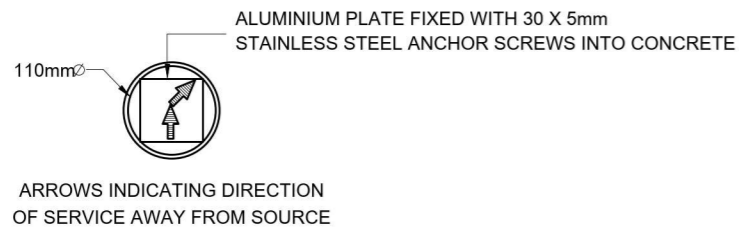


MARKERS FOR PARALLEL UNDERGROUND SERVICES WITHIN ROAD RESERVE

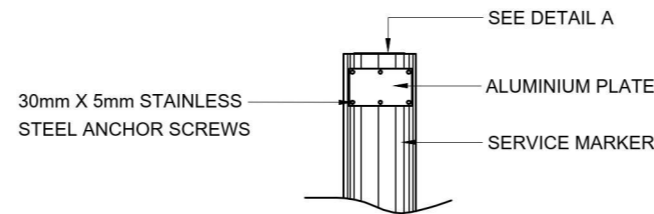


MARKERS FOR UNDERGROUND SERVICES CROSSING ROAD RESERVE

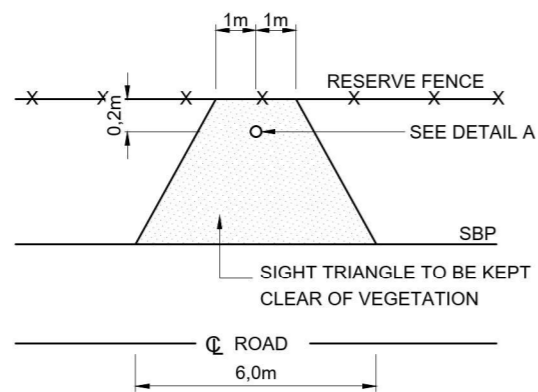
POSITION OF SERVICES MARKERS



DETAIL A



DETAIL B



PLACING OF SERVICES MARKER

- NOTES:**
- SERVICES MARKERS TO BE uPVC CLASS 9 PIPES FILLED WITH CONCRETE CLASS 15/20 (1:3:6 MIX).
 - LENGTH OF PIPE : 1000mm ABOVE GROUND
500mm BELOW GROUND
 - SERVICE MARKER TO BE PAINTED ACCORDING TO COLOUR CODE AS SHOWN, IF REQUIRED BY ROAD AUTHORITY.
 - EACH MARKER IS TO HAVE AN ALUMINIUM PLATE WITH THE DETAIL OF SERVICE AND OWNER PUNCHED ONTO IT (SEE DETAIL B).
 - THE TOP OF EACH MARKER IS ALSO TO HAVE AN ALUMINIUM PLATE WITH ARROWS PUNCHED ONTO IT INDICATING THE DIRECTION OF THE SERVICE AWAY FROM IT'S SOURCE. (SEE DETAIL A)
 - SERVICES MARKERS TO BE PROVIDED ON ALL ROADS.

SERVICE COLOUR CODES	
TYPE OF SERVICE	COLOUR
PETRONET PIPELINES	ORANGE
ESKOM CABLES	RED
TELKOM CABLES	YELLOW
ELECT.CABLES (PRIVATE)	RED
WATER PIPELINES	BLUE
TRANSTEL CABLES	BROWN

No.	DATE	ADDITIONS AND AMENDMENTS
0	OCT - 2023	ORIGINAL VERSION

STANDARD PLANS

WESTERN CAPE GOVERNMENT
DEPARTMENT OF INFRASTRUCTURE
TRANSPORT INFRASTRUCTURE BRANCH

SERVICE DUCTS

DETAILS OF SERVICE DUCT MARKERS

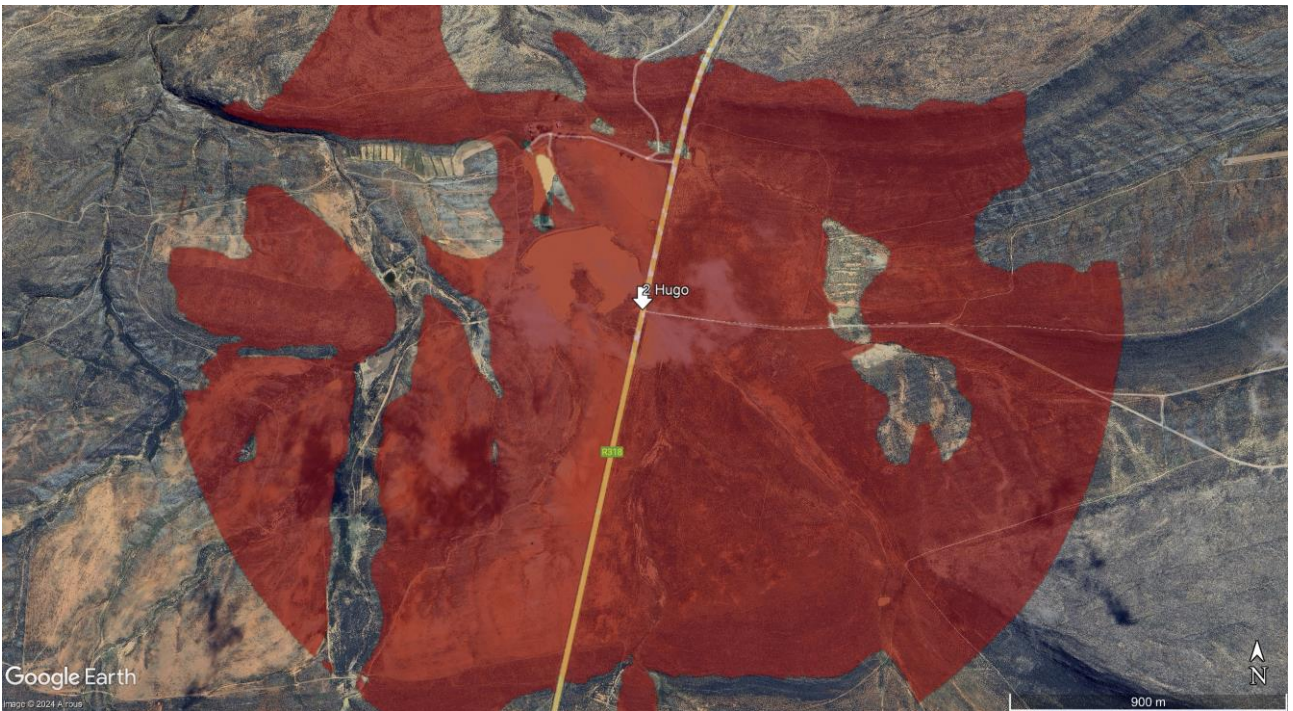
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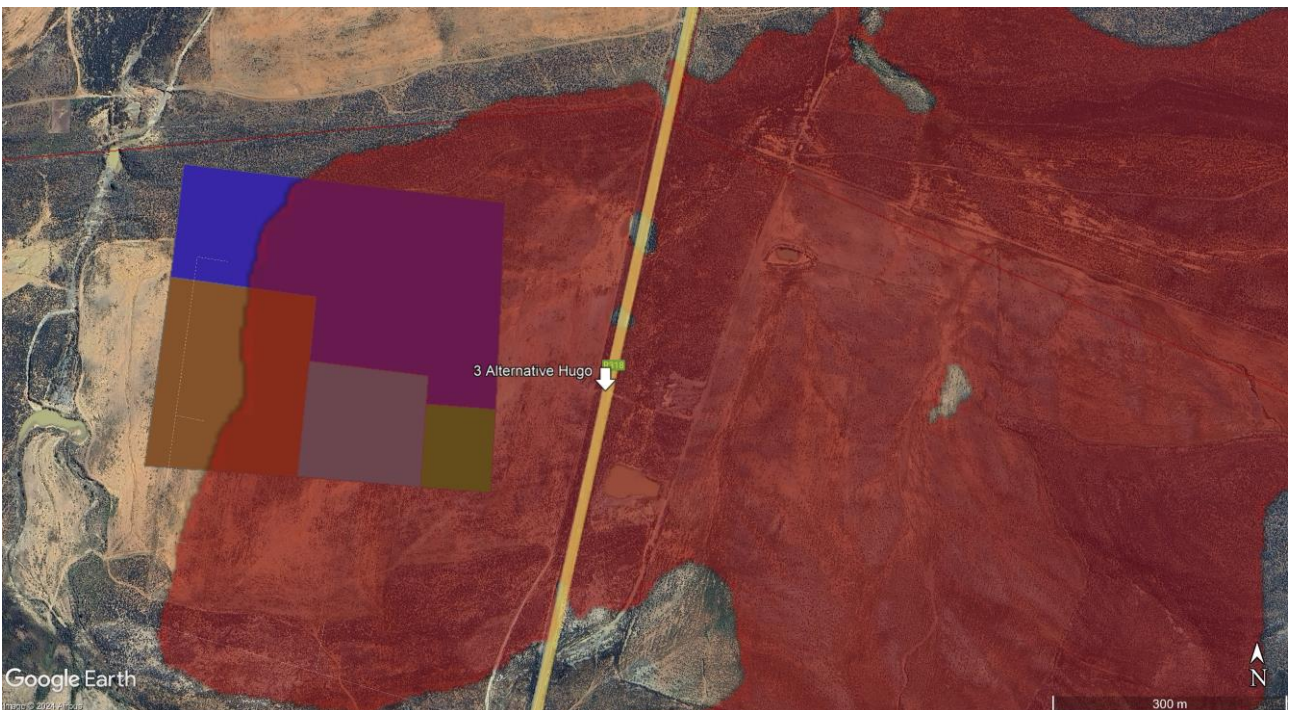
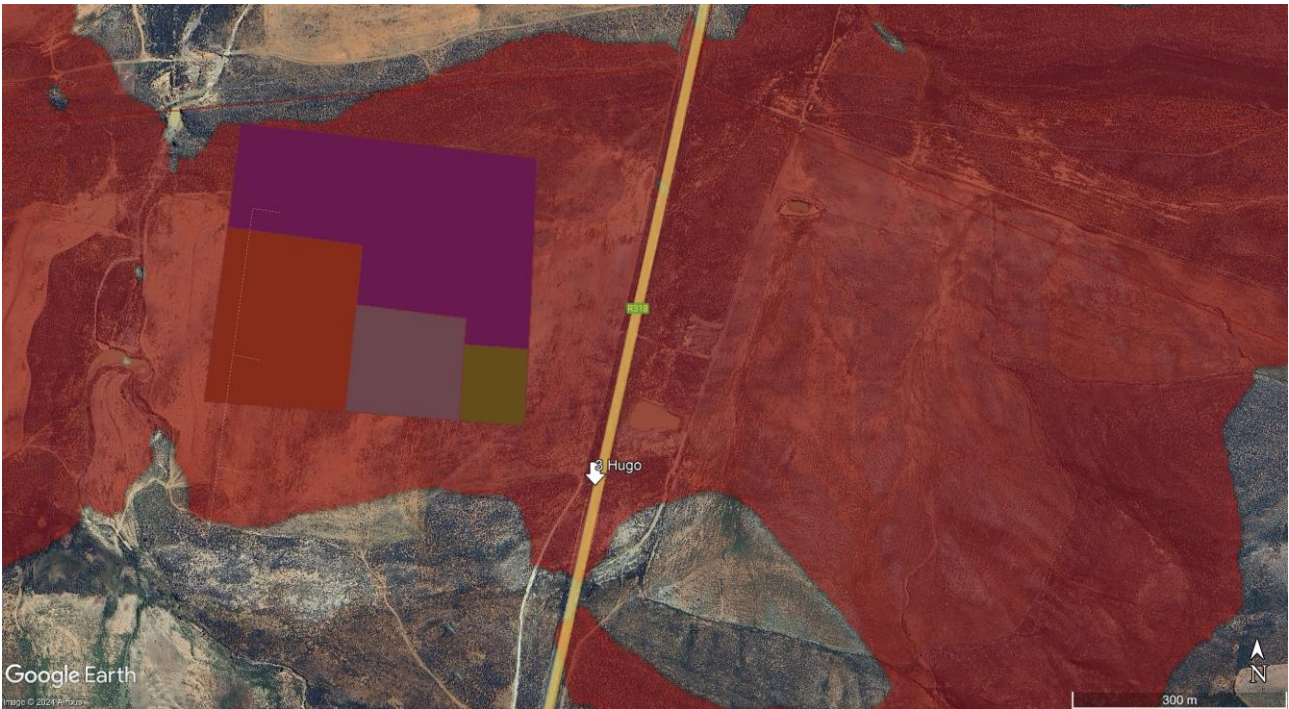
A2 ORIGINAL

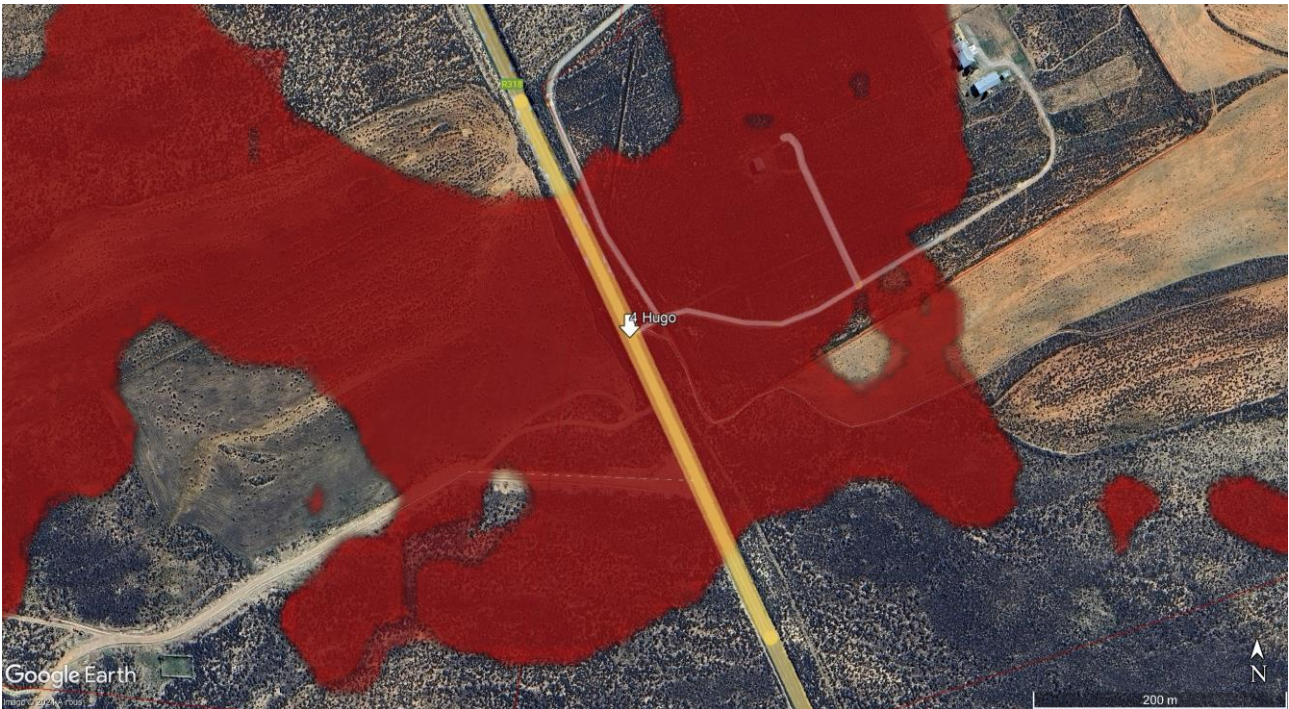
INDEX NO.
WCS/22/4/C2

PLAN NO.
SHEET 2 OF 2

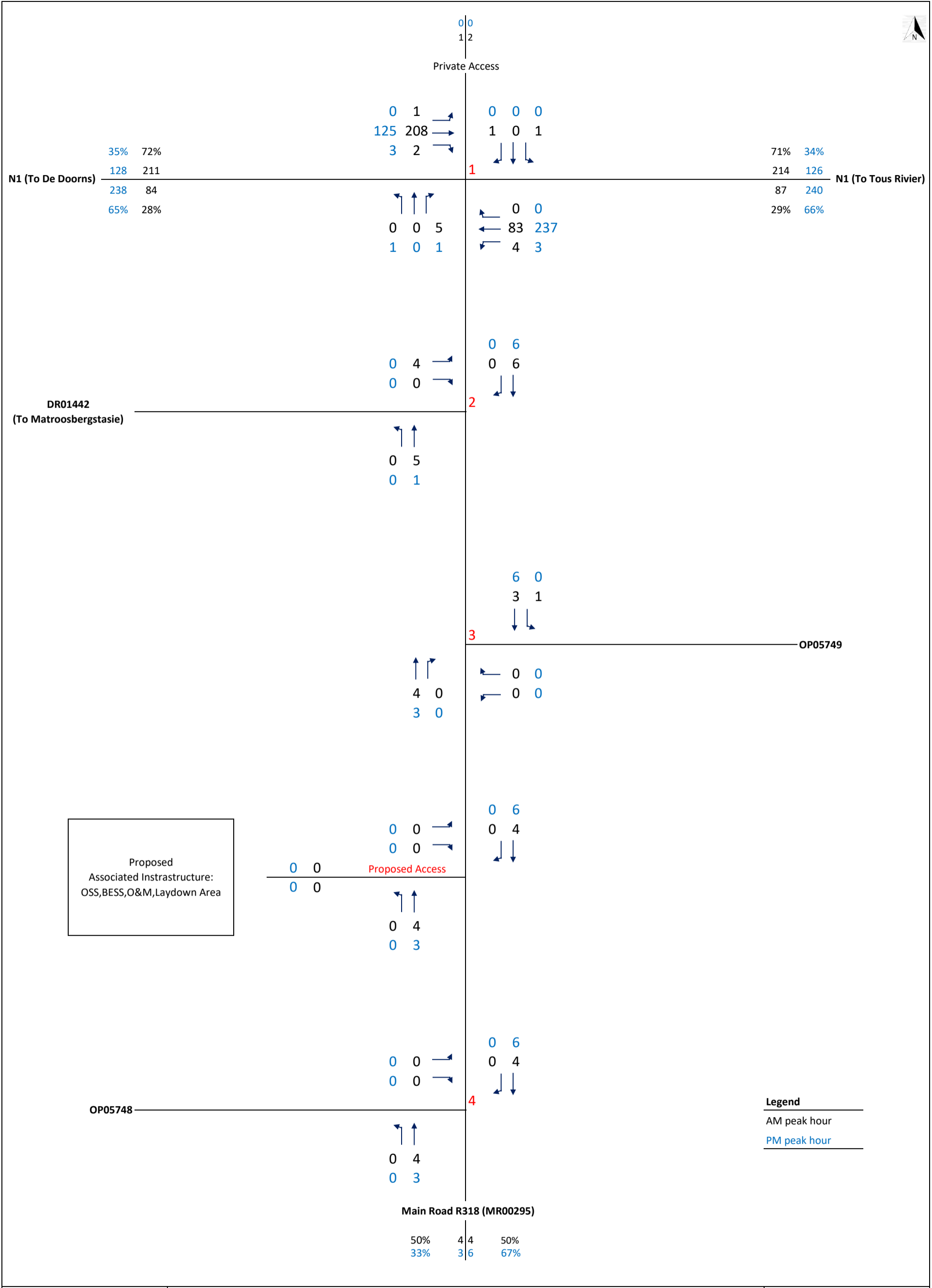
Appendix I – Sight Distance Assessment





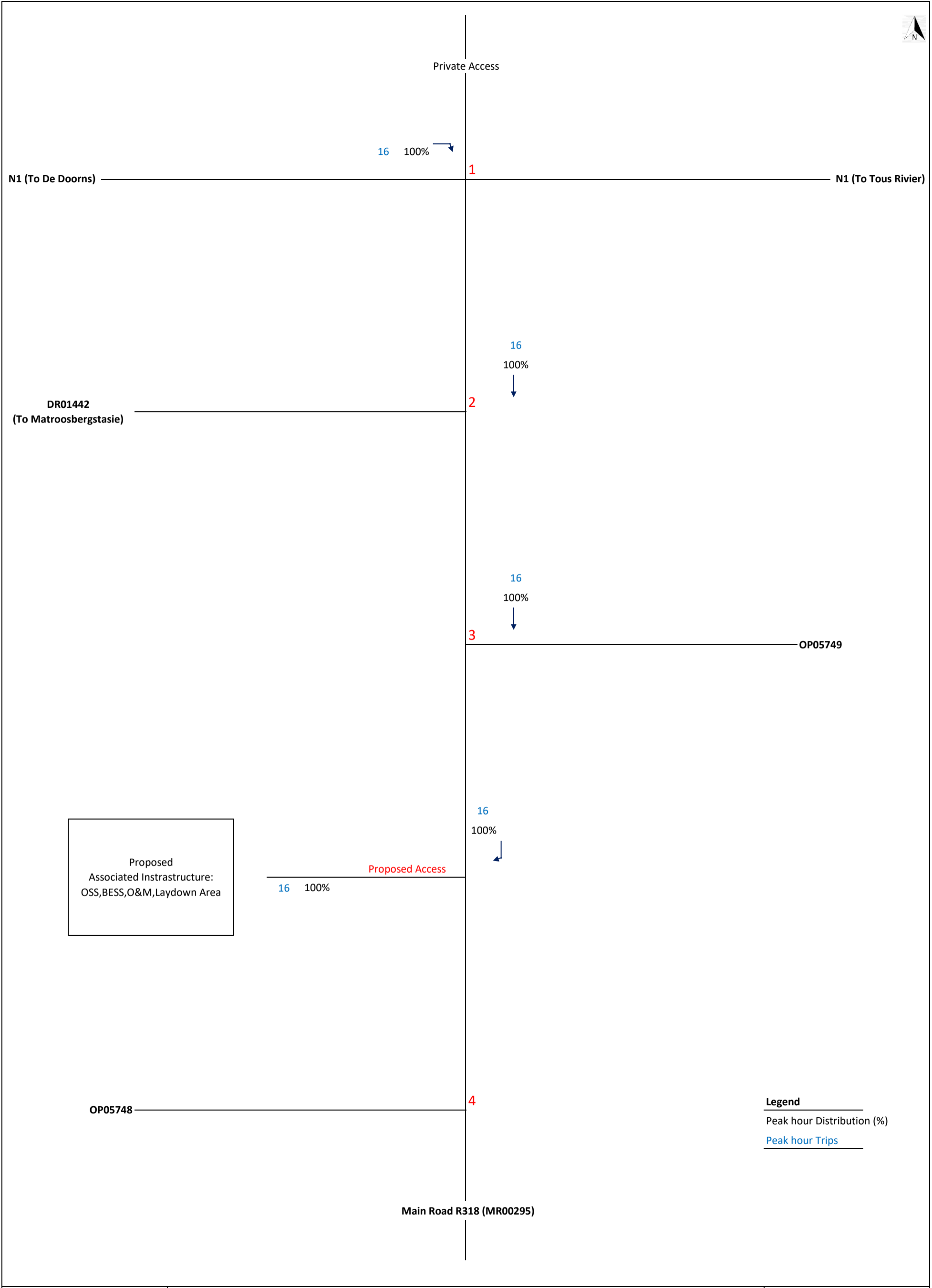


Appendix J – Traffic Flow Diagrams



Proposed
 Associated Infrastructure:
 OSS, BESS, O&M, Laydown Area



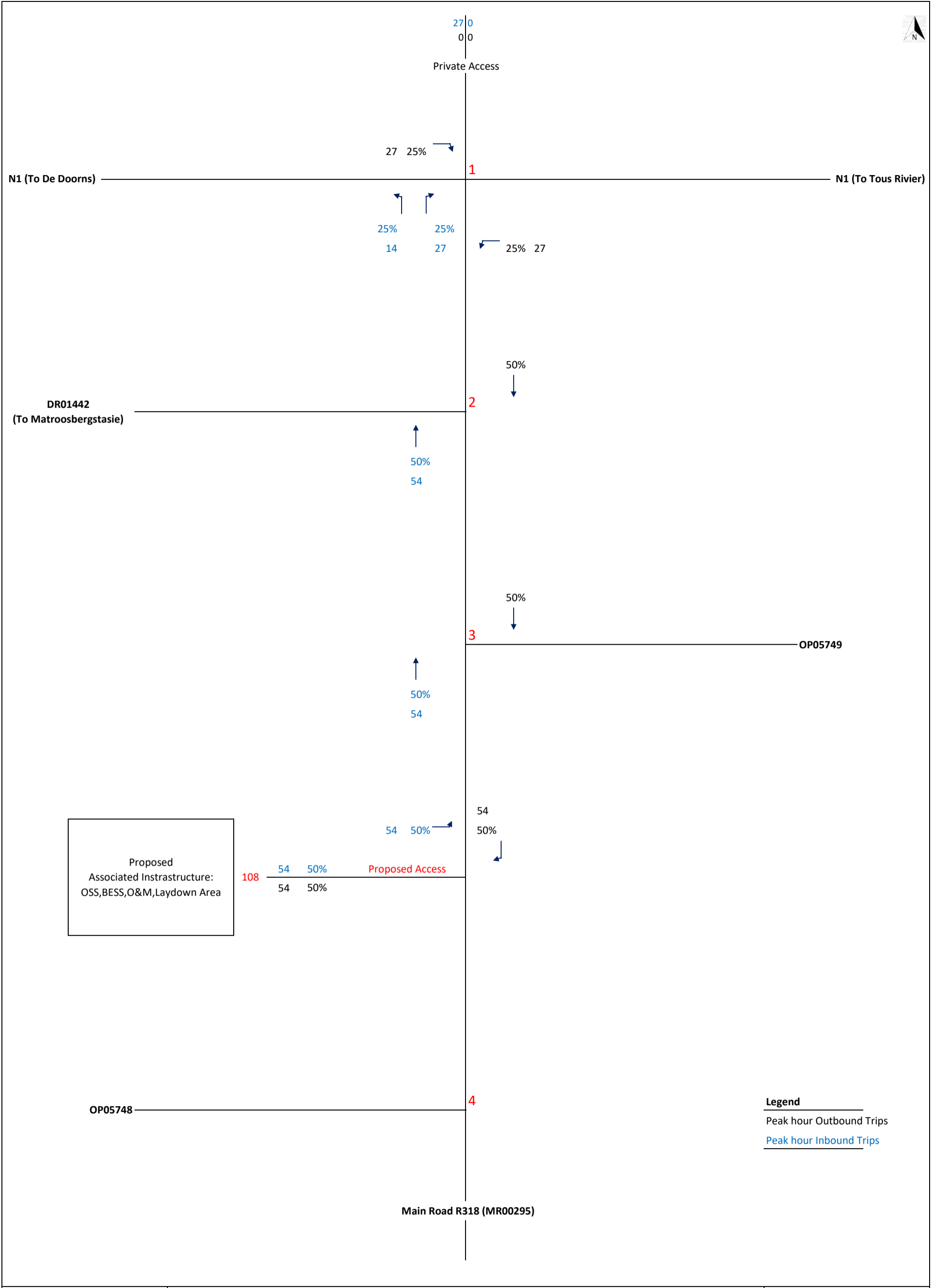


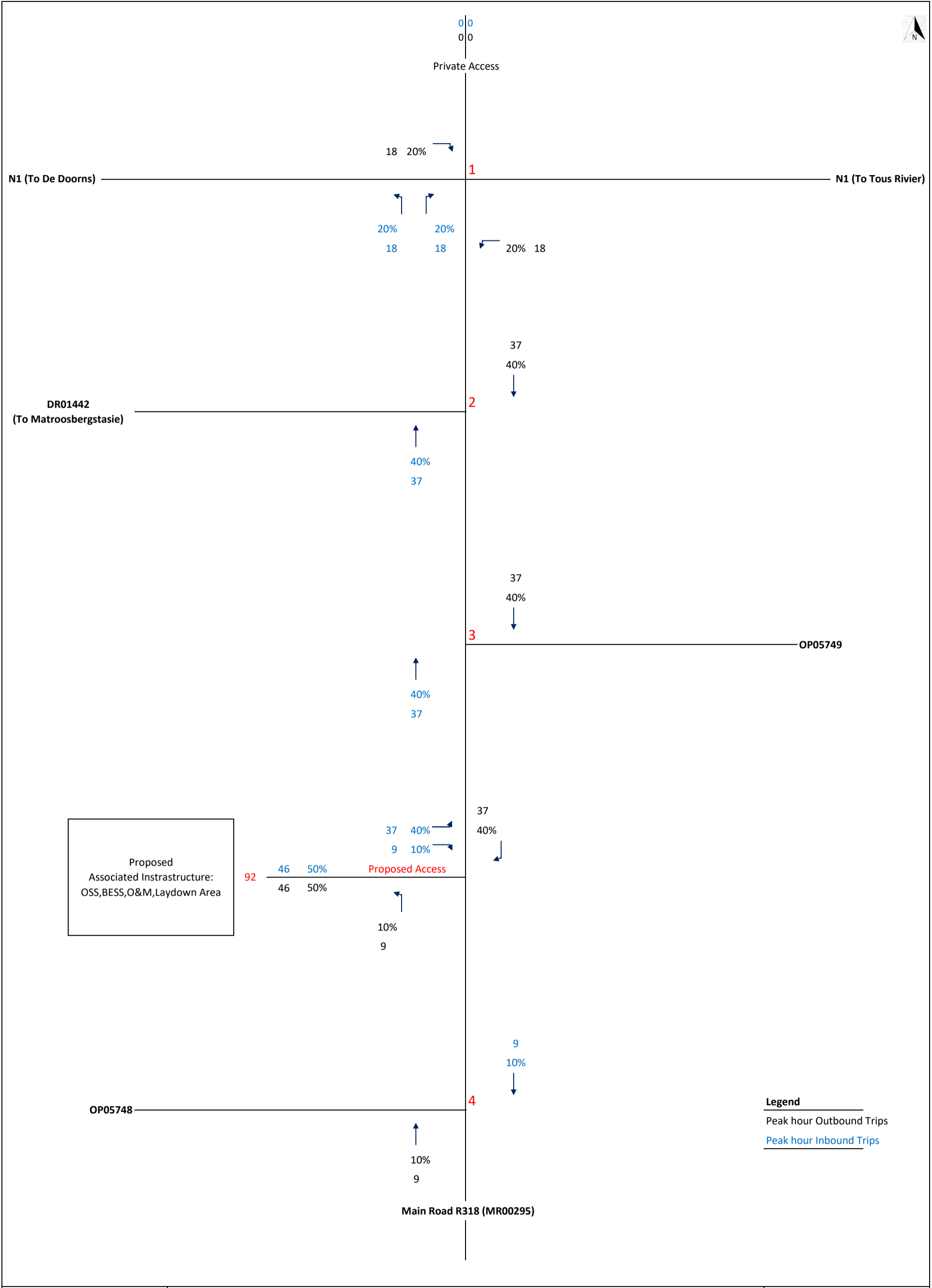
Legend
 Peak hour Distribution (%)
 Peak hour Trips

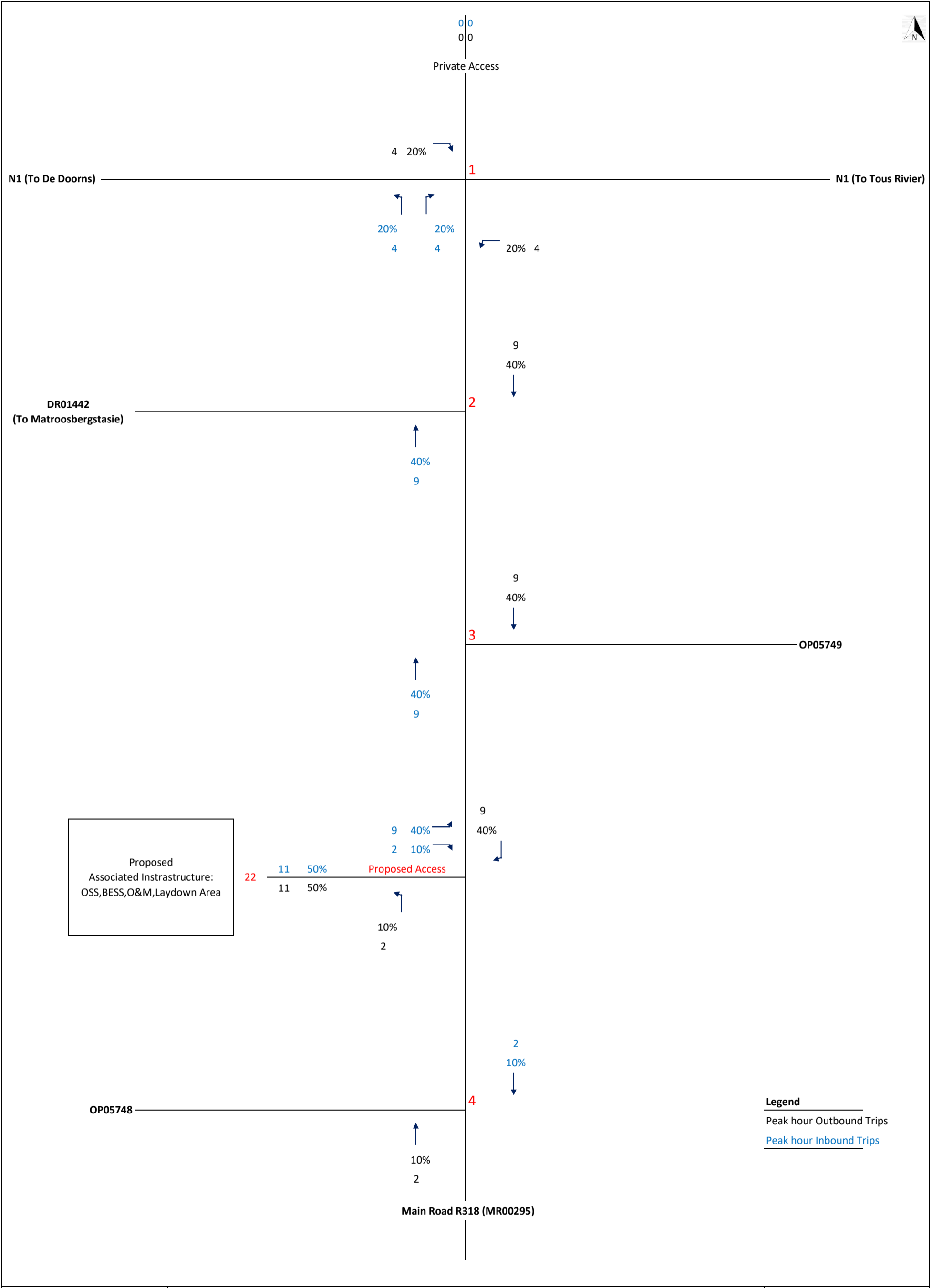


Hugo WEF
 Construction Phase Distribution (%)
 Abnormal Load

Figure J2





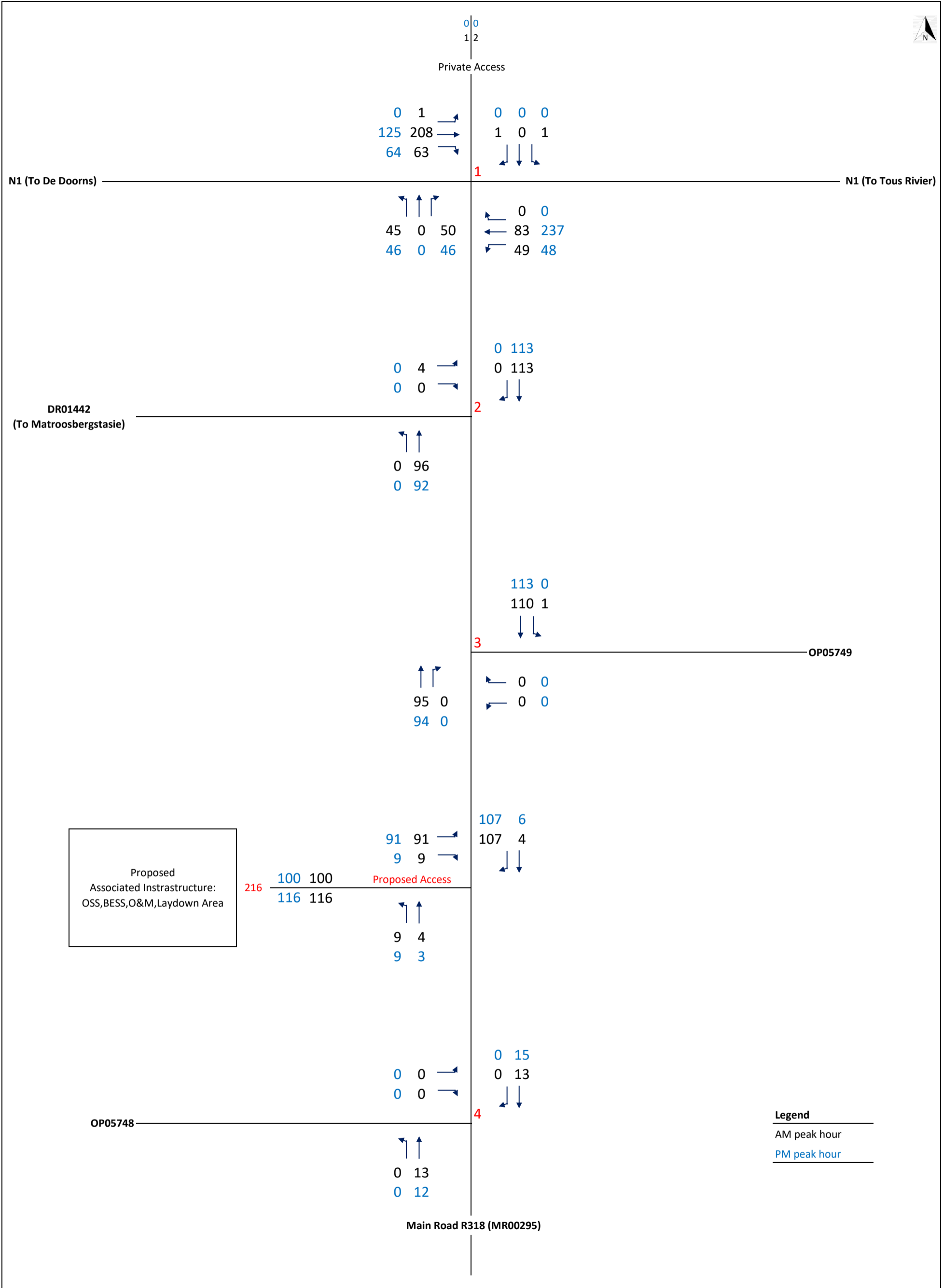


Legend
 Peak hour Outbound Trips
 Peak hour Inbound Trips



Hugo WEF
 Operational Phase Distribution (%)
 Labour

Figure J5



Proposed
Associated Infrastructure:
OSS, BESS, O&M, Laydown Area

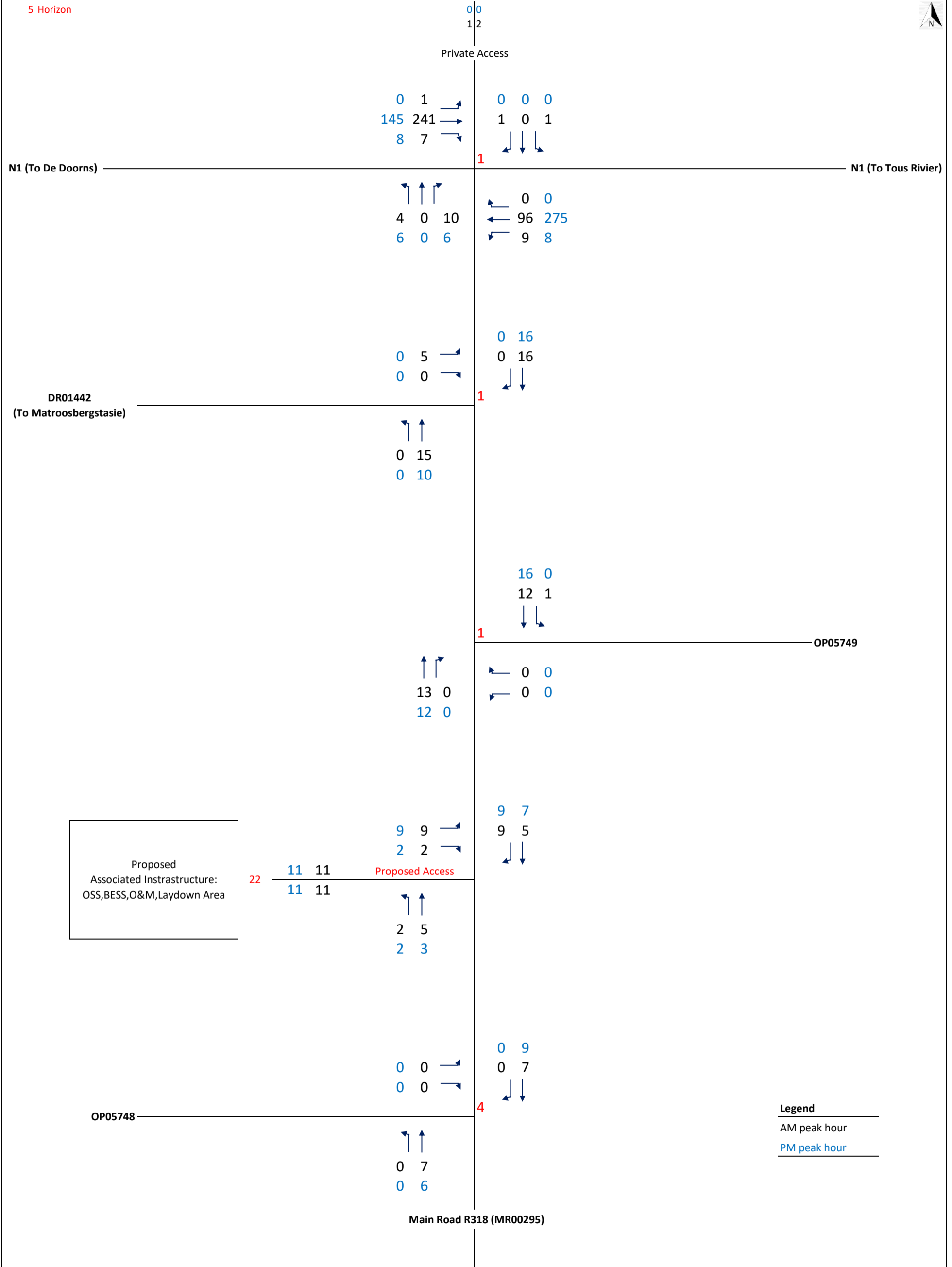
Legend
AM peak hour
PM peak hour

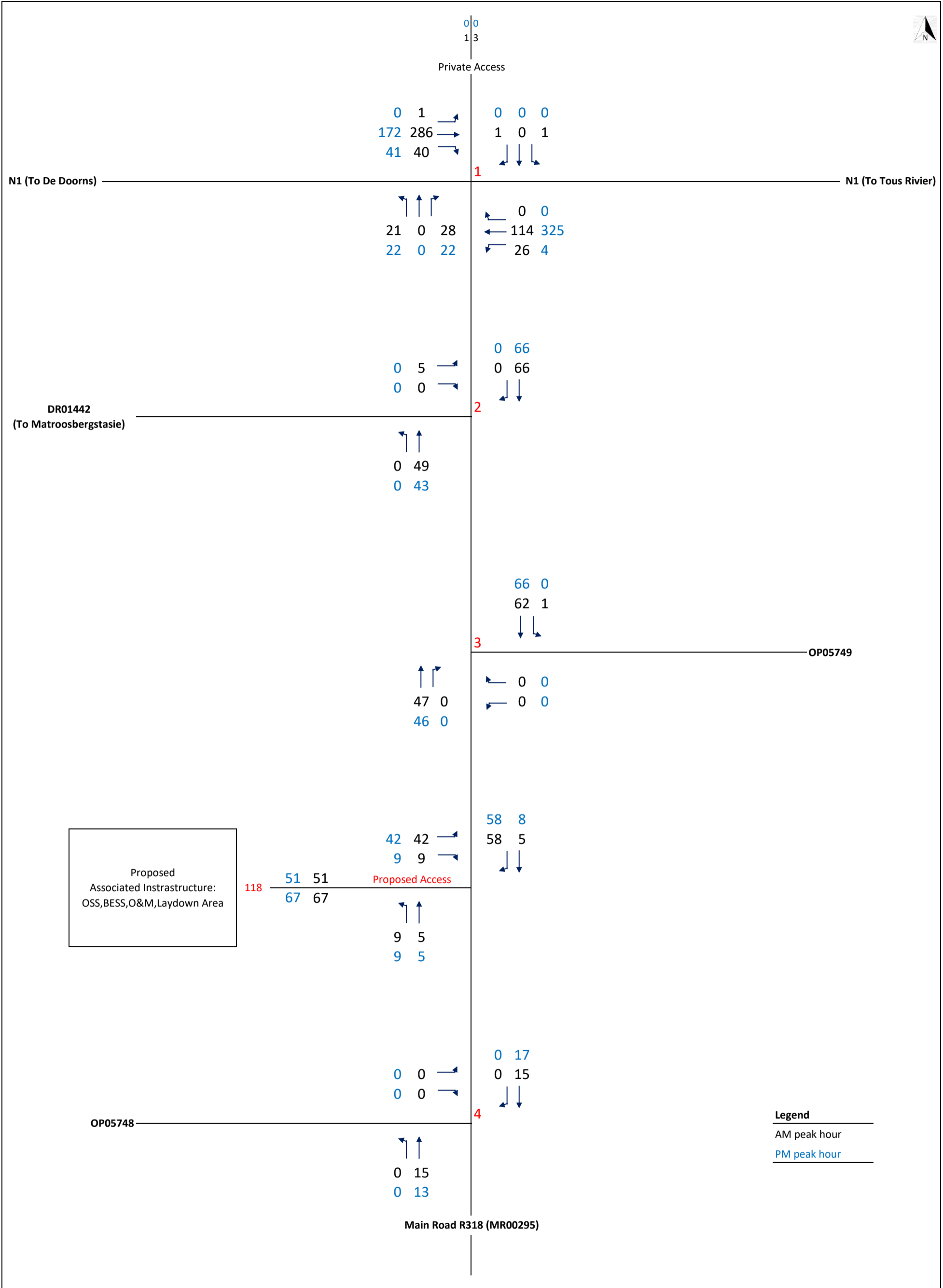


Hugo WEF
2024 Base Year Traffic + Construction Phase Traffic
Total AM Peak Hour & PM Peak Hour

Figure J6

3% Annual Traffic
5 Horizon





Hugo WEF
 2046 Background Traffic + Construction Phase Traffic
 Total AM Peak Hour & PM Peak Hour

Figure J8

Appendix K – Impact Assessment Methodology

1 SPECIALIST REPORTING REQUIREMENTS

The Specialist EIA Report must comply with the requirement of GN 43110 of NEMA: Environmental Themes Reporting Criteria and the Relevant Protocols Gazetted, unless no protocol is prescribed, then the Appendix 6 of the EIA Regulations, 2014 (as amended), must be followed, as well as other relevant protocols, guidelines, policies and/or plans.

The specialist report will include the specialist impact assessment of the proposed developments. The terms of reference for specialist studies includes (but is not limited to):

- Site Visit
- Desktop Screening
- Mapping
- Sensitivity Analysis and/or modelling
- Submission of Shapefiles
- Defining the legal, planning and policy context,
- Description of the Baseline Environment
- Determination of potential impacts (direct, indirect, cumulative)
- Determination of residual risks
- Reporting
- Recommendation and input into project design
- Management Plan and/or Monitoring Programme for inclusion in the EMPr
- Sensitivity Verification Reporting in terms of GN 320 of 20 March 2020 and/or a Compliance Statement in terms of GN 320 / GN 1150 of 20 March 2020

2 IMPACT ASSESSMENT METHODOLOGY

The purpose of the assessment of impacts in an EIA is to evaluate the likely extent and overall significance that a potential impact may have on an identified receptor or resource. Another important aspect of the assessment of impacts is to quantify those impacts that are not scientific-based or evidence-based and include the opinions of others (i.e., the involvement and comment from I&APs).

A successful assessment of the potential significance of impacts will include the description and development of measures that will be taken to avoid, minimise or compensate for any adverse environmental impacts, to enhance positive impacts, and to report the significance of residual impacts that occur following mitigation.

A 7-step approach for the determination of significance of potential impacts was developed by ERM to align with the requirements of Appendix 3 of the EIA Regulations, 2014 (as amended). The approach is both objective and scientific based to allow appointed specialists and EAPs to retain independence throughout the assessment process.

ERM has adapted this 7-step approach from standard ranking metrics such as the Hacking Method, Crawford Method etc. The ERM 7-step approach complies with the method provided in the EIA guideline document (GN 654 of 2010) and considers international EIA Regulatory reporting standards such as the newly amended European Environmental Impact Assessment (EIA) Directive (2014/52/EU).

The 7-Step approach for determining the significance of impacts pre, and post mitigation, is described below:

- **Step 1:** Predict potential impacts by means of an appraisal of:
 - Site Surveys,
 - Project-related components and infrastructure,
 - Activities related with the project life-cycle,

- The nature and profile of the receiving environment and potential sensitive environmental features and attributes,
 - Input received during public participation from all stakeholders, and
 - The relevant legal framework applicable to the proposed development
- **Step 2:** Determination of whether the potential impacts identified in **Step 1** will be *direct* (caused by construction, operation, decommissioning or maintenance activities on the proposed development site or immediate surroundings of the site), *indirect* (not immediately observable or do not occur on the proposed development site or immediate surroundings of the site), *residual* (those impacts which remain after post mitigation) and *cumulative* (the combined impact of the project when considered in conjunction with similar projects in proximity).
 - **Step 3:** Description and determination of the significance of the predicted impacts in terms of the criteria below to ensure a consistent and systematic basis for the decision-making process. Significance is numerically quantified on the basis score of the following impact parameters:
 1. **Extent (E)** of the impact: The geographical extent of the impact on a given environmental receptor.
 2. **Duration (D)** of the impact: The length of permanence of the impact on the environmental receptor.
 3. **Reversibility (R) of the impact:** The ability of the environmental receptor to rehabilitate or restore after the activity has caused environmental change
 4. **Magnitude (M)** of the impact: The degree of alteration of the affected environmental receptor.
 5. **Probability (P)** of the impact: The likelihood of the impact actually occurring.

A widely accepted numerical quantification of significance is the formula:

$$S=(E+D+R+M)*P$$

Where: *Significance=(Extent+Duration+Reversibility+Magnitude) * Probability*

The following has also been considered when determining the significance of a potential impact.

6. **Nature (N)** of the impact: A description of what causes the effect, what will be affected, and how it will be affected.
7. **Status (S)** of the impact: described as either positive, negative or neutral
8. **Cumulative impacts.**
9. Inclusion of **Public comment.**

The significance of environmental impacts is determined and ranked by considering the criteria presented in **Table 1** below. All criteria are rank according to 'Very Low', 'Low', 'Moderate', 'High' and 'Very High' and are assigned scores of 1 to 5 respectively.

Table 1: Defining the significant in terms of the impact criteria.

Impact Criteria	Definition	Score	Criteria Description
Extent (E)	Site	1	Impact is on the site only
	Local	2	Impact is localized inside the activity area
	Regional	3	Impact is localized outside the activity area
	National	4	Widespread impact beyond site boundary. May be defined in various ways, e.g. cadastral, catchment, topographic

Impact Criteria	Definition	Score	Criteria Description
	International	5	Impact widespread far beyond site boundary. Nationally or beyond
Duration (D)	Immediate	1	On impact only
	Short term	2	Quickly reversible, less than project life. Usually up to 5 years.
	Medium term	3	Reversible over time. Usually between 5 and 15 years.
	Long term	4	Longer than 10 years. Usually for the project life.
	Permanent	5	Indefinite
Magnitude (M)	Very Low	1	No impact on processes
	Low	2	Qualitative: Minor deterioration, nuisance or irritation, minor change in species/habitat/diversity or resource, no or very little quality deterioration. Quantitative: No measurable change; Recommended level will never be exceeded.
	Moderate	3	Qualitative: Moderate deterioration, discomfort, Partial loss of habitat /biodiversity /resource or slight or alteration. Quantitative: Measurable deterioration; Recommended level will occasionally be exceeded.
	High	4	Qualitative: Substantial deterioration death, illness or injury, loss of habitat /diversity or resource, severe alteration or disturbance of important processes. Quantitative: Measurable deterioration; Recommended level will often be exceeded(e.g. pollution)
	Very High	5	Permanent cessation of processes
Reversibility (R)	Reversible	1	Recovery which does not require rehabilitation and/or mitigation.
	Recoverable	3	Recovery which does require rehabilitation and/or mitigation.
	Irreversible	5	Not possible, despite action. The impact will still persist, and no mitigation will remedy or reverse the impact.
Probability (P)	Improbable	1	Not likely at all. No known risk or vulnerability to natural or induced hazards
	Low Probability	2	Unlikely; low likelihood; Seldom; low risk or vulnerability to natural or induced hazards
	Probable	3	Possible, distinct possibility, frequent; medium risk or vulnerability to natural or induced hazards.
	Highly Probable	4	Highly likely that there will be a continuous impact. High risk or vulnerability to natural or induced hazards
	Definite	5	Definite, regardless of prevention measures.

The *significance* (s) of potential impacts identified according to the criteria above has been colour coded for the purpose of comparison. This colour coding will be used in impact tables.

Significance is deemed Negative (-)			Significance is deemed Positive (+)		
0 - 30	31 - 60	61 - 100	0 - 30	31 - 60	61 - 100
Low	Moderate	High	Low	Moderate	High

- **Step 4:** Determination of practical and reasonable mitigation measures based on specialists' inputs and field observations following the mitigation hierarchy (avoid, minimise, manage, mitigate, or rehabilitate).
- **Step 5:** Evaluation of predicted residual impacts after implementation of mitigation measures.
- **Step 6:** Determination of the significance of the impact taking into consideration the predicted residual impacts after implementation of mitigation measures.
- **Step 7:** Based on an acceptable significance of the impact, determination of the need and desirability of the proposed development and an opinion as to whether the development should proceed or not.

Appendix L – Specialist Declaration Form_August 2023



forestry, fisheries & the environment

Department:
Forestry, Fisheries and the Environment
REPUBLIC OF SOUTH AFRICA

Private Bag X447, Pretoria, 0001, Environment House, 473 Steve Biko Road, Pretoria, 0002 Tel: +27 12 399 9000, Fax: +27 86 625 1042

SPECIALIST DECLARATION FORM – AUGUST 2023

Specialist Declaration form for assessments undertaken for application for authorisation in terms of the National Environmental Management Act, Act No. 107 of 1998, as amended and the Environmental Impact Assessment (EIA) Regulations, 2014, as amended (the Regulations)

REPORT TITLE

Traffic Impact Assessment: Proposed Hugo Wind Energy Facility (WEF)

Kindly note the following:

1. This form must always be used for assessment that are in support of applications that must be subjected to Basic Assessment or Scoping & Environmental Impact Reporting, where this Department is the Competent Authority.
2. This form is current as of August 2023. It is the responsibility of the Applicant / Environmental Assessment Practitioner (EAP) to ascertain whether subsequent versions of the form have been published or produced by the Competent Authority. The latest available Departmental templates are available at <https://www.dffe.gov.za/documents/forms>.
3. An electronic copy of the signed declaration form must be appended to all Draft and Final Reports submitted to the department for consideration.
4. The specialist must be aware of and comply with 'the Procedures for the assessment and minimum criteria for reporting on identified environmental themes in terms of sections 24(5)(a) and (h) and 44 of the act, when applying for environmental authorisation - GN 320/2020', where applicable.

1. SPECIALIST INFORMATION

Title of Specialist Assessment	Traffic Impact Assessment: Proposed Hugo Wind Energy Facility (WEF)
Specialist Company Name	SMEC South Africa (Pty) Ltd
Specialist Name	Victor de ABREU
Specialist Identity Number	6310295131087
Specialist Qualifications:	Master of Science in Engineering
Professional affiliation/registration:	Professional Engineer (ECSA) – Membership No. 950108, 16/03/1995
Physical address:	267 Kent Avenue, Ferndale, Johannesburg, 2194, South Africa
Postal address:	PO Box 72927
Postal address	Pinegowrie, 2023
Telephone	+27 11 369 0600
Cell phone	+27 82 416 9393
E-mail	Victor.deAbreu@smec.com

SPECIALIST DECLARATION FORM – AUGUST 2023

2. DECLARATION BY THE SPECIALIST

I, Victor de Abreu declare that –

- I act as the independent specialist in this application;
- I am aware of the procedures and requirements for the assessment and minimum criteria for reporting on identified environmental themes in terms of sections 24(5)(a) and (h) and 44 of the National Environmental Management Act (NEMA), 1998, as amended, when applying for environmental authorisation which were promulgated in Government Notice No. 320 of 20 March 2020 (i.e. “the Protocols”) and in Government Notice No. 1150 of 30 October 2020.
- I will perform the work relating to the application in an objective manner, even if this results in views and findings that are not favourable to the applicant;
- I declare that there are no circumstances that may compromise my objectivity in performing such work;
- I have expertise in conducting the specialist report relevant to this application, including knowledge of the Act, Regulations and any guidelines that have relevance to the proposed activity;
- I will comply with the Act, Regulations and all other applicable legislation;
- I have no, and will not engage in, conflicting interests in the undertaking of the activity;
- I undertake to disclose to the applicant and the competent authority all material information in my possession that reasonably has or may have the potential of influencing –
 - any decision to be taken with respect to the application by the competent authority; and;
 - the objectivity of any report, plan or document to be prepared by myself for submission to the competent authority;
- All the particulars furnished by me in this form are true and correct; and
- I realise that a false declaration is an offence in terms of Regulation 48 and is punishable in terms of section 24F of the NEMA Act.



Signature of the Specialist

SMEC South Africa (Pty) Ltd

Name of Company:

05 Aug 2024

Date

SPECIALIST DECLARATION FORM – AUGUST 2023

3. UNDERTAKING UNDER OATH/ AFFIRMATION

I, Victor de Abreu, swear under oath / affirm that all the information submitted or to be submitted for the purposes of this application is true and correct.

Signature of the Specialist

SMEC South Africa (Pty) Ltd

Name of Company

5 Aug 2024

Date

~~DAVIDENE~~ America

Signature of the Commissioner of Oaths

05 | 08 | 2024

Date

DAVIDENE AMERICA
Senior Proposal Administrator
Commissioner of Oaths
Area: Johannesburg North
Date: 31 January 2022
Reference: RO-05/01/2022
267 Kent Avenue, Ferndale, Randburg, 2194

Appendix M – Specialist Detailed CV



Personal Information

- ID no.: 631029
- Nationality: South African

Years of Industry Experience

- 34+ years

Qualifications and Memberships

- Master of Science in Engineering, University of Witwatersrand, 11/12/1990
- Bachelor of Science in Civil Engineering, University of Witwatersrand, 10/12/1985
- Graduate Diploma in Engineering, University of Witwatersrand, 13/12/1988
- Professional Engineer (ECSA) – Membership No. 950108, 16/03/1995
- Fellow (SAICE) - Membership No. 038948

Key Skills and Competencies

- Transport Planning
- Traffic Engineering
- Highway Design
- Highway Management
- Sustainable Transport
- Business Development
- Strategic Management
- Project Management
- Skills Development & Mentoring

Professional Overview

Victor de Abreu is a registered Professional Civil Engineer with over 33 years' experience in the Traffic and Transport planning field. He holds a BSc, MSc and GDE from WITS University.

Victor has worked in both the private and public sectors (municipal and provincial level) in South Africa and in the United Kingdom as a consultant.

Although his main field of expertise is Transport Planning and Traffic Engineering, he has operated in environments with an infrastructure focus particularly related to Roads and Stormwater management and design.

Rail, event planning and the effect of the 4th industrial revolution on transport are other speciality areas that Victor has a particular interest in.

Victor has held senior management positions in medium and large consultancy environments and serves in a voluntary capacity in SAICE as well as at board level in the education sector. Victor currently sits on the Board of SMEC South Africa

Relevant Project Experience

JU0116: New City (Project name under NDA), Western Region, Saudi Arabia

Client: (undisclosed under NDA) | **Date:** Jan 2022 – Ongoing

Client Contact Details: (undisclosed under NDA).

Consultant details: Sybille Tildsley, Consultant Representative, Surbana Jurong, Email: sybille.tildsley@smec.com

Description: Mega project located in the middle east

Role and Responsibilities: Technical Transportation Lead responsible for delivery of the mobility planning aspects

C1965: Lake Volta Masterplan, Ghana | R 1 700 000

Client: Volta River Authority (VRA) | **Date:** 2022 – Jan 2024

Client Contact Details: SMEC Ghana, Paulo Trinidad, paulo.trinidad@smec.com
Ph: +212 537 650 575

Description: Masterplanning around the Lake Volta Transport Regional and selected Urban Areas and Infrastructure planning only selected urban areas of Phase 1 and Phase 2

Role and Responsibilities: Technical Lead Transportation Engineer responsible for the technical team lead, supervision and reviewing of all reports, tasks and submissions

J0063 Greater Diepsloot Transport Master Plan for the City of Johannesburg | R 2.1 million

Client: City of Johannesburg | **Date:** 2021 – June 2023

Client Contact Details: Esther Letlhaka, Ph: 011 688 7851

Description: Development of a Transport Masterplan for the Greater Diepsloot Area

Role and Responsibilities: Technical Lead Transportation Engineer responsible for the technical team lead, supervision and reviewing of all reports, tasks and submissions

JT0060 Feasibility Study the Introduction of an Integrated Corridor Management Approach for the Orange Farm-Johannesburg Inner City Corridor in the City of Johannesburg | R 3.9 Million

Client: Johannesburg Development Agency | **Date:** 09/06/2021 – 09/10/2022

Client Contact Details: Nobuntu Duze Ph: 011 688 7851

Description: Feasibility study into the introduction of an Integrated Corridor Management ICM which is the management of a Transport Corridor including Public Transport Traffic Management Infrastructure and other elements as a system rather than with individual Transport Modes and elements acting independently.

Role and Responsibilities: Project Director responsible for overall project management, oversight, review and client liaison

XL0048: Mega-Project in Kingdom of Saudi Arabia (Feasibility and Concept Design) – under NDA | Fee Value: SMEC Africa: USD 212 486; SMEC South Africa: R 14 179 869, 35

Client: Bureau Proberts | Date: Oct 2020 – Ongoing

Client Contact Details:

Description: Mega project located in the Middle East. SMEC International signed a Contract with an international architect, Bureau Proberts, who won a design competition for the design of a Lake and Lake Village.

SMEC South Africa is required to provide input to the Feasibility and Concept Design for various Infrastructure components; Dam, Geology, Hydrology, Power, Mobility Planning & Urban Infrastructure of the Lake and Village.

Role and Responsibilities: Lead Transportation Engineer responsible for mobility planning input

DD0098: Public Transport Plan for Durban Inner City and Outer Ring (Planning), KZN South Africa | R 10 million

Client: eThekweni Transport Authority (ETA) | Date: Nov 2017 – Current

Client Contact Details: Robin Chetty; Head PT Planning Ph +27 83 329 2029.

Description: Develop and assess plans, using EMME, Transcad and Aimsun, to improve PT within the Durban Inner City and Outer Ring area, to accommodate future densification within the Inner City of Durban with a 2040 horizon including conceptual design of identified infrastructure interventions as well as Public Transport operational plans for the short, medium and long term.

Role and Responsibilities: Project Director responsible for overall project oversight, Transport engineering, and Technical Reviewer

DD0100: Detailed Public Transport Study for Hill Street Public Transport Precinct, KZN South Africa | R 4 million

Client: eThekweni Transport Authority (ETA) | Date: Jan 2018 – Current

Client Contact Details: Robin Chetty; Head PT Planning Ph +27 83 329 2029.

Description: The Hill Street PT node within Pinetown is congested and needs to integrate well with the new C3 Corridor BRT route. The project was aimed at investigating the situation and recommending and detailing a concept that would result in short and long term improvements to transport in the Pinetown central area.

Role and Responsibilities: Project Director responsible for overall project oversight, Transport engineering, and Technical Reviewer

JT0041 Scenario Fare Testing for Gautrain Phase 2 (Modelling), GP South Africa | R 2.1 million

Client: Gautrain Management Agency (GMA) | Date: 2017, 2018, 2019

Client Contact Details: Victor Shange; Senior Manager: Civil, Perway and Structures; Ph +27 60 995 3059

Description: Assessing the operational and financial impact of fare variability in the Gauteng Rapid Rail Integrated Network (Gautrain Phase 2) with a view to advising provincial treasury of the impact of increasing accessibility through reducing fares on the system.

Role and Responsibilities: Project Director. Overall Project Management and input

JT0042 The Collection, Compilation and Analysis of Private and Public Transport Data in the North-East Quadrant Area of Johannesburg, South Africa | R10m

Client: City of Johannesburg (CoJ) | Date: 16/05/2018 – 16/10/2019

Client Contact Details: Lisa Seftel, Executive Director - Transportation, Ph +27 82 301 6826.

Description: Collection of relevant demand, supply and utilization information on the current public and private transport services and utilisation information within the North East Quadrant (NEQ) area of Johannesburg. The information was used to determine compensation for paratransit services replaced by the CoJ Rea Vaya Phase 1C BRT system.

Role and Responsibilities: Project Director responsible for oversight, Transportation Engineering, Technical Advisor and Reviewer.

Kigali Transport Master Plan Implementation Report Update & GIS Database | R3m

Client: City of Kigali (CoK) | Date: 2018 – 2019

Client Contact Details: Mr Mugabo Vianney; Ph: +250 788 355 357

Description: A transport masterplan was developed for the City of Kigali in Rwanda. The masterplan addressed significant expected

economic growth in the city. The plan was supported by a Macro Demand Model. The road network demand model was used to assess the re-routing of traffic as a result of the socio-economic development plan, planned road network improvements and other demand management interventions. The model is based in the PTV Visum software.

Role and Responsibilities: Project Director

M1, M2, M70 Road Masterplan and Simulation Model, Johannesburg, | ± R 3 700 000

Client: Johannesburg Roads Agency | **Date:** 2017

Client Contact Details: Alan Robinson; Project Manager, Ph +27 62 519 0397

Description: The development of a SATURN simulation model to test various proposed road infrastructure improvements and to determine the demand that has to be accommodated on the network. The process involved interaction with the City of Johannesburg's multi-modal demand model. The forecast demand flows were extracted from the SATURN model and used to develop the road master plan and provided to the design teams to inform the detailed geometric designs and micro-simulation where relevant.

Role and Responsibilities: Project Director

OR Tambo SATURN TIA | R700k

Client: AMCE on behalf of Mangaung Department of Settlements | **Date:** 2018

Client Contact Details: Givon Van Eyck; Business Development Manager, Ph +27 11 312 1569

Description: Development of a SATURN Model to test the impact of a mixed use development in Mangaung, Bloemfontein. The development is made up of Vista Park 2, 3 and Hillside View with approximately 18 282 residential units to be built within a space of 10 years. The SATURN model took into consideration all latent right demand in the Mangaung area and made appropriate recommendations in terms of upgrade apportionment.

Role and Responsibilities: Project Director

Tswaing Mega-City Development TIA | R568 168

Client: Makole Property Developers | **Date:** 2017, 2018

Description: Development of a SATURN Model to test the impact of the proposed Tswaing Mega City Development on the surrounding road network in the immediate vicinity of the development site. The development will comprise of 510 hectares of mixed land use with approximately 50 000 residents. The development will consist of seven township extensions, namely Tswaing X8, X9, X10, X11A, X11B, X11C and X11D.

Role and Responsibilities: Project Director

JT0059 Traffic Impact Study of Line 2B City of Tshwane | R324 042

Client: Koleko Solutions (Pty) Ltd on behalf of the City of Tshwane | **Date:** 2017

Description: SMEC South Africa was appointed to undertake AIMSUN Simulations Modelling and to revise the Traffic Impact Study of Line 2B BRT. The traffic impact study investigated the impact of introducing BRT on the road network currently utilised by normal traffic. Various scenarios were investigated including whether BRT should run on right of way lanes or whether it should operate on mixed traffic lanes.

Role and Responsibilities: Project Director responsible for Project Oversight, Transportation Engineer, Technical Advisor and Reviewer

ZL0035: Imbuga City Walk Project | R286 079.60

Client: Kigali City | **Date:** 2017

Description: The City of Kigali appointed SMEC South to assist with traffic engineering solutions in the pedestrianisation of KN4 Avenue in Kigali. The task was to assess the impact of the closure of KN4 Avenue to normal traffic and recommend solutions to minimise impact and improve circulation within the city.

Role and Responsibilities: Project Director. The task was to assess the impact of the closure of KN4 Avenue to normal traffic and recommend solutions to minimise impact and improve circulation within the city.

COJ Eco Mobility Festival Transport Planning | R2 477 618

Client: City of Johannesburg | **Date:** 2016

Client Contact Details: Lisa Seftel; Director Transportation, Ph +27 83 231 0380, E lisas@joburg.org.za

Description: Project management of planning and implementation of interventions for the Eco Mobility Festival held in Sandton in 2015. This festival focused on transforming the neighbourhood of Sandton for an entire month and demonstrated the possibilities

of enhancing travel through integrated, socially inclusive, and environmentally friendly options: namely walking, cycling, and public transport.

Role and Responsibilities: Project Director. Project Management; Planning; Design; Execution; Review.

Traffic Impact Assessments | R239 724

Client: City of Johannesburg | **Date:** 2015 – 2016

Client Contact Details: Various

Description: Various TIA's including area wide studies such as Patterson Park to support concept of BRT in the city.

Role and Responsibilities: Project Director. Project Management; Planning; Design; Execution; Review.

Rea Vaya Section 9 Transport Planning | R205 136

Client: City of Johannesburg | **Date:** 2014 – 2015

Client Contact Details: Adrian Brislin, Ph +27 82 600 6757

Description: Concept planning of Section 9 of the City's BRT network from Sandton to Randburg.

Role and Responsibilities: Project Director responsible for project Oversight, Transportation Engineer, Technical Advisor and Reviewer.

COJ Guidelines for Transport Assessments | R973 747

Client: City of Johannesburg | **Date:** 2015

Client Contact Details: Nobuntu Ciko; Project Manager, Ph +27 11 870 4508

Description: Development of guidelines for transport assessments for the city with a focus on moving away from a private vehicle to a public transport and non-motorised transport (NMT) focused approach / environment.

Role and Responsibilities: Project Director. Overview, Design and Review.

DOT National Transport Masterplan | R789 800

Client: National Department of Transport | **Date:** 2013 – 2015

Description: National Transport Masterplan. Involved with the modelling activities related to the inventory, analysis, forward planning and implementation phases of this project.

Role and Responsibilities: Project Director. Involved with the modelling activities related to the inventory, analysis, forward planning and implementation phases of this project.

COT Feeder Network for Phase 1 and 2 of the TRT. | R817 500

Client: City of Tshwane | **Date:** 2013 – 2015

Client Contact Details: Givon Van Eyck, Ph +27 84 279 6759, E gvaneyck@amce.co.za

Description: Planning and Design for implementation of the TRT feeder network bus stop infrastructure and road network upgrades for Phase 1 and 2 of the City's TRT rollout plan.

Role and Responsibilities: Project Director. Project Management; Overview, Design and Review.

COT TRT Feeder Bus Infrastructure Design | R817 500

Client: City of Tshwane | **Date:** 2013 – 2015

Client Contact Details: Givon Van Eyck, Ph +27 84 279 6759, E gvaneyck@amce.co.za

Description: Planning and Design for implementation of the TRT feeder network bus stop infrastructure.

Role: Project Director. Project Oversight, Transportation Engineer, Technical Advisor and Reviewer

JRA Roads and Stormwater Standards | R968 303

Client: Johannesburg Roads Agency (JRA), | **Date:** 2014

Client Contact Details: Philiswe (Gugu) Mbambo, Deputy Direct: Transport Planning and Policy, Ph +27 82 301 6826, E PhilisweM@joburg.org.za

Description: Project lead for the development of Roads and Stormwater standards for the Johannesburg Roads Agency.

Role and Responsibilities: Project Director

COT Development of an NMT Policy | R800k

Client: City of Tshwane | **Date:** 2013 – 2014

Client Contact Details: Bavusile Ramekane, Ph +27 12 358 7822, E bavusiler@tshwane.gov.za

Description: Project lead for City of Tshwane 3-year as and when Traffic Investigations project with projects including development of an NMT Policy for the City, safety assessments on identified high accident zone corridors, NMT and pedestrian assessments as well as review of various Traffic Impact Assessments on behalf of the City.

Role and Responsibilities: Project Director

COT Soshanguve to CBD BRT Planning | R3.5 million

Client: City of Tshwane | **Date:** 2010 – 2014

Client Contact Details: Bavusile Ramekane, Ph +27 12 358 7822, E bavusiler@tshwane.gov.za

Description Concept planning of initial Tshwane Rapid Transit corridor from Soshanguve to CBD in the north of Tshwane.

Role and Responsibilities: Project Director. Project Oversight, Transportation Engineer, Technical Advisor and Reviewer

DPW Traffic Analysis of Operational Aspects | R800k

Client: National Department of Public Works | **Date:** 2007 – 2014

Description: Traffic analysis of operational aspects related to Lebombo border post including assessment of freight, public transport and general traffic flow – the outcomes of this assessment will be utilized to appropriately design infrastructure for the reconstructed facility.

Role and Responsibilities: Project Director.

COT Design of Line 2C of the COT TRT | R3 781 701

Client: City of Tshwane | **Date:** 2013

Client Contact Details: Lloyd Moti; Ph +27 84 422 3544, E lmoti@amce.co.za

Description Design of section of Line 2C of the COT TRT system from Menlyn to Mamelodi.

Role and Responsibilities: Project Director. Project Oversight, Transportation Engineer, Technical Advisor and Reviewer

Rea Vaya Phase 1C Traffic and NMT Assessments | R21 453 795

Client: City of Johannesburg | **Date:** 2012

Client Contact Details: Siyabonga Genu, Ph +27 11 688 7823, E sgenu@jda.org.za

Description: The project entailed being the Traffic discipline lead for traffic assessment of Sections 8 and 15 of the City of Johannesburg Rea Vaya Phase 1C Bus Rapid Transit project including assessment of non-motorised transport requirements adjacent to stations.

Role and Responsibilities: Project Director. Overall project management

COJ Traffic Signal Phasing | R1 million

Client: City of Johannesburg | **Date:** 2006 – 2011

Description: Involved with the collection of intersection configuration, road signs and marking and traffic signal inventory of identified intersections within the Greater Johannesburg area as well as undertaking the necessary traffic counts, traffic signal design and phasing.

Role and Responsibilities: Project Director

DPW Drafting of PDR | R2 307 602

Client: National Department of Public Works | **Date:** 2005 – 2011

Description: Drafting of PDR for Maseru South African High Commission headquarters.

Role and Responsibilities: Project Director

2010 FIFA World Cup™ Transport Operations Plan (TOP) | R300k

Client: City of Johannesburg | **Date:** 2009 – 2010

Client Contact Details: Philiswe (Gugu) Mbambo, Deputy Direct: Transport Planning and Policy, Ph +27 82 301 6826, E PhilisweM@joburg.org.za

Description: Member of team appointed to develop the 2010 FIFA World Cup™ Transport Operations Plan (TOP) for the City of Johannesburg.

Role and Responsibilities: Project Director

COJ Gauteng Freeway Improvement Scheme (GFIS) | R1 million

Client: City of Johannesburg | **Date:** 2009-2010

Description: Assessment of the impact of the Gauteng Freeway Improvement Scheme (GFIS) on the road system in the city.

Role and Responsibilities: Project Director

DPW Drafting of Preliminary Design Report (PDR) for Carletonville Police Precinct | R1.1 million

Client: National Department of Public Works | **Date:** 2005 – 2010

Description: Drafting of Preliminary Design Report (PDR) for Carletonville Police Station that had been decommissioned due to risks associated with sinkhole formation due to dolomites.

Role and Responsibilities: Project Director

ORTIA Assessment of Traffic Impacts | R1 720 853

Client: OR Tambo International Airport | **Date:** 2008 – 2009

Description: Assessment of traffic impact landside as a result of predicted passenger growth airside.

Role and Responsibilities: Project Director

ORTIA Traffic Study | R450k

Client: OR Tambo International Airport | **Date:** 2008 – 2009

Description: Traffic Study of entrance and exit to new Multi Storey Parkade 3 and capacity analysis of Spine Road at critical points at ORTIA.

Role and Responsibilities: Project Director

DOT Initial Transport Operations Plan (INTOP) | R250k

Client: National Department of Transport | **Date:** 2007 – 2008

Description: Member of team responsible for drafting the Initial Transport Operations Plan (INTOP) for the NDoT for FIFA World Cup™.

Role and Responsibilities: Project Director.

COJ Randburg CBD Upgrade Planning | R400k

Client: City of Johannesburg | **Date:** 2005 – 2007

Description: Recommendations of road network upgrades to support Randburg CBD revitalization initiative.

Role and Responsibilities: Project Director

ACSA Passenger Growth Study at Cape Town, George, BFN, and Kimberley Airports | R2 million

Client: ACSA | **Date:** 2005 – 2006

Description: Cape Town, George, Bloemfontein and Kimberly Airports – Estimation of projected passenger growth at these airports, made recommendations on land-side response in term of infrastructure requirements such as capacity of access roadways as well as internal Parking requirements..

Role and Responsibilities: Project Director

ETA Assessment of Parking Requirements | R3.5m

Client: Ethekwini

Description: Assessment of parking requirements and recommended upgrade of municipal precincts.

Role and Responsibilities: Project Director

ETA Undertaking of Public Transport Study in Welbedacht | R2 million

Client: Ethekwini

Description: Undertaking of public transport study in Welbedacht area to identify requirements for wider community.

Role and Responsibilities: Project Director

ORTIA Traffic Operations | R900k

Client: OR Tambo International Airport

Description: Project management of review of traffic operations and flow at freight cargo facility/terminal

Role and Responsibilities: Project Director

GPG Building Capacity within the Planning Directorate

Client: Gauteng Provincial Government

Description: Building capacity within the planning directorate and assuming mentorship role for internal staff.

Role: Project Director

GPG Audits

Client: Gauteng Provincial Government

Description: Audit and make recommendations on the restructuring of the Planning Directorate in the Department.

Role: Project Director

GPG Project Management

Client: Gauteng Provincial Government

Description: Project management of the transportation requirements for the 2010 World Cup™ at a provincial level.

Role: Project Director

GPG Review of Gauteng Strategic Road Network

Client: Gauteng Provincial Government

Description: Project management and review of the Gauteng Strategic Road Network.

Role: Project Director

GPG Freight Implementation Strategy for Gauteng

Client: Gauteng Provincial Government

Description: Project management and the development of a Freight Implementation Strategy for Gauteng.

Role: Project Director

Regional Call Centre for the 2010 FIFA World Cup™

Client: Gauteng Provincial Government

Description: Initiate project to develop a regional Call Centre for the 2010 FIFA World Cup™.

Role: Project Director

GPG Integrated Ticketing Strategy for Gauteng

Client: Gauteng Provincial Government

Description: Advisory on project initiated to assess an Integrated Ticketing Strategy for Gauteng.

Role: Project Director

GPG Advisory on Traffic Impact Studies for Various Regional Developments in Gauteng

Client: Gauteng Provincial Government

Description: Advisory on traffic impact studies for various regional developments in Gauteng.

Role: Project Director

GPG Public Transport Integration within the Province | R80k

Client: Gauteng Provincial Government

Description: A Represent the department in discussion with Gautrain regarding public transport integration within the province.

Role: Project Director

GPG Development of Concept for Gauride System | R800k

Client: Gauteng Provincial Government

Description: Development of concept for Gauride system for the 2009 FIFA Confederations Cup™.

Role: Project Director

DPW Assessment of Options to Improve Traffic Operations at Maseru Border Post. | R1 million

Client: National Department of Public Works

Description: Assessment of options to improve traffic operations at the South Africa-Lesotho Maseru border post.

Role: Project Director

Professional History

- 2017 – Date | Function General Manager
| SMEC South Africa (Pty) Ltd
- 2005 – 2017 | Director
| MPA Consulting Engineers
- 2003 – 2005 | Member
| VSM Projects
- 2001 – 2003 | Principal Engineer
| Mouchel Consulting Engineers, United Kingdom
- 1995 – 2001 | Head of Public Transport Planning
| Greater Johannesburg Metropolitan Council
- 1990 – 1995 | Assistant Town Engineer
| Sandton Town Council
- 1988 – 1990 | Graduate Engineer
| De Leuw Cather Consulting Engineers

Courses & Conferences attended

N/A

Publications & Papers Presented

2015: Feasibility study on traffic decongestion strategies at Maseru bridge border post South African Transport Conference (2015).

2017: Post Eco-Mobility experiences and lessons learnt (under development) South African Transport Conference (2017).

On-going: External examiner for various MSc dissertations at the University of Pretoria.

On-going: Peer Review papers on NMT and Public Transport Operations for South African Transport Conference (SATC).

Language Skills

Mother Tongue:	English		
Languages	Speak	Read	Write
English	Excellent	Excellent	Excellent
Afrikaans	Good	Good	Good
French	Basic	Basic	Basic
Portuguese	Good	Basic	Basic



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SMEC simplifies the complex. We unlock the potential of our people to look at infrastructure differently, creating better outcomes for the future.

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